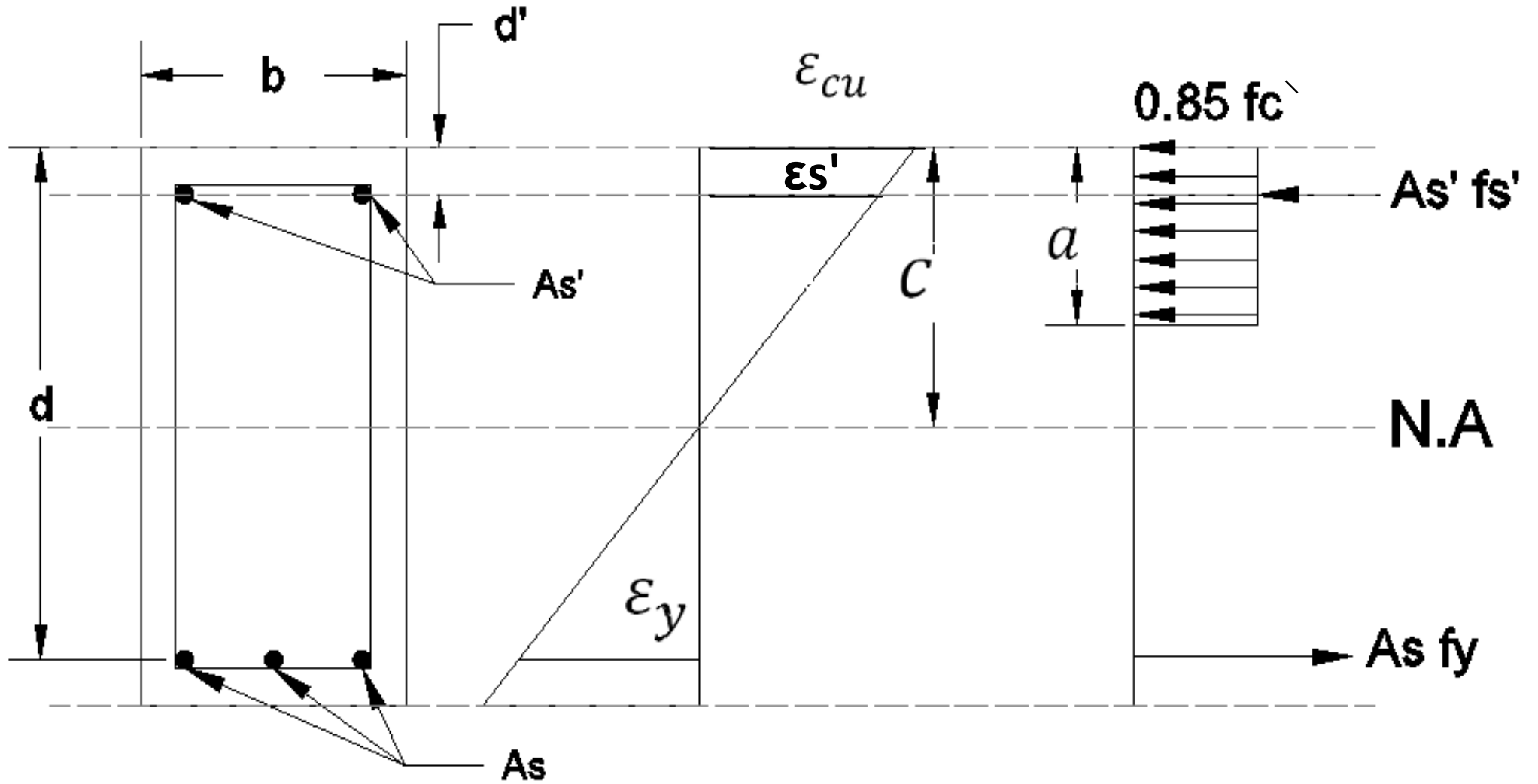


Doubly reinforce section

1. To increase moment capacity of sections having limited dimensions
2. To reduce the amount of long-term deflection
3. To support shear reinforcement (Stirrups)



Balanced steel ratio:

$$\varepsilon_s = \varepsilon_y$$

$$\varepsilon_c = \varepsilon_{cu} \quad \text{balance failure}$$

Let

$$\bar{\rho} = \frac{A_s}{bd}, \quad \rho' = \frac{A_s'}{bd}$$

$$\bar{\rho}_b = \frac{A_{s_b}}{bd} \quad \text{balance steel ratio}$$

$$\sum F_x = 0$$

$$A_{s_b} f_y = A_s' f_s' + 85 f_c' b a \quad \div b d f_y$$

$$\frac{As_b}{bd} = \frac{As'}{bd} * \frac{fs'}{fy} + 0.85 \frac{fc'}{fy} * \frac{a}{d}$$

$$\bar{\rho}_b = \rho' \frac{fs'}{fy} + 0.85 \frac{fc'}{fy} * \frac{a}{d} \dots \dots \dots (1)$$

From strain diagram $\frac{\epsilon_{cu}}{c_b} = \frac{\epsilon_{cu} + \epsilon_y}{d}$

$$c_b = \frac{\epsilon_{cu}}{\epsilon_{cu} + \epsilon_y} * d$$

$$a = \beta_1 c = \beta_1 * \frac{\epsilon_{cu}}{\epsilon_{cu} + \epsilon_y} d = \beta_1 * \frac{0.003}{0.003 + \frac{fy}{200000}} * d = \beta_1 * \frac{600}{600 + fy} * d \dots (2)$$

