



Refrigeration and Air conditioning Engineering.

3rd year – refrigeration and Air conditioning Course

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Duct design

Lecture -7-

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Duct Design Methods

Duct design methods for HVAC systems and for exhaust systems conveying vapors, gases, and smoke are the :

1- equal friction method

2-the static regain method

3- T-method.

The section on Industrial Exhaust System Duct Design presents the design criteria and procedures for exhaust systems conveying particulates.

Equal friction and static regain are non - optimizing methods, while the T-method is a practical optimization method. To ensure that system designs are acoustically acceptable, noise generation should be analyzed and sound attenuators and/or acoustically lined duct provided where necessary. Dampers must be installed throughout systems designed by equal friction, static regain, and the T-method because inaccuracies are introduced into these design methods by duct size round-off and the effect of close coupled fittings on the total pressure loss calculations.

Equal Friction Method

In the equal friction method, ducts are sized for a constant pressure loss per unit length. The shaded area of the friction chart is the suggested range of friction rate and air velocity.

When energy cost is high and installed ductwork cost is low, a low friction rate design is more economical. For low energy cost and high duct cost, a higher friction rate is more economical.

After initial sizing, calculate the total pressure loss for all duct sections, and then resize sections to balance pressure losses at each junction.

The objective of the static regain method is to obtain the same static pressure at diverging flow junctions by changing downstream duct sizes.

HVAC DUCT DESIGN PROCEDURES

1- Duct dimensions

The general procedure for HVAC system duct design is as follows:

- a) Study the building plans, and arrange the supply and return outlets to provide proper distribution of air within each space. Adjust calculated air quantities for duct heat gains or losses and duct leakage. Also, adjust the supply, return, and/or exhaust air quantities to meet space pressurization requirements.
- b) Select outlet sizes from manufacturers' data.
- c) Sketch the duct system, connecting supply outlets and return intakes with the air-handling units/air conditioners. Space allocated for supply and return ducts often dictates system layout and ductwork shape. Use round ducts whenever feasible.
- d) Divide the system into sections and number each section. A duct system should be divided at all points where flow, size, or shape changes. Assign fittings to the section toward the supply and return (or exhaust) terminals.
- e) Size ducts by the selected design method. Calculate system total pressure loss; then select the fan.
- f) Lay out the system in detail. If duct routing and fittings vary significantly from the original design, recalculate the pressure losses. Reselect the fan if necessary.
- g) Resize duct sections to approximately balance pressures at each junction.
- h) Analyze the design for objectionable noise levels, and specify sound attenuators as necessary. Refer to the section on System and Duct Noise.

Example (2)

For the system illustrated by Figures belows, size the ductwork by the equal friction method. Determine the system resistance and total pressure unbalance at the junctions. The airflow quantities are actual values adjusted for heat gains or losses, and ductwork is sealed (assume no leakage), Air is at 1.204 kg/m^3 density. The supply system is constructed of rectangular ductwork. the maximum main duct height is 0.25 m

