# Multilayer Conduction

# **EXAMPLE 2-1**

An exterior wall of a house may be approximated by a 4-in layer of common brick  $[k = 0.7 \text{ W/m} \cdot ^{\circ}\text{C}]$  followed by a 1.5-in layer of gypsum plaster  $[k = 0.48 \text{ W/m} \cdot ^{\circ}\text{C}]$ . What thickness of loosely packed rock-wool insulation  $[k = 0.065 \text{ W/m} \cdot ^{\circ}\text{C}]$  should be added to reduce the heat loss (or gain) through the wall by 80 percent?

### ■ Solution

The overall heat loss will be given by

$$q = \frac{\Delta T}{\sum R_{\text{th}}}$$

Because the heat loss with the rock-wool insulation will be only 20 percent (80 percent reduction) of that before insulation

$$\frac{q \text{ with insulation}}{q \text{ without insulation}} = 0.2 = \frac{\sum R_{\text{th}} \text{ without insulation}}{\sum R_{\text{th}} \text{ with insulation}}$$

We have for the brick and plaster, for unit area,

$$R_b = \frac{\Delta x}{k} = \frac{(4)(0.0254)}{0.7} = 0.145 \text{ m}^2 \cdot ^{\circ}\text{C/W}$$
  
 $R_p = \frac{\Delta x}{k} = \frac{(1.5)(0.0254)}{0.48} = 0.079 \text{ m}^2 \cdot ^{\circ}\text{C/W}$ 

so that the thermal resistance without insulation is

$$R = 0.145 + 0.079 = 0.224 \text{ m}^2 \cdot ^{\circ}\text{C/W}$$

Then

R with insulation = 
$$\frac{0.224}{0.2}$$
 = 1.122 m<sup>2</sup> · °C/W

and this represents the sum of our previous value and the resistance for the rock wool

$$1.122 = 0.224 + R_{rw}$$

$$R_{rw} = 0.898 = \frac{\Delta x}{k} = \frac{\Delta x}{0.065}$$

so that

$$\Delta x_{rw} = 0.0584 \text{ m} = 2.30 \text{ in}$$

## **EXAMPLE 2-2**

# Multilayer Cylindrical System

A thick-walled tube of stainless steel [18% Cr, 8% Ni, k = 19 W/m·°C] with 2-cm inner diameter (ID) and 4-cm outer diameter (OD) is covered with a 3-cm layer of asbestos insulation [k = 0.2 W/m·°C]. If the inside wall temperature of the pipe is maintained at 600°C, calculate the heat loss per meter of length. Also calculate the tube–insulation interface temperature.

# Figure Example 2-2 $T_1 = 600^{\circ}\text{C}$ Stainless steel $T_2 = 100^{\circ}\text{C}$ $T_2 = 100^{\circ}\text{C}$ $\frac{\ln (r_2/r_1)}{2\pi k_z L}$ $\frac{\ln (r_3/r_2)}{2\pi k_a L}$

### ■ Solution

Figure Example 2-2 shows the thermal network for this problem. The heat flow is given by

$$\frac{q}{L} = \frac{2\pi (T_1 - T_2)}{\ln (r_2/r_1)/k_s + \ln(r_3/r_2)/k_a} = \frac{2\pi (600 - 100)}{(\ln 2)/19 + (\ln \frac{5}{2})/0.2} = 680 \text{ W/m}$$

This heat flow may be used to calculate the interface temperature between the outside tube wall and the insulation. We have

$$\frac{q}{L} = \frac{T_a - T_2}{\ln{(r_3/r_2)/2\pi k_a}} = 680 \text{ W/m}$$

where  $T_a$  is the interface temperature, which may be obtained as

$$T_a = 595.8^{\circ} \text{C}$$

The largest thermal resistance clearly results from the insulation, and thus the major portion of the temperature drop is through that material.

# **Convection Boundary Conditions**

The heat transfer by convection can be calculated as:

$$q_{\text{conv}} = hA (T_w - T_\infty)$$

An electric-resistance analogy can also be drawn for the convection process by

$$q_{\rm conv} = \frac{T_w - T_\infty}{1/hA}$$

Where 1/hA becomes the convection thermal resistance.