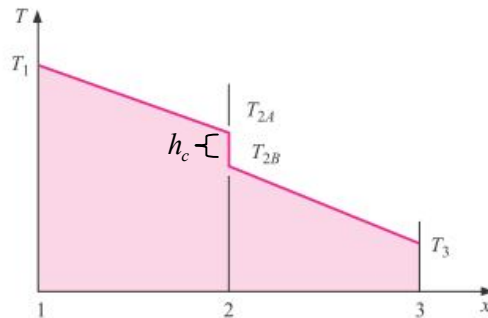
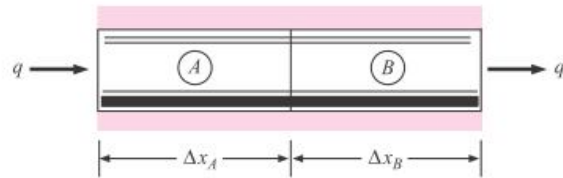


Thermal Contact Resistance



The temperature drop at plane 2, the contact plane between the two materials, is said to be the result of a *thermal contact resistance*. Performing an energy balance on the two materials, we obtain

$$q = k_A A \frac{T_1 - T_{2A}}{\Delta x_A} = \frac{T_{2A} - T_{2B}}{1/h_c A} = k_B A \frac{T_{2B} - T_3}{\Delta x_B}$$

or

$$q = \frac{T_1 - T_3}{\Delta x_A/k_A A + 1/h_c A + \Delta x_B/k_B A}$$

$$q_{\text{interface}} = h_c A (T_{2A} - T_{2B})$$

Where $1/h_c A$ is called the thermal contact resistance (R_c).
 h_c is called the contact coefficient.

Let the contact area by A_c and the void area by A_v , then

$$q = \frac{T_{2A} - T_{2B}}{L_g/2k_A A_c + L_g/2k_B A_c} + k_f A_v \frac{T_{2A} - T_{2B}}{L_g} = \frac{T_{2A} - T_{2B}}{1/h_c A}$$

Where L_g is the thickness of the void space and k_f is the thermal conductivity of the fluid which fills the void space. The total cross-sectional area of the bars is A . Solving for h_c , the contact coefficient, we obtain

$$h_c = \frac{1}{L_g} \left(\frac{A_c}{A} \frac{2k_A k_B}{k_A + k_B} + \frac{A_v}{A} k_f \right)$$

Influence of Contact Conductance on Heat Transfer

EXAMPLE 2-12

Two 3.0-cm-diameter 304 stainless-steel bars, 10 cm long, have ground surfaces and are exposed to air with a surface roughness of about $1 \mu\text{m}$. If the surfaces are pressed together with a pressure of 50 atm and the two-bar combination is exposed to an overall temperature difference of 100°C , calculate the axial heat flow and temperature drop across the contact surface.

$$1/h_c = 5.28 \times 10^{-4} \text{ m}^2 \cdot \text{C}^\circ/\text{W}$$

■ Solution

The overall heat flow is subject to three thermal resistances, one conduction resistance for each bar, and the contact resistance. For the bars

$$R_{\text{th}} = \frac{\Delta x}{kA} = \frac{(0.1)(4)}{(16.3)\pi(3 \times 10^{-2})^2} = 8.679^\circ\text{C}/\text{W}$$

$$R_c = \frac{1}{h_c A} = \frac{(5.28 \times 10^{-4})(4)}{\pi(3 \times 10^{-2})^2} = 0.747^\circ\text{C}/\text{W}$$

The total thermal resistance is therefore

$$\sum R_{\text{th}} = (2)(8.679) + 0.747 = 18.105$$

and the overall heat flow is

$$q = \frac{\Delta T}{\sum R_{\text{th}}} = \frac{100}{18.105} = 5.52 \text{ W} \quad [18.83 \text{ Btu/h}]$$

The temperature drop across the contact is found by taking the ratio of the contact resistance to the total thermal resistance:

$$\Delta T_c = \frac{R_c}{\sum R_{\text{th}}} \Delta T = \frac{(0.747)(100)}{18.105} = 4.13^\circ\text{C} \quad [39.43^\circ\text{F}]$$

In this problem the contact resistance represents about 4 percent of the total resistance.

Unsteady State Conduction

Unsteady-state heat-transfer processes (heating or cooling) takes place in the interim period before equilibrium is established. To analyze a transient heat-transfer problem, we can proceed by solving the general heat-conduction equation, which is

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial \tau}$$

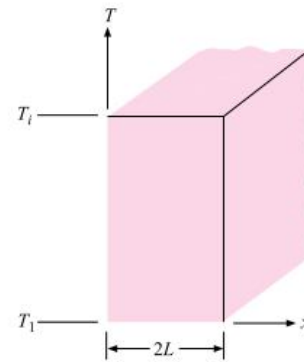
Consider the infinite plate of thickness $2L$ shown in Figure below. Initially the plate is at a uniform temperature T_i , and at time zero the surfaces are suddenly lowered to $T = T_l$. For one-dimension unsteady-state without heat generation, the differential equation is

$$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{\partial T}{\partial \tau}$$

Put $\theta = T - T_l$
($T = \text{any temp.}$), then

$$\frac{\partial^2 \theta}{\partial x^2} = \frac{1}{\alpha} \frac{\partial \theta}{\partial \tau}$$

Figure 4-1 | Infinite plate subjected to sudden cooling of surfaces.



Types of boundary conditions

- 1- Constant wall temperature (variable heat flux).
- 2- Constant heat flux (variable wall temperature).
- 3- Convection boundary conditions.

The initial and boundary conditions for infinite plate (constant wall temperature) will be

$$\text{I.C} \quad t = 0 \quad 0 \leq x \leq 2L \quad \theta = \theta_i = T_i - T_l$$

$$\text{B.C.1} \quad x = 0 \quad T = T_l \quad \theta = 0 \quad t > 0$$

$$\text{B.C.2} \quad x = 2L \quad T = T_l \quad \theta = 0 \quad t > 0$$

The final solution is therefore

$$\frac{\theta}{\theta_i} = \frac{T - T_l}{T_i - T_l} = \frac{4}{\pi} \sum_{n=1}^{\infty} \frac{1}{n} e^{-[n\pi/2L]^2 \alpha \tau} \sin \frac{n\pi x}{2L} \quad n = 1, 3, 5 \dots$$

$$\alpha = \frac{k}{\rho c p}$$