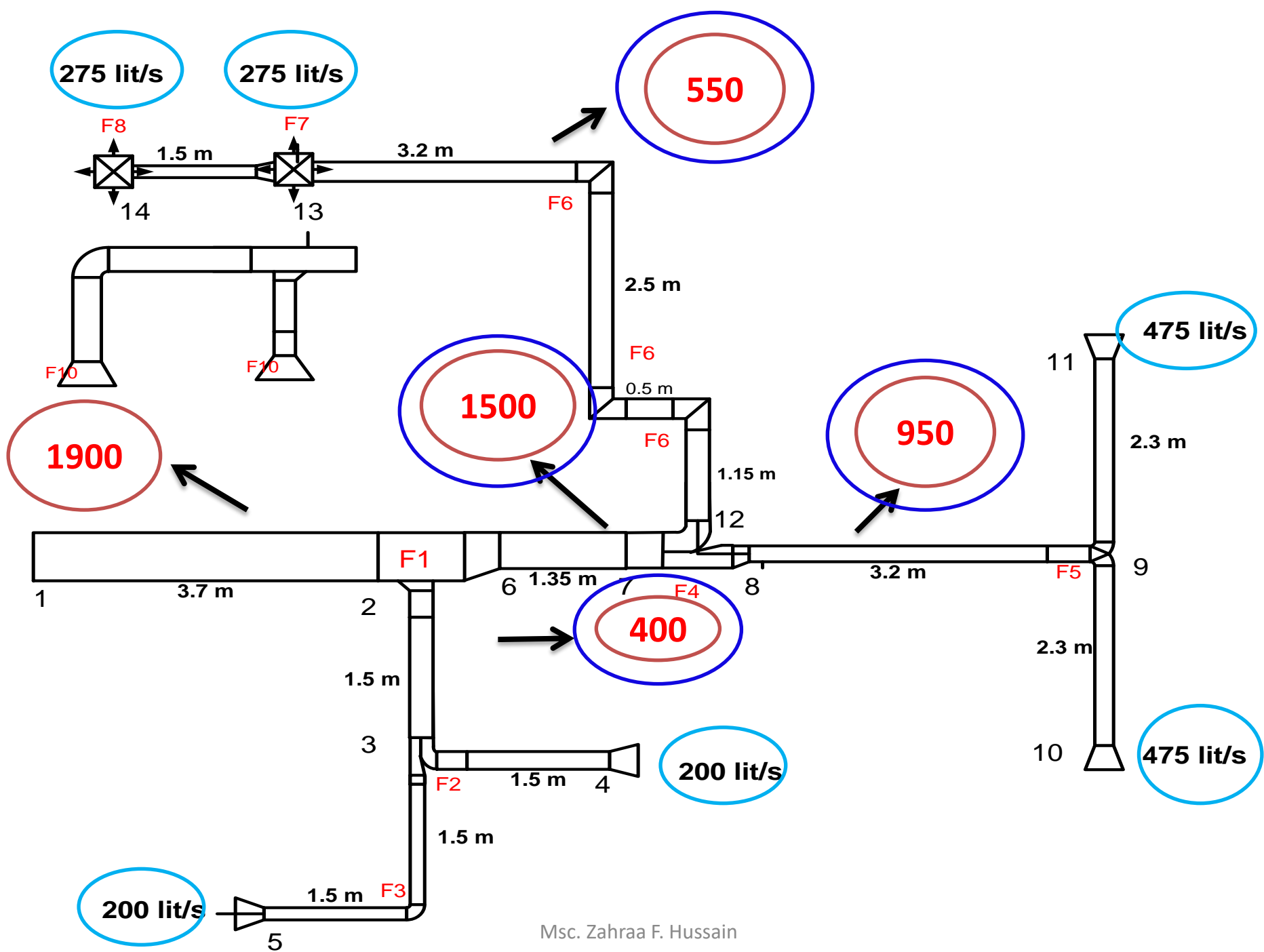


Table (2-1) Air velocity in duct system (m/s)

APPLICATION	CONTROLLING FACTOR NOISE GENERATION Main Duct	CONTROLLING FACTOR — DUCT FRICTION			
		Main Ducts		Branch Duct	
		Supply	Return	Supply	Return
Residences	3.0	5.1	3.0	3.0	3.0
Apartments Hotel Bedrooms Hospital Bedrooms	5.1	7.6	6.6	6.1	5.1
Private Offices Directors Rooms Libraries	6.1	10.2	7.6	7.1	6.1
Theatres Auditoriums	4.1	6.6	5.6	5.1	4.1
General Offices High Class Restaurants High Class Stores	7.6	10.2	7.6	8.1	6.1
Banks					
Average Stores Cafeterias	8.5	10.2	7.6	8.1	6.1
Industrial	12.7	15.2	9.1	11.2	7.6