Sub eq. 2 into eq. 1

$$\bar{\rho}_b = \rho' \frac{f_s'}{f_y} + 0.85\beta_1 \frac{f_c'}{f_y} \frac{600}{600+f_y}$$

$$\bar{\rho}_b = \rho' * \frac{f_s'}{f_y} + \rho_b \quad \text{for } f_s' < f_y$$

$$\bar{\rho}_b = \rho' + \rho_b \quad \text{for } f_s' = f_y$$

fs' at balance condition:

$$\frac{\varepsilon_{cu} - \varepsilon'_s}{d'} = \frac{\varepsilon_{cu} + \varepsilon_y}{d}$$

$$\varepsilon'_s = \varepsilon_{cu} - \frac{d'}{d} (\varepsilon_{cu} + \varepsilon_y)$$

$$f_s' = f_y \quad \text{if } \varepsilon'_s \geq \varepsilon_y$$

$$f_s' < f_y \quad \text{if } \varepsilon'_s < \varepsilon_y$$

$$\therefore f_s' = E_s \varepsilon'_s = E_s \left[\varepsilon_{cu} - \frac{d'}{d} (\varepsilon_{cu} + \varepsilon_y) \right]$$

$$E_s = 200000 \text{ MPa} \quad , \quad \varepsilon_{cu} = 0.003$$

$$f_s' = 600 - \frac{d'}{d} (600 + f_y)$$

$$\frac{d'}{d} = \frac{600 - f_s'}{600 + f_y}$$

$$\text{If } \left[\begin{array}{l} \frac{d'}{d} > 0.2 \\ \frac{d'}{d} \leq 0.2 \end{array} \right. \left. \begin{array}{l} f_s' < f_y \\ f_s' = f_y \end{array} \right] \text{ for } f_y = 400 \text{ MPa}$$

$$\text{If } \left[\begin{array}{l} \frac{d'}{d} > 0.333 \\ \frac{d'}{d} \leq 0.333 \end{array} \right. \left. \begin{array}{l} f_s' < f_y \\ f_s' = f_y \end{array} \right] \text{ for } f_y = 300 \text{ MPa}$$

To find $\bar{\rho}_{\max}$, follow the same steps above for $\bar{\rho}_b$, but $\epsilon_s = 0.004$

$$f_s' = E_s \left[\epsilon_{cu} - \frac{d'}{d} (\epsilon_{cu} + 0.004) \right] \rightarrow f_s' = 600 - 1400 \frac{d'}{d} \leq f_y$$

$$\bar{\rho}_{\max} = 0.85 \beta_1 * \frac{f_c'}{f_y} * \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004} + \rho' \frac{f_s'}{f_y}$$

$$\bar{\rho}_{\max} = 0.364 \beta_1 \frac{f_c'}{f_y} + \rho' \frac{f_s'}{f_y}$$

Bending moment capacity of doubly reinforced rectangular section

$$M_u = \phi M_n$$

1. $f_s' = f_y$

$$M_u = \phi \left[0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' f_y (d - d') \right]$$

$$\sum F_x = 0$$

$$A_s f_y = A_s' f_y + 0.85 f_c' b a \quad \div b a f_y$$

$$a = (\bar{\rho} - \rho') \frac{f_y}{0.85 f_c'} * d$$

2. $f_s' < f_y$

$$M_u = \phi \left[0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s f_s' (d - d') \right]$$

$$\sum F_x = 0$$

$$A_s f_y = A_s f_s' + 0.85 f_c' b a \quad \div b d f_y$$

$$a = \left(\bar{\rho} - \rho' * \frac{f_s'}{f_y} \right) * \frac{f_y}{0.85 f_c'} * d \dots \dots \dots (1)$$

From strain diagram

$$\frac{\epsilon_{cu} - \epsilon_s'}{d'} = \frac{\epsilon_{cu}}{c}$$

$$c = \frac{\epsilon_{cu}}{\epsilon_{cu} - \epsilon_s'} * d' = \frac{600}{600 - f_s'} * d'$$

$$\therefore a = \beta_1 * c = \frac{600\beta_1}{600 - f_s'} * d' \dots \dots \dots (2)$$

$$Eq_1 = Eq_2$$

$$\left(\bar{\rho} - \rho' \frac{f_s'}{f_y} \right) * \frac{f_y}{0.85f_c'} * d = \frac{600\beta_1}{600 - f_s'} * d'$$

2nd order eq. to be solved for f_s' then find (a) from eq1 or eq2

Condition for yielding of compression reinforcement

For large $\bar{\rho}$, $\varepsilon'_s \geq \varepsilon_y \rightarrow fs' = fy$

For small $\bar{\rho}$, $\varepsilon'_s < \varepsilon_y \rightarrow fs' < fy$

For min. $\bar{\rho}$, $\varepsilon'_s = \varepsilon_y \rightarrow fs' = fy$

$\bar{\rho}_{min}$: The min. steel ratio required to insure yielding of
compression reinforcement

$$\sum Fx = 0$$

$$As'fy = Asfy + 0.85fc'ba \quad \div b d fy$$

$$\bar{\rho}_{min} = \rho' + 0.85 \frac{fc'}{fy} * \frac{a}{d}$$

From strain diagram

$$\frac{\varepsilon_{cu} - \varepsilon'_s}{d'} = \frac{\varepsilon_{cu}}{c} \quad \text{sub } \varepsilon'_s = \varepsilon_y$$

$$\frac{\varepsilon_{cu} - \varepsilon_y}{d'} = \frac{\varepsilon_{cu}}{c}$$

$$c = \frac{\varepsilon_{cu} \cdot d'}{\varepsilon_{cu} - \varepsilon_y} = \frac{600}{600 - f_y} * d'$$

$$\therefore a = \beta_1 c = \frac{600\beta_1}{600 - f_y} * d'$$

$$\bar{\rho}_{\min} = \rho' + 0.85\beta_1 \frac{f_c'}{f_y} * \frac{d'}{d} * \frac{600}{600 - f_y} \quad \text{for analysis problems}$$

IF $\bar{\rho} \geq \bar{\rho}_{\min} \rightarrow fs' = fy$ For moment equation

IF $\bar{\rho} < \bar{\rho}_{\min} \rightarrow fs' < fy$ For moment equation

For design problems set $\bar{\rho}_{\min} = \bar{\rho}_{\max}$ (to ensure that $fs' = fy$ for moment equation)

$$\rho' + 0.85\beta_1 \frac{fc'}{fy} * \frac{d'}{d} * \frac{600}{600-fy} = 0.85\beta_1 \frac{fc'}{fy} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004} + \rho' \frac{fs'}{fy} \rightarrow$$

$$\rightarrow \frac{d'}{d} = \frac{3}{4200} (600 - fy)$$

For $fy=400\text{MPa}$, if $\frac{d'}{d} \leq 0.143 \rightarrow fs' = fy$

For $fy=300\text{MPa}$, if $\frac{d'}{d} \leq 0.210 \rightarrow fs' = fy$

Reduction factor ϕ

To find $\bar{\rho}_t$, follow the same steps above, but $\varepsilon_s = 0.005$

$$\bar{\rho}_t = 0.85\beta_1 \frac{f_c'}{f_y} * \frac{\varepsilon_{cu}}{\varepsilon_{cu} + 0.005} + \rho' = \rho_t + \rho' \quad \text{For } f_s' = f_y$$

$$\text{If } \bar{\rho} \leq \bar{\rho}_t \rightarrow \varepsilon_s \geq 0.005 \rightarrow \phi = 0.9$$

$$\text{If } \bar{\rho} > \bar{\rho}_t \rightarrow \varepsilon_s < 0.005 \rightarrow \phi = 0.483 + 83.3\varepsilon_t$$

$$\bar{\rho}_t = 0.85 \beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005} + \bar{\rho} \frac{f_s'}{f_y} \quad \text{for } f_s' < f_y$$

$$\bar{\rho}_t = \rho_t + \bar{\rho} \frac{f_s'}{f_y} \quad \text{for } f_s' < f_y, \quad f_s' = E_s \left[\epsilon_{cu} - \frac{d'}{d} (\epsilon_{cu} + 0.005) \right] \rightarrow$$