C=8.5

- **Main duct section (1-2)**

- **V=C.A**

- **V=1.9 m³/s**

- **C=8.5 m/s (T2-1)**

- **1.9=8.5×A**

- **A=0.22335 m²**

- $A = \pi \frac{D^2}{4}$

- $0.22335 = \pi \frac{D^2}{4}$

- $D = \sqrt{\frac{4 \cdot A}{\pi}} = \sqrt{\frac{4 \cdot 0.22335}{3.14}} =$

- **D=0.533 m= 533mm**

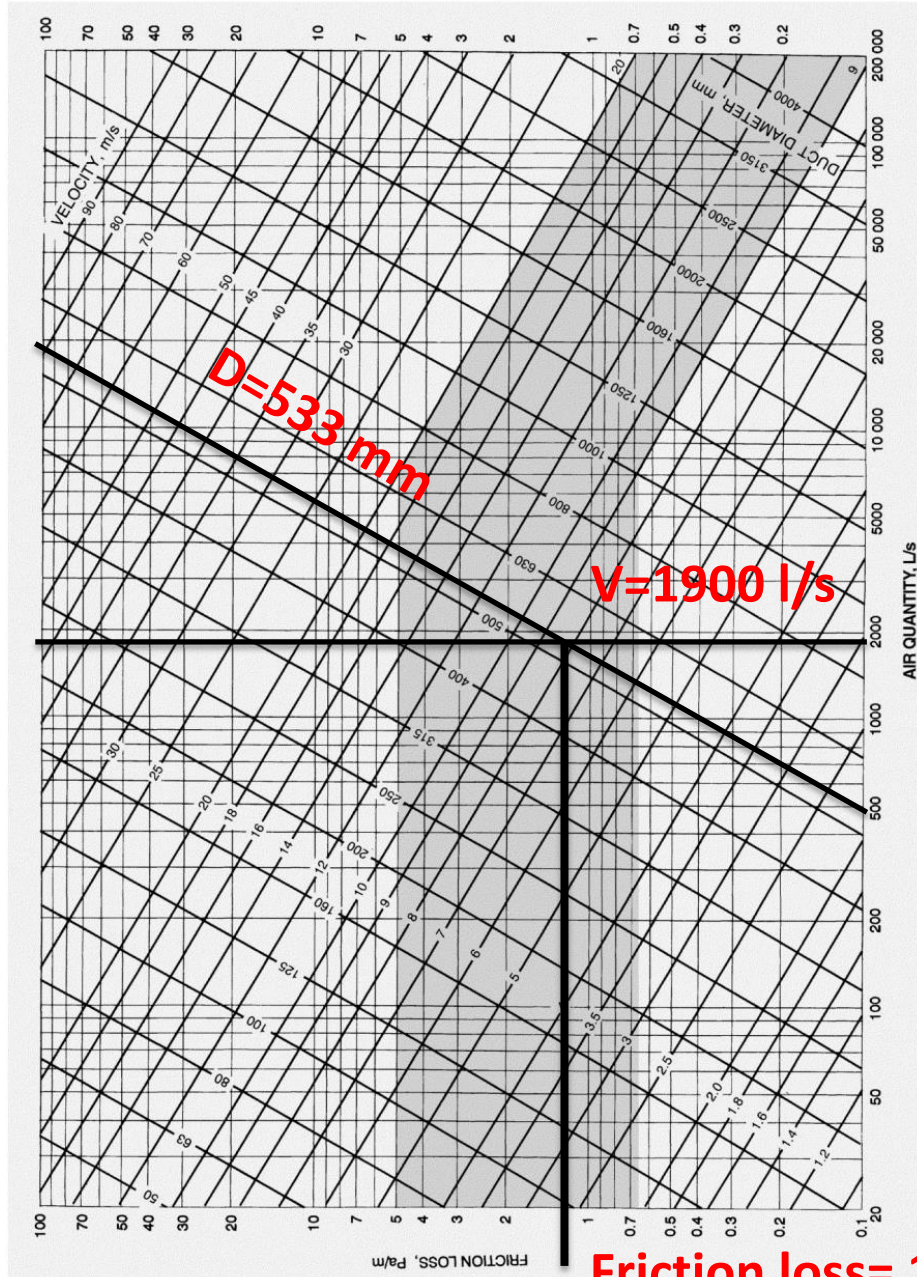
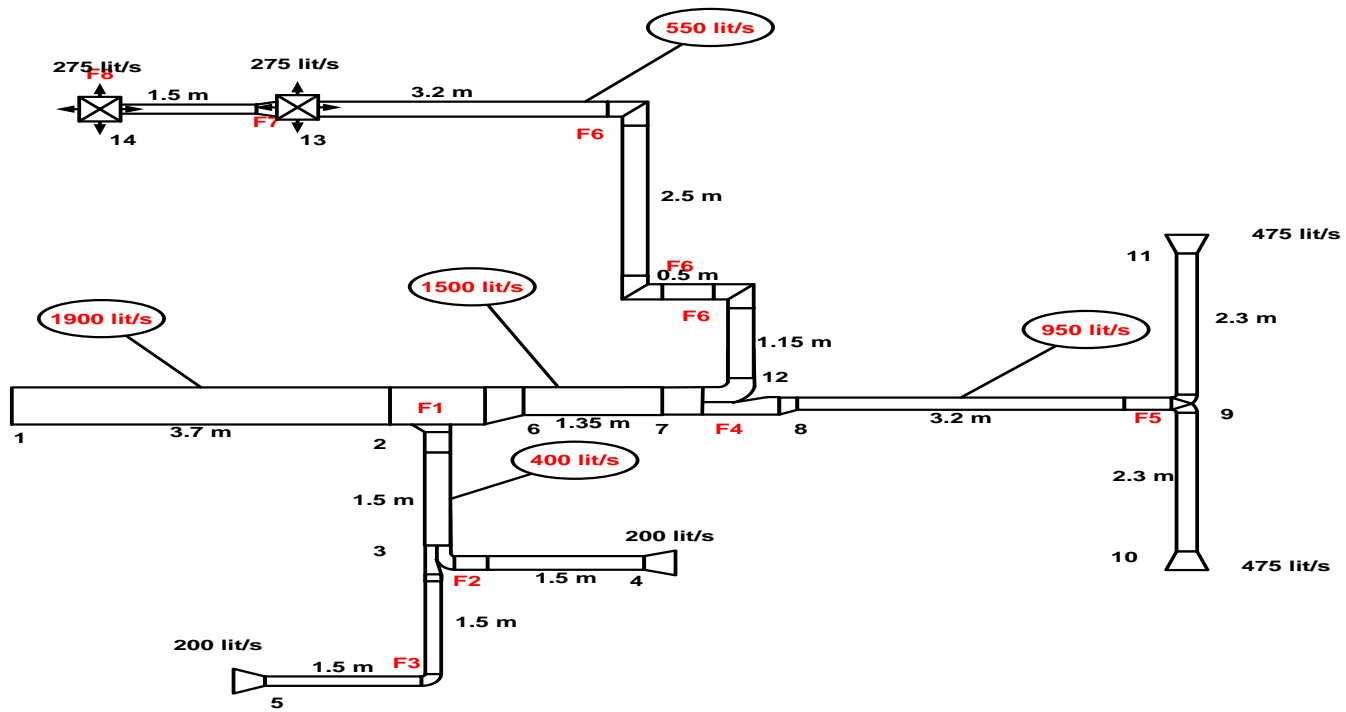