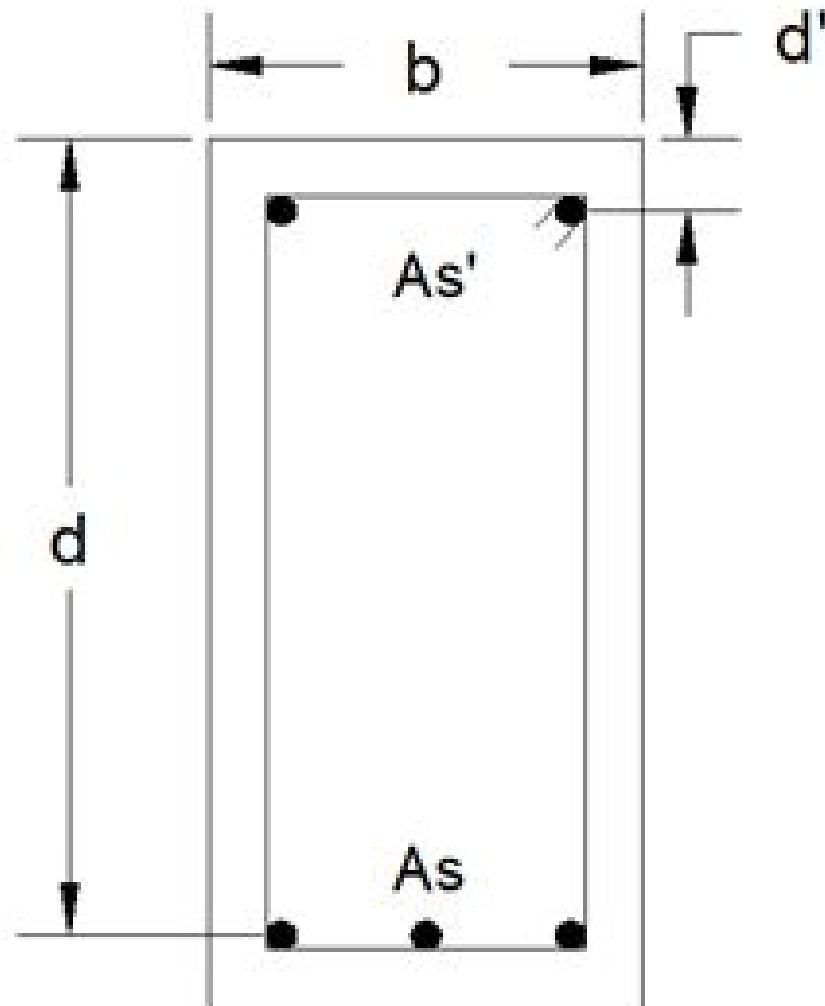
$$f_s' = 600 - 1600 \frac{d'}{d} \leq f_y$$

$$\text{if } \bar{\rho} \leq \rho_t \rightarrow \phi = 0.9$$

$$\text{if } \bar{\rho} > \rho_t \rightarrow \phi = 0.483 + 83.3 \epsilon_t$$

$$\epsilon_t = \epsilon_{cu} * \frac{dt - c}{c}$$

Summary



$$\bar{\rho} = \frac{As}{bd} \quad , \quad \rho' = \frac{As'}{bd}$$

1. Check

$$\rho_{\max} \quad \text{iF} \quad \left[\begin{array}{l} \bar{\rho} \leq \rho_{\max(\text{Single})} \\ \bar{\rho} > \rho_{\max(\text{Single})} \end{array} \right. \quad \begin{array}{l} \therefore \text{Singly reinforced section} \\ \therefore \text{Doubly reinforced section} \end{array} \quad \left. \vphantom{\rho_{\max}} \right]$$

2. Check $\bar{\rho} \leq \bar{\rho}_{\max} = 0.85\beta_1 \frac{fc'}{fy} \frac{\varepsilon_{cu}}{\varepsilon_{cu}+0.004} + \rho' \frac{fs'}{fy}$

$$fs' = 600 - 1400 \frac{d'}{d} \leq fy \quad \text{for } \bar{\rho}_{\max} \text{ equation}$$

3. Check $\bar{\rho}_{\min} = 0.85\beta_1 \frac{fc' d'}{fy d} \frac{600}{600-fy} + \rho'$

a. If $\bar{\rho} \geq \bar{\rho}_{\min} \rightarrow fs' = fy$

$$Mu = \phi \left[0.85 fc' ba \left(d - \frac{a}{2} \right) + As' fy (d - d') \right]$$

$$a = (\bar{\rho} - \rho') \frac{fy}{0.85 fc'} * d \rightarrow a = (As - As') \frac{fy}{0.85 fc' b}$$

If $\bar{\rho} \leq \bar{\rho}_t = 0.85\beta_1 \frac{fc'}{fy} * \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005} + \rho' \rightarrow \phi = 0.9$

If $\bar{\rho} > \bar{\rho}_t \rightarrow \phi = 0.483 + 83.3\epsilon_t$

b. If $\bar{\rho} < \bar{\rho}_{\min} \rightarrow fs' < fy$

$$Mu = \phi \left[0.85fc'ba \left(d - \frac{a}{2} \right) + As fs' (d - d') \right]$$

$$\left[\begin{array}{l} a = \left(\bar{\rho} - \rho' \frac{fs'}{fy} \right) \frac{fy}{0.85 fc'} d \dots \dots \dots (1) \\ a = \frac{600\beta_1}{600 - fs'} d' \dots \dots \dots (2) \end{array} \right] \text{ solve for } fs' \text{ and } a$$

$$\text{If } \bar{\rho} \leq \bar{\rho}_t = 0.85\beta_1 \frac{fc'}{fy} * \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005} + \rho' \frac{fs'}{fy} \rightarrow \phi = 0.9$$

$$fs' = 600 - 1600 \frac{d'}{d} \leq fy$$

$$\text{If } \bar{\rho} > \bar{\rho}_t \rightarrow \phi = 0.483 + 83.3\varepsilon_t$$

$$\varepsilon_t = \varepsilon_{cu} \frac{dt - c}{c}$$

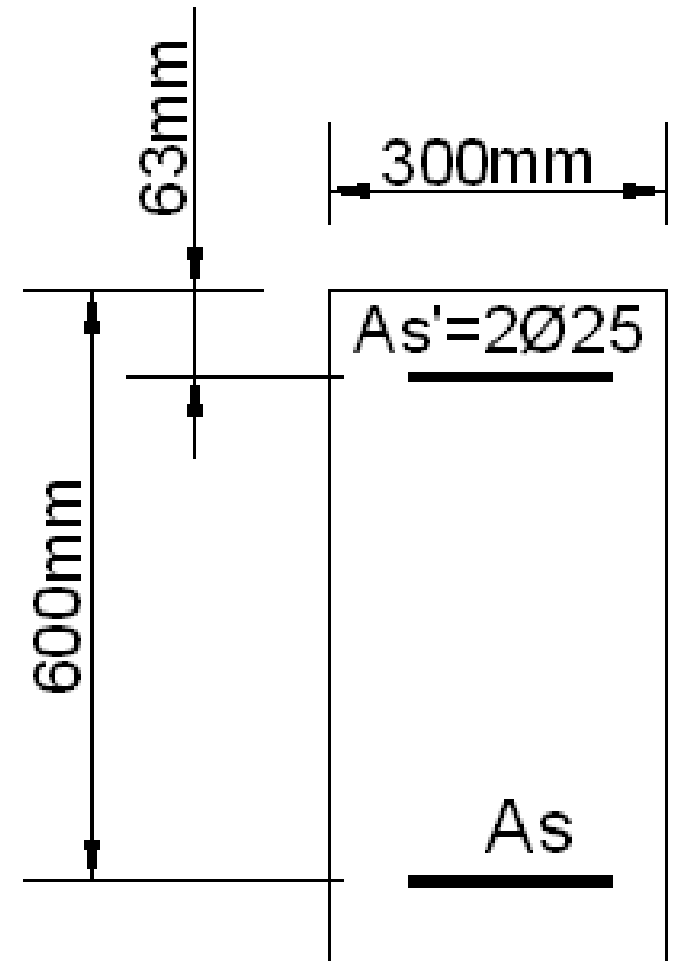
Ex1: $\frac{S}{c} = \frac{414}{35} MPa$, find M_u , if

1. $3\text{Ø}32$, $A_s=2413\text{mm}^2$
2. $6\text{Ø}32$, $A_s=4826\text{mm}^2$
3. $5\text{Ø}32 + 1\text{Ø}25$, $A_s=4513\text{mm}^2$

Solution:

$$A_s' = 2\text{Ø}25 = 982\text{mm}^2, \rightarrow \rho' = \frac{A_s'}{bd} =$$

$$\frac{982}{300 \cdot 600} = 0.0055$$



1 – 3Ø32,

$$\mathbf{As} = 2413\text{mm}^2 \rightarrow \bar{\rho} = \frac{As}{bd} = \frac{2413}{300 * 600} = 0.0134$$

$$\rho_{max} = 0.85\beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004}$$

for $f_c' = 35\text{MPa} > 28$,

$$\begin{aligned} \beta_1 &= 0.85 - 0.05 * \frac{f_c' - 28}{7} = 0.85 - 0.05 * \frac{35 - 28}{7} \\ &= 0.80 \end{aligned}$$

$$\rho_{max} = 0.85 * 0.8 * \frac{35}{400} \frac{0.003}{0.003 + 0.004} = 0.0246$$

$$\bar{\rho} = 0.0134 < \rho_{max} = 0.0246 \rightarrow \textit{singly R.S}$$

ρ_{min}

$$= \max \left(\frac{1.4}{f_y} = \frac{1.4}{414} = 0.0034, \frac{\sqrt{f_c'}}{4f_y} = \frac{\sqrt{35}}{4 * 414} = 0.0036 \right)$$

$$= 0.0036 < \bar{\rho} = 0.0134 \text{ O.K}$$

$$Mu = \phi \rho b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f_c'} \right)$$

$$\rho_t = 0.85 \beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005}$$

$$= 0.85 * 0.80 * \frac{35}{414} \frac{0.003}{0.003 + 0.005} = 0.0215$$

$$\bar{\rho} = 0.0134 < \rho_t = 0.0215 \rightarrow \phi = 0.9$$

$$Mu = 0.9 * 0.0134 * 0.3 * 0.6^2 * 414 * \left(1 - 0.59 * 0.0134 * \frac{414}{35}\right) = 0.489MN.m$$

$$2 - 6\text{Ø}32, A_s = 4826\text{mm}^2 \rightarrow \bar{\rho} = \frac{A_s}{bd} = \frac{4826}{300*600} = 0.0268$$

$$\bar{\rho} = 0.0268 > \rho_{max} = 0.0246 \rightarrow \text{doubly R.S}$$

$$\bar{\rho}_{max} = 0.85\beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004} + \rho' \frac{f_s'}{f_y}$$

$$f_s' = 600 - 1400 \frac{d'}{d} = 600 - 1400 * \frac{63}{600} = 453\text{MPa} > f_y \rightarrow$$

$$f_s' = 414\text{MPa}$$

$$\bar{\rho}_{max} = 0.85 * 0.8 * \frac{35}{414} * \frac{0.003}{0.003 + 0.004} + 0.0055 * \frac{414}{414} = 0.0301$$

$$\bar{\rho} = 0.0268 < \bar{\rho}_{max} = 0.0301 \text{ O.K}$$

$$\bar{\rho}_{\min} = 0.85\beta_1 \frac{f_c' d'}{f_y d} \frac{600}{600 - f_y} + \rho'$$

$$\bar{\rho}_{\min} = 0.85 * 0.8 * \frac{35}{414} * \frac{63}{600} * \frac{600}{600 - 414} + 0.0055 = 0.025$$