Fig.9 Friction Chart for Round Duct ($\rho = 1.20 \text{ kg/m}^3$ and $\epsilon = 0.09 \text{ mm}$)

V=1900 l/s
D=533 mm
Friction line

Friction loss = 1.2 Pa./m



Section	V	Deq.	C	W	H	L
1-2	1900					
2-3	400					
3.4	200					
3-5	200					
6-7	1500					
8-9	950					
9-10	475					
9-11	475					
12-13	550					
13-14	275					

Section	V	Deq.	C
1-2	1900	533	8.5
2-3	400	280	5.5
3-4	200	230	4.5
3-5	200	230	4.5
6-7	1500	480	7.8
8-9	950	420	6.8
9-10	475	320	5.8
9-11	475	320	5.8
12-13	550	330	6
13-14	275	260	4.8

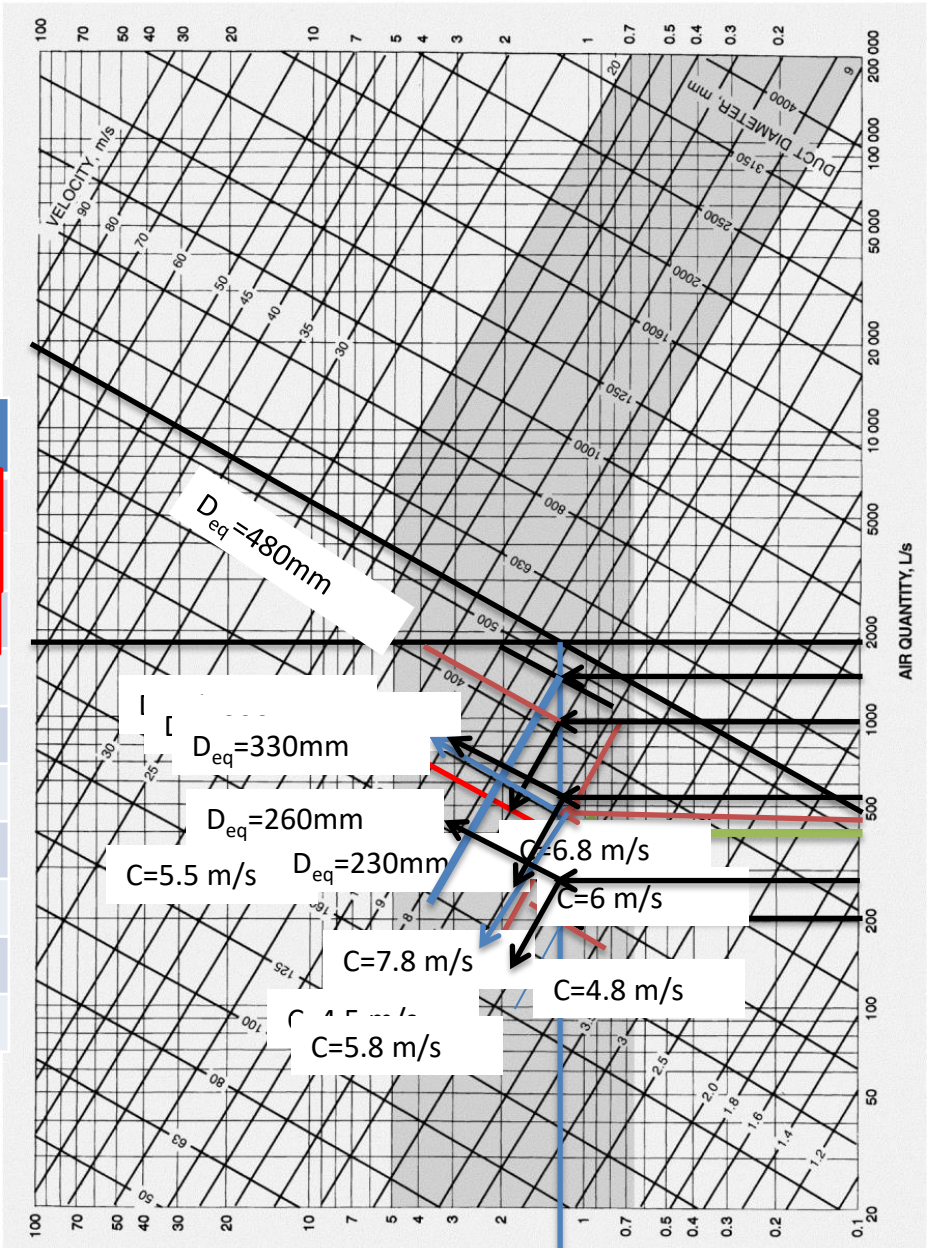
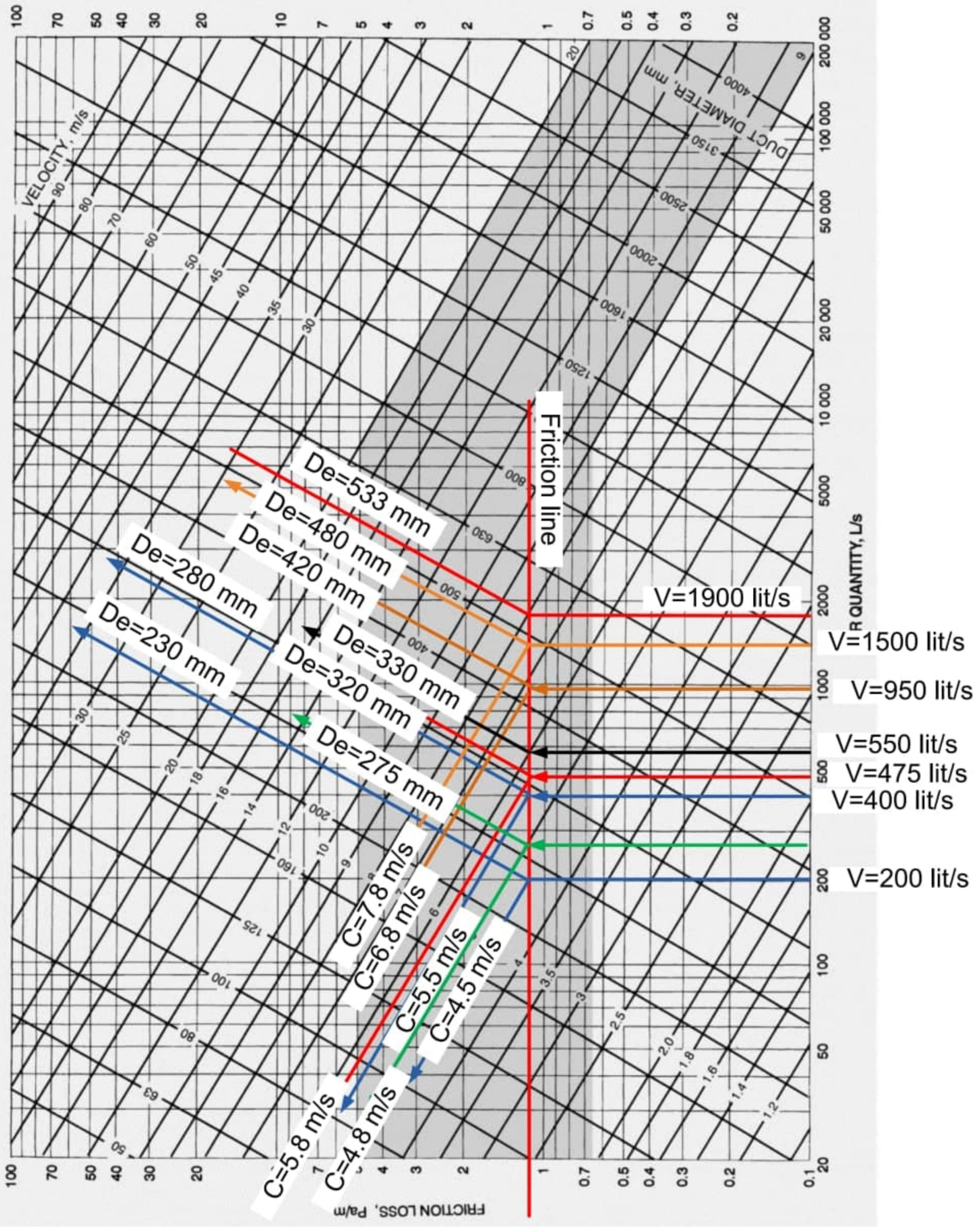
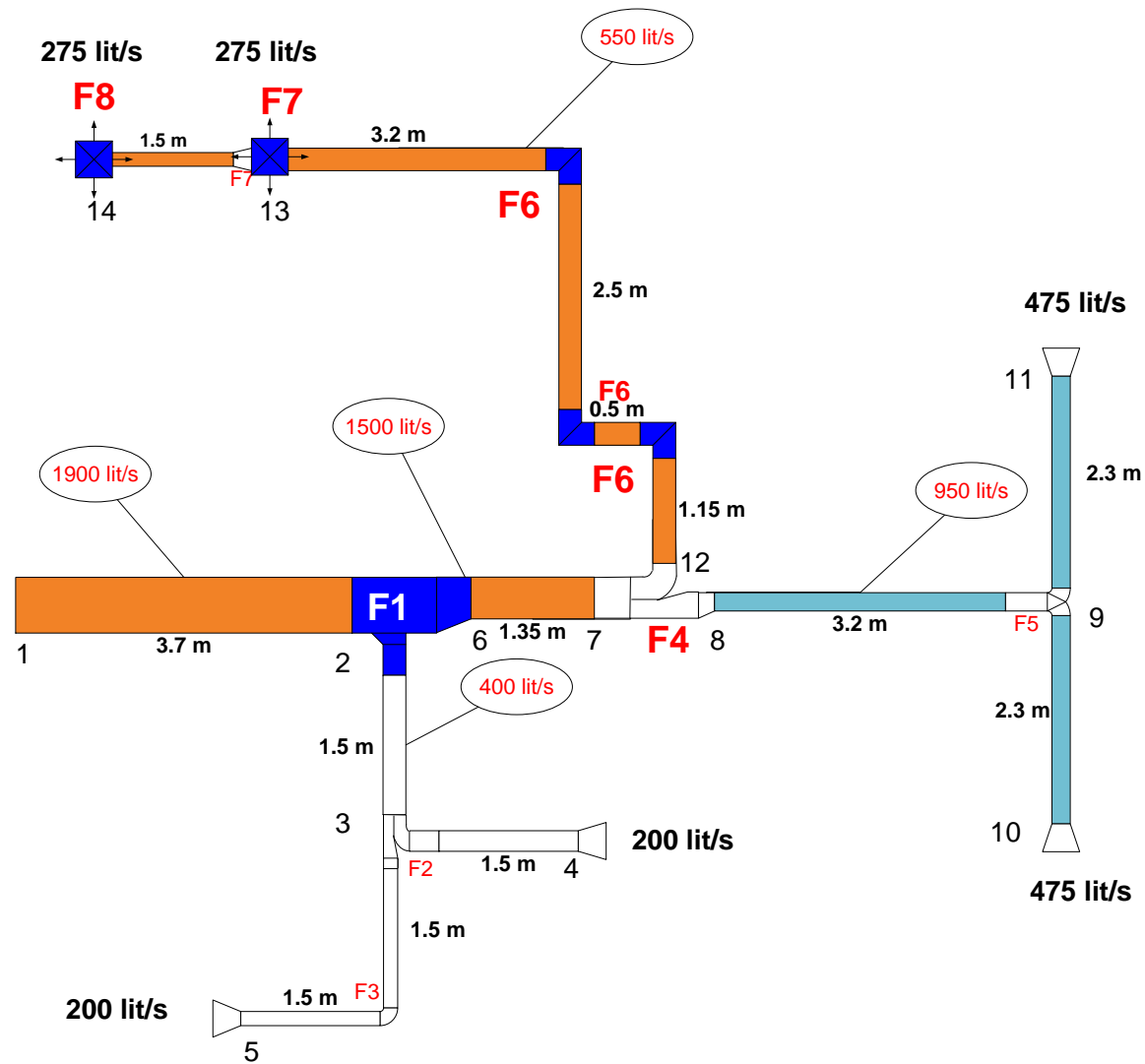