$$\bar{\rho} = 0.0268 > \bar{\rho}_{\min} = 0.025 \rightarrow f_s' = f_y \text{ for moment equation}$$

$$\bar{\rho} = 0.0268 < \bar{\rho}_t = 0.85\beta_1 \frac{f_c'}{f_y} * \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005} + \rho' = \rho_t + \rho' = 0.0215 + 0.0055 = 0.027 \rightarrow \phi = 0.9$$

$$\sum f_x = 0$$

$$A_s f_y = 0.85 f_c' b a + A_s' f_y \rightarrow [A_s - A_s'] f_y = 0.85 f_c' b a$$

$$a = \frac{(4826 - 982) * 10^{-6} * 414}{0.85 * 35 * 0.3} = 0.178m$$

$$c = \frac{a}{\beta_1} = \frac{178}{0.8} = 222mm$$

$$M_u = \phi [0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' f_s' (d - d')]$$

$$\begin{aligned}
 Mu &= 0.9 \left[0.85 * 35 * 0.3 * 0.178 \left(0.6 - \frac{0.178}{2} \right) + \right. \\
 &\quad \left. 928 * 10^{-6} * 414(0.6 - 0.063) \right] \\
 &= 0.927 \text{ MN.m}
 \end{aligned}$$

$$\begin{aligned}
 \text{for check: } \frac{\epsilon_{s'}}{c - d'} &= \frac{\epsilon_{cu}}{c} \rightarrow \frac{\epsilon_{s'}}{222 - 63} = \frac{0.003}{222} \rightarrow \epsilon_{s'} \\
 &= 0.00215 \rightarrow f_{s'} = E_s * \epsilon_{s'} = 200000 * 0.00215 \\
 &= 430 \text{ MPa} > f_y \rightarrow f_{s'} = 414 \text{ MPa for moment eq.}
 \end{aligned}$$

$$3 - 5\text{Ø}32 + 1\text{Ø}25, \quad A_s = 4513\text{mm}^2 \rightarrow$$

$$\bar{\rho} = \frac{A_s}{bd} = \frac{4513}{300 \times 600} = 0.025$$

$$\bar{\rho} = 0.025 > \rho_{max} = 0.0246 \rightarrow \text{doubly R.S}$$

$$\bar{\rho} = 0.025 < \bar{\rho}_{max} = 0.0301 \text{ O.K}$$

$$\bar{\rho} = 0.025 < \bar{\rho}_{min} = 0.025 \rightarrow f_s' < f_y$$

$$a = \left(\bar{\rho} - \rho' \frac{f_s'}{f_y} \right) \frac{f_y}{0.85 f_c'} d \dots \dots \dots (1)$$

$$a = \left(0.025 - 0.0055 * \frac{f_s'}{414} \right) \frac{414}{0.85 * 35} * 0.6 \dots \dots \dots (1)$$

$$a = \frac{600\beta_1}{600 - f_s'} d' \dots \dots \dots (2)$$

$$a = \frac{600 * 0.80}{600 - f_s'} * 0.063 \dots \dots \dots (2)$$

$$0.0055(f_s')^2 - 13.65f_s' + 4690.62 = 0 \quad \text{solve for } f_s'$$

$$f_s' = 412 \text{ MPa} < f_y$$

$$a = 0.163 \text{ m}$$

$$\bar{\rho}_t = 0.85\beta_1 \frac{f_c'}{f_y} * \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005} + \rho' \frac{f_s'}{f_y}$$

$$f_s' = 600 - 1600 \frac{d'}{d} = 600 - 1600 \frac{63}{600} = 432 \text{MPa} > f_y \rightarrow f_s' \\ = 414 \text{MPa}$$

$$\bar{\rho}_t = 0.85 * 0.8 * \frac{35}{414} * \frac{0.003}{0.003 + 0.005} + 0.0055 * \frac{414}{414} \\ = 0.0271$$

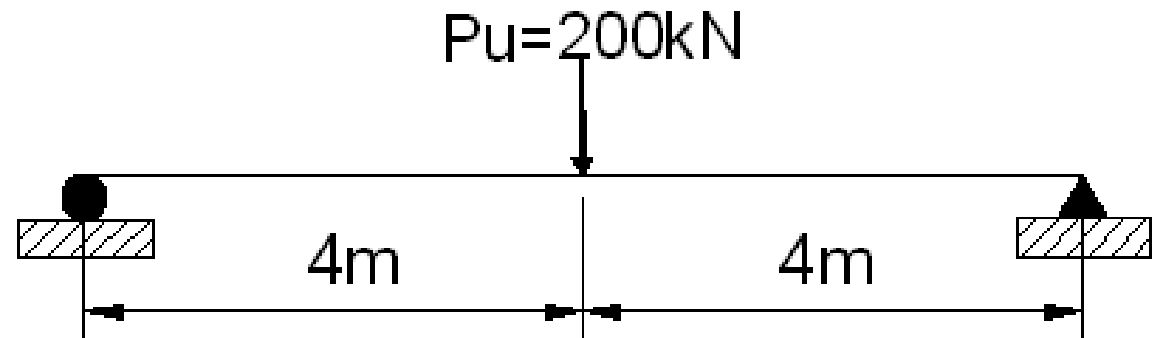
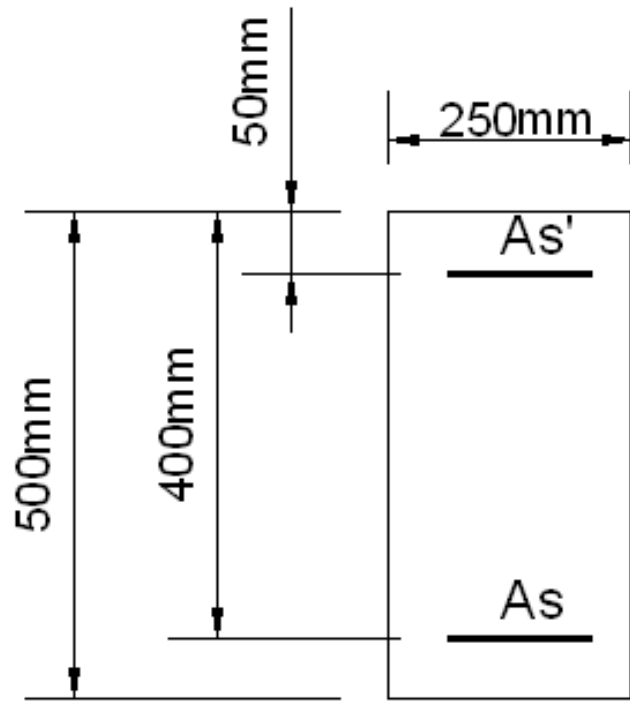
$$\bar{\rho} = 0.025 < \bar{\rho}_t = 0.0271 \rightarrow \phi = 0.9$$

$$Mu = \phi \left[0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' f_s' (d - d') \right]$$