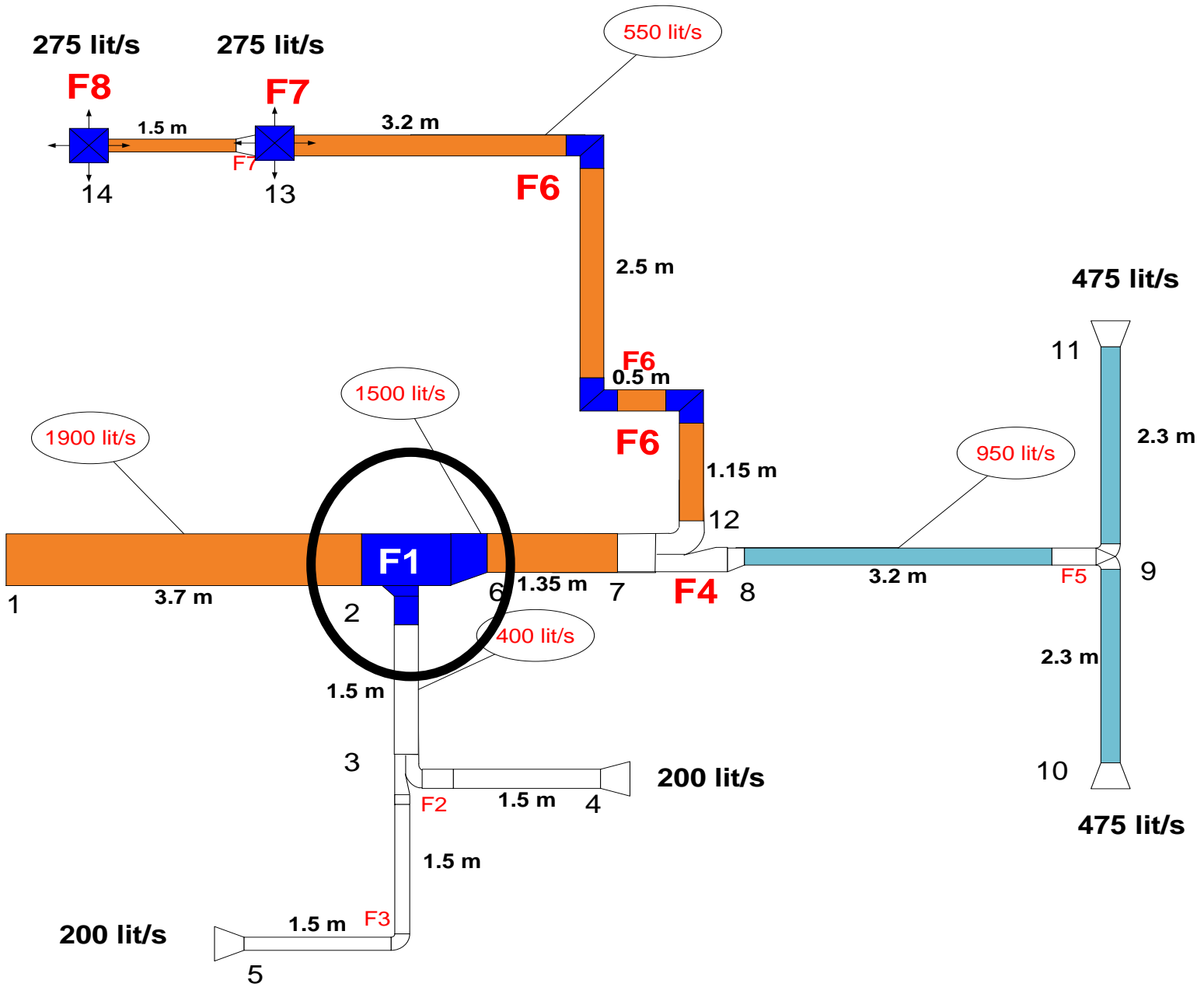
Fig.9 Friction Chart for Round Duct ($\rho = 1.20 \text{ kg/m}^3$ and $\epsilon = 0.09 \text{ mm}$)