Mu

$$= 0.9 \left[0.85 * 35 * 0.3 * 0.163 \left(0.6 - \frac{0.163}{2} \right) + 928 * 10^{-6} * 412 * (0.6 - 0.063) \right] = 0.874 MN.m$$

Ex2: $\frac{s}{c} = \frac{400}{30}$ MPa , factored load $P_u=200$ kN, ignore beam wt., Design beam for flexure.



$$\text{Solution: } Mu_{ext} = \frac{Pu.l}{4} = \frac{200*8}{4} = 400 \text{ kN.m}$$

Let $\phi=0.9$

$$Mu = \phi \rho b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f_c'}\right)$$

$$0.4 = 0.9 * \rho * 0.25 * 0.4^2 * 400 \left(1 - 0.59 \rho * \frac{400}{30}\right)$$

$$\rho = \begin{pmatrix} 0.041 \\ 0.086 \end{pmatrix} \text{ choose min. positive value, } \rho = 0.041$$

$$\rho_{max} = 0.85 \beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004}$$

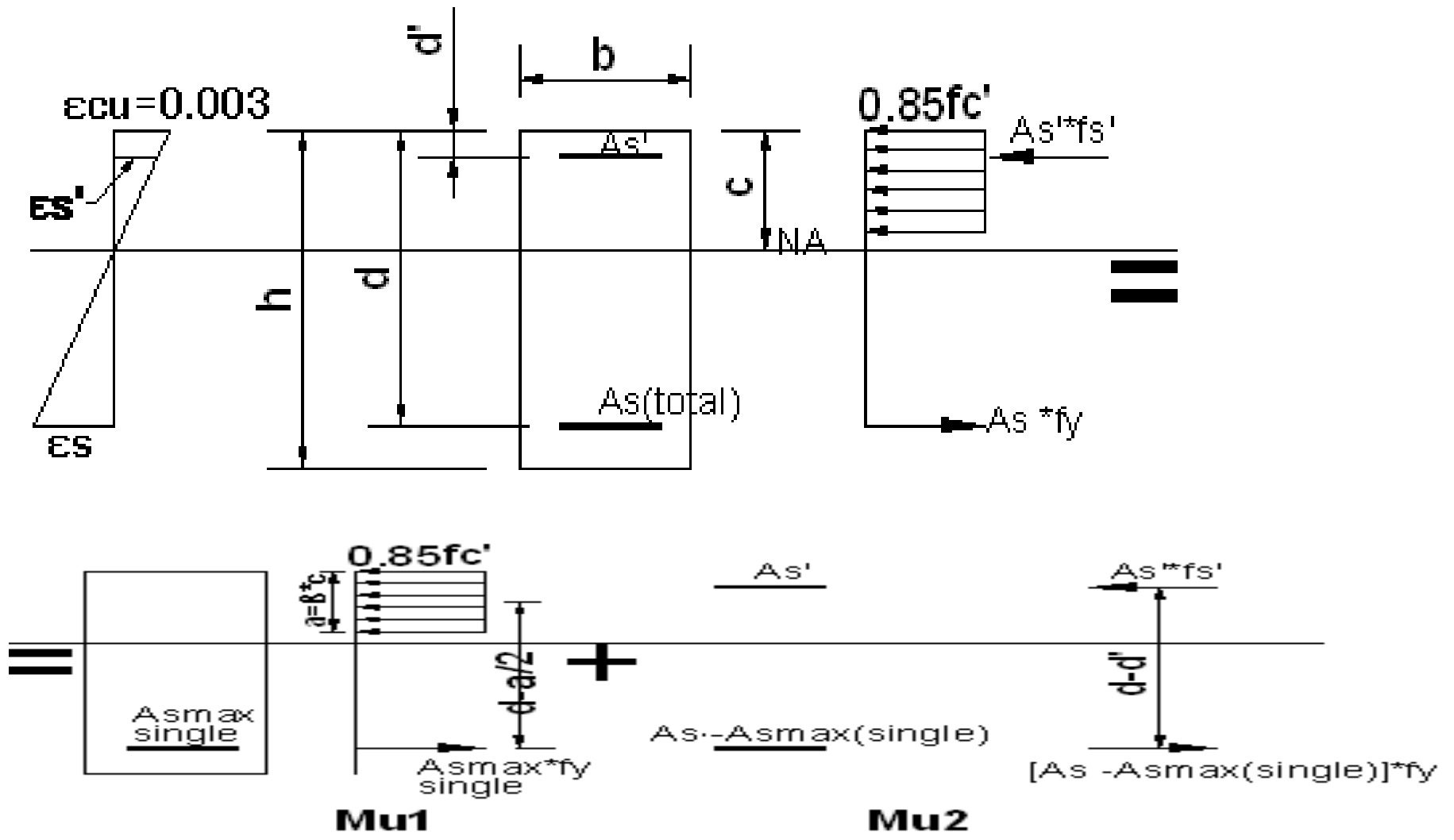
for $f_c' = 30\text{MPa} > 28$,

$$\beta_1 = 0.85 - 0.05 * \frac{f_c' - 28}{7} = 0.85 - 0.05 * \frac{30 - 28}{7}$$

$$= 0.83$$

$$\rho_{max} = 0.85 * 0.83 * \frac{30}{400} \frac{0.003}{0.003 + 0.004} = 0.0227$$

$$\rho = 0.041 > \rho_{max} = 0.0227 \rightarrow \text{doubly RCS}$$



$$\text{for } \rho = \rho_{max}, \rightarrow \varepsilon_t = 0.004, \rightarrow \phi = 0.483 + 83.3 * 0.004 \\ = 0.816$$

$$Mu_1 = \phi \rho_{max} b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f_c'}\right)$$

$$Mu_1 \\ = 0.816 * 0.0227 * 0.25 * 0.4^2 \\ * 400 \left(1 - 0.59 * 0.0227 * \frac{400}{30}\right) = 0.243 MN.m$$