Section	V (lit/s)	Deq. (mm)	C m/s	W (mm)	H (mm)
1-2	1900	533	8.5	1100	250
2-3	400	280	7	500	150
3-4	200	230	4.5	300	150
3-5	200	230	4.5	300	150
6-7	1500	480	7.8	900	250
8-9	950	420	6.8	650	250
9-10	475	320	5.8	650	150
9-11	475	320	5.8	650	150
12-13	550	330	6	700	150
13-14	275	260	4.8	400	150

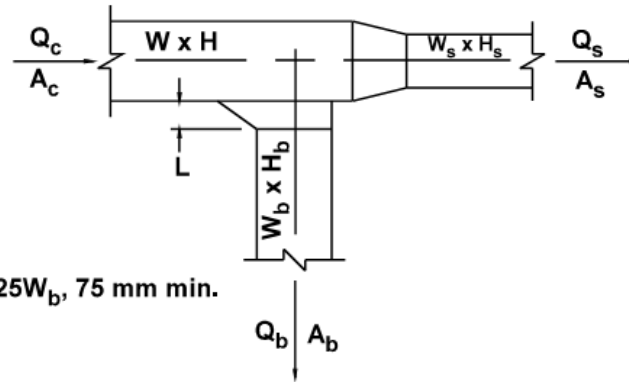
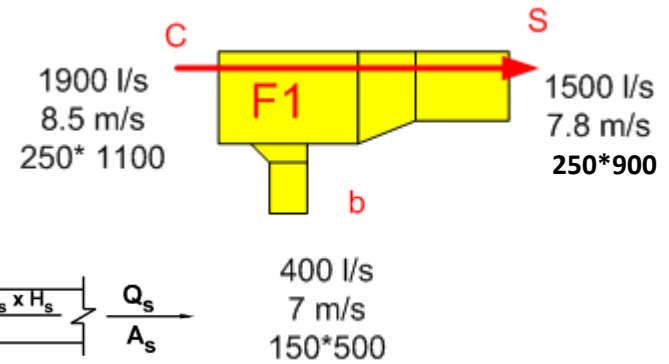
- Maximum length of the duct:
- **Path (1-2-6-7-12-13-14)=**
 $=3.7+1.35+1.15+0.5+2.5+3.2+1.5=13.9\text{ m}$
- **Path(1-2-6-7-8-9-11)=**
 $3.7+1.35+3.2+2.3=10.55\text{ m}$
- Then the **first path** must be selected.
- **Fittings** in path (1-2-6-7-12-13-14) are:
F1, F4, F6,F7 and F8.
- The pressure loss in the fittings above should be calculated