$$Mu_{total} = Mu_1 + Mu_2$$

$$400 = 243 + Mu_2$$

$$Mu_2 = 157 \text{ kN.m}$$

Let $f_s' = f_y$ to be checked later

$$\text{OR} \quad \frac{d'}{d} = \frac{50}{400} = 0.125 < 0.143 \rightarrow \therefore f_s' = f_y$$

$$Mu_2 = \phi A_s' f_s' (d - d')$$

$$0.157 = 0.816 * A_s' * 400 (0.4 - 0.05)$$

$$A_s' = 1.37 * 10^{-3} \text{ m}^2 = 1370 \text{ mm}^2 \rightarrow \rho' = \frac{A_s'}{bd} = \frac{1370}{250 * 400} = 0.0137$$

$$\text{Total tension reinforcement}(A_s) = \rho_{max} bd + A_s' \frac{f_s'}{f_s}$$

$$A_s = 0.0227 * 250 * 400 + 1370 * \frac{400}{400} = 3640 \text{mm}^2$$

$$\bar{\rho} = \frac{A_s}{bd} = \frac{3640}{250 * 400} = 0.0364$$

$$\bar{\rho}_{\min} = 0.85\beta_1 \frac{f_c' d'}{f_y d} \frac{600}{600 - f_y} + \rho'$$

$$\begin{aligned} \bar{\rho}_{\min} &= 0.85 * 0.83 * \frac{30}{400} * \frac{50}{400} * \frac{600}{600 - 400} + 0.0133 \\ &= 0.03354 \end{aligned}$$

$$\bar{\rho}=0.0364$$

> $\bar{\rho}_{\min}=0.03354 \rightarrow$ The previous assumption is valid, $f_s'=f_y$ O.K

$$\bar{\rho}_{\max}=0.85\beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004} + \rho' \frac{f_s'}{f_y}$$

$$f_s' = 600 - 1400 \frac{d'}{d} = 600 - 1400 * \frac{50}{400} = 425 \text{MPa} > f_y$$

$$\rightarrow f_s' = 400 \text{MPa}$$

$$\bar{\rho}_{\max}=0.85*0.83* \frac{30}{400} * \frac{0.003}{0.003 + 0.004} + 0.0137 * \frac{400}{400}$$

$$= 0.03637$$

$$\rho = 0.0364 < \bar{\rho}_{\max} = 0.03637 \text{ O.K}$$

Use $2\text{Ø}36 + 3\text{Ø}28 = 3883 \text{mm}^2$ tension Reinf.

Use $3\text{Ø}28 = 1847 \text{mm}^2$ comp. Reinf.

Check reduction factor $\phi = 0.816$

$$A_{s \text{ single provided}} = A_{st} - A_{s'} * (f_{s'} / f_y)$$

$$= 3883 - 1847 * (400 / 400) = 2036 \text{ mm}^2$$

$$\sum f_x = 0$$

$$A_{s \text{ single}} f_y = 0.85 f_c' b a$$

$$a = \frac{2036 * 10^{-6} * 400}{0.85 * 30 * 0.25} = 0.128m$$

$$c = \frac{a}{\beta_1} = \frac{128}{0.83} = 154mm$$

$$\frac{\epsilon t}{d - c} = \frac{\epsilon_{cu}}{c} \rightarrow \frac{\epsilon t}{400 - 154} = \frac{0.003}{154} \rightarrow \epsilon t = 0.0048 \rightarrow \therefore \phi$$

$$= 0.483 + 83.3 * 0.0048 = 0.88 > 0.816 \text{ O.K}$$

$$Mu = \phi(Mu_1 + Mu_2)$$

$$Mu = \phi \left[0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' f_s' (d - d') \right]$$

$$\frac{\varepsilon_{s'}}{c - d'} = \frac{\varepsilon_{cu}}{c} \rightarrow \frac{\varepsilon_{s'}}{154 - 50} = \frac{0.003}{154} \rightarrow \varepsilon_{s'} = 0.002 \rightarrow f_{s'}$$

$$= E_s * \varepsilon_{s'} = 200000 * 0.002 = 400 \text{ MPa}$$

Mu

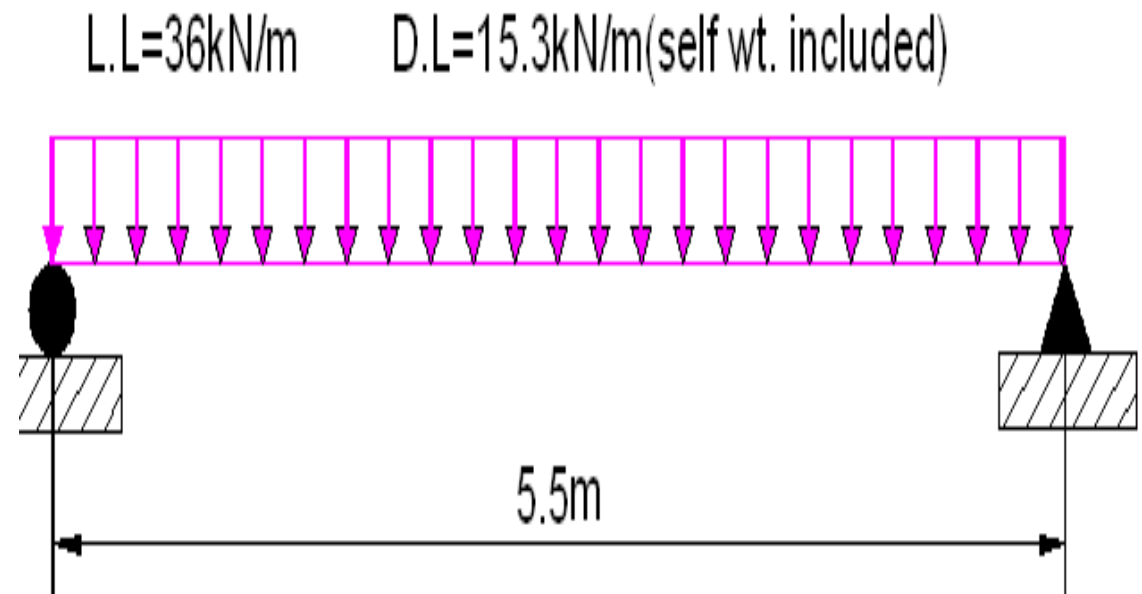
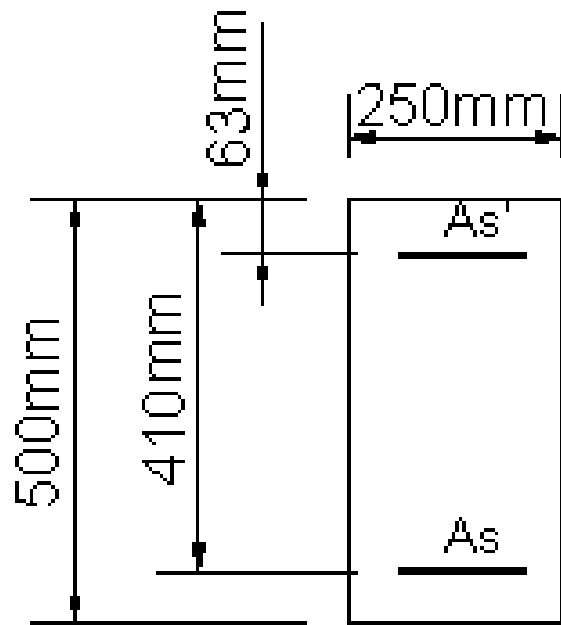
$$= 0.88 \left[0.85 * 30 * 0.25 * 0.128 \left(0.4 - \frac{0.128}{2} \right) + 1847 * 10^{-6} * 400(0.4 - 0.05) \right] = 0.469 \text{ MN.m}$$

> Muext = 0.400 MN.m

∴ no further reinforcement is necessary

Ex3: $\frac{S}{C} = \frac{414}{28} MPa$, service load (L.L=36 kN/m,

D.L=15.3kN/m(self wt included)). Design beam for flexure.



Solution:

$$W_u = 1.2 * 15.3 + 1.6 * 36 = 76 \text{ kN/m}$$

$$M_{u_{ext}} = \frac{W_u l^2}{8} = \frac{76 * 5.5^2}{8} = 287 \text{ kN.m}$$

$$M_u = \phi M_n$$

$$M_u = \phi \rho b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f_c'}\right)$$

$$0.287 = 0.9 * \rho * 0.25 * 0.41^2 * 414 \left(1 - 0.59 * \rho * \frac{414}{28}\right)$$

$$130\rho^2 - 14.9\rho + 0.287 = 0 \rightarrow \rho = 0.0245$$

$$\rho_{max} = 0.85\beta_1 \frac{f_c'}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004}$$

for $f_c' = 28\text{MPa} \leq 28\text{MPa}$, $\beta_1 = 0.85$

$$\rho_{max} = 0.85 * 0.85 * \frac{28}{414} \frac{0.003}{0.003 + 0.004} = 0.0209$$

$\rho = 0.0245 > \rho_{max} = 0.0209 \rightarrow$ doubly RCS

$$\rho_t = 0.85 * 0.85 * \frac{28}{414} * \frac{0.003}{0.003+0.005} = 0.0183$$

Let $\rho = \rho_t = 0.0183$ (slightly from ρ_{max}) $\rightarrow \phi = 0.9$

$$Mu_1$$

$$= 0.9 * 0.0183 * 0.25 * 0.41^2$$

$$* 414 \left(1 - 0.59 * 0.0183 * \frac{414}{28} \right) = 0.241 MN.m$$

$$Mu_{total} = Mu_1 + Mu_2$$

$$287 = 241 + Mu_2 \rightarrow Mu_2 = 46 kN.m$$

$$\frac{d'}{d} = \frac{63}{410} = 0.153 > 0.143 \rightarrow fs' < fy$$

$$A_{S_{single}} fy = 0.85fc' ba$$

$$\rho_t b d f_y = 0.85 f_c' b a$$

$$a = \frac{0.0183 * 0.41 * 414}{0.85 * 28} = 0.13m$$

$$c = \frac{a}{\beta_1} = \frac{130}{0.85} = 153mm$$

$$\frac{\epsilon_s'}{c - d'} = \frac{\epsilon_{cu}}{c} \rightarrow \frac{\epsilon_s'}{153 - 63} = \frac{0.003}{153} \rightarrow \epsilon_s' = 0.00176 \rightarrow f_s'$$

$$= E_s * \epsilon_s' = 200000 * 0.00176 = 352MPa$$

$$M_u = \phi A_s' f_s' (d - d') \rightarrow 0.046 = 0.9 * A_s' * 352 (0.41 - 0.063) \rightarrow$$

$$A_s' = 4.18 * 10^{-6} m^2 = 418mm^2$$

$$A_s = \rho_t b d + A_{s'} * \left(\frac{f_{s'}}{f_y} \right)$$

$$= 0.0183 * 250 * 410 + 418 * \left(\frac{352}{414} \right) = 2231 \text{ mm}^2$$

Use 4Ø28 (2463 mm²), tension reinforcement

Use 2Ø20 (628 mm²), compression reinforcement

$$\sum F_x = 0 \rightarrow (A_s - A_{s'} * \frac{f_{s'}}{f_y}) f_y = 0.85 f_c' b a \rightarrow a$$

$$= \frac{\left(2463 - 628 * \frac{352}{414} \right) * 10^{-6} * 414}{0.85 * 28 * 0.25} = 0.134 \text{ m}$$

$$c = \frac{a}{\beta_1} = \frac{134}{0.85} = 158\text{mm}$$

$$\frac{\varepsilon_t}{d - c} = \frac{\varepsilon_{cu}}{c} \rightarrow \frac{\varepsilon_t}{410 - 158} = \frac{0.003}{158} \rightarrow \varepsilon_t = 0.00478 < 0.005$$

$$\rightarrow \phi = 0.483 + 83.3 * 0.00478 = 0.881 < 0.9$$

$$Mu = \phi \left[0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' f_s' (d - d') \right]$$

$$\frac{\varepsilon_{s'}}{c - d'} = \frac{\varepsilon_{cu}}{c} \rightarrow \frac{\varepsilon_{s'}}{158 - 63} = \frac{0.003}{158} \rightarrow \varepsilon_{s'} = 0.0018 \rightarrow$$

$$f_s' = E_s * \varepsilon_{s'} = 200000 * 0.0018 = 361\text{MPa}$$

M_u

$$= 0.881 \left[0.85 * 28 * 0.25 * 0.134 \left(0.41 - \frac{0.134}{2} \right) + 628 * 10^{-6} * 361(0.41 - 0.063) \right] = 0.310 MN.m$$

$> M_{uext} = 0.287 MN.m$

\therefore *no further reinforcement is necessary*