Fitting F1

1. $Q_c=1900$ lit/s
2. $A_c=1.1*0.25=0.275$ m²
3. $Q_s=1500$ lit/s
4. $A_s=0.25*0.9=0.225$



$$1. \frac{A_s}{A_c} = \frac{0.225}{0.275} = 0.82$$

$$2. \frac{Q_s}{Q_c} = \frac{1500}{1900} = 0.789$$

C_s Values

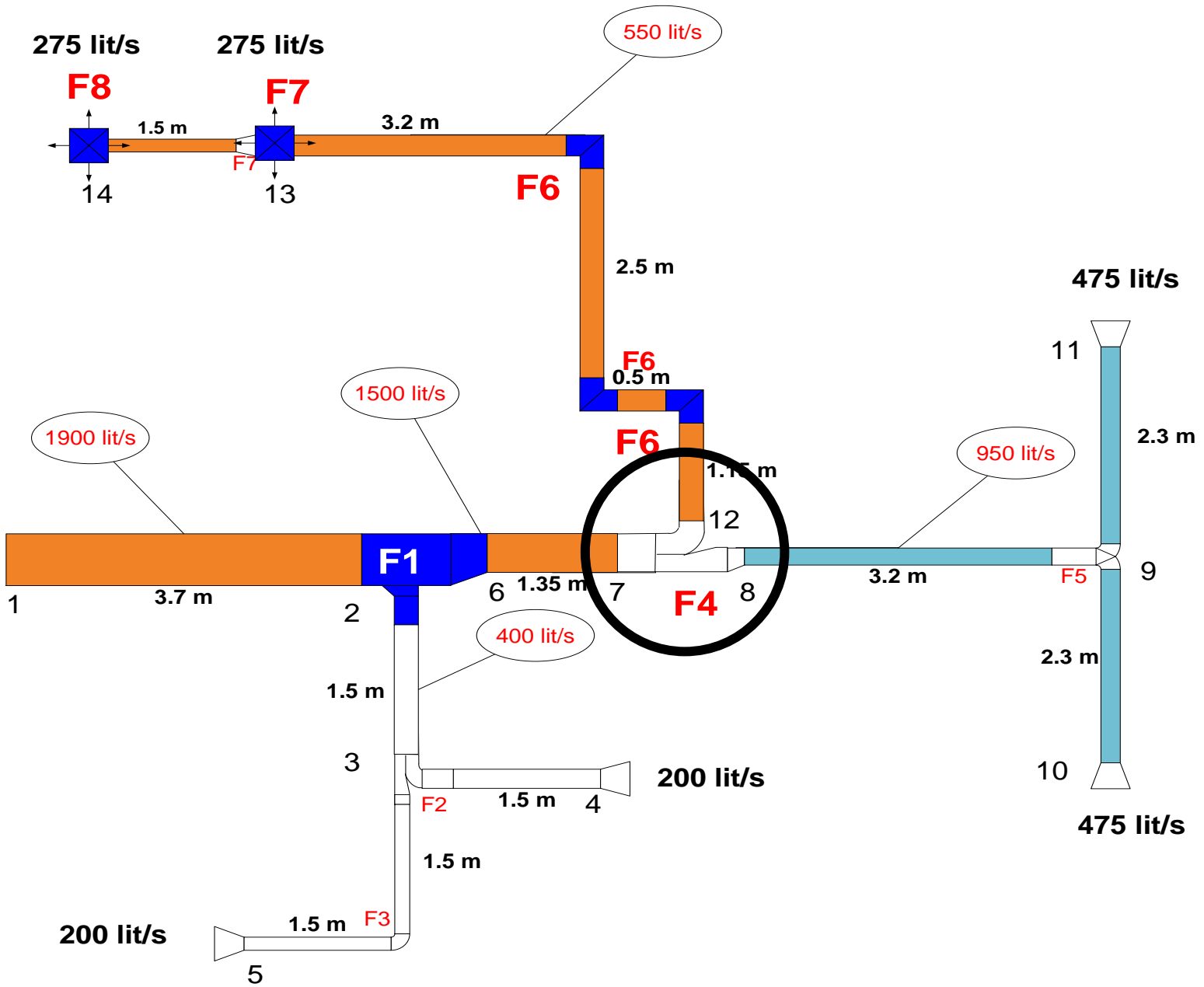
A_s/A_c	Q_s/Q_c								
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.04								
0.2	0.98	0.04							
0.3	3.48	0.31	0.04						
0.4	7.55	0.98	0.18	0.04					
0.5	13.18	2.03	0.49	0.13	0.04				
0.6	20.38	3.48	0.98	0.31	0.10	0.04			
0.7	29.15	5.32	1.64	0.60	0.23	0.09	0.04		
0.8	39.48	7.55	2.47	0.98	0.42	0.18	0.08	0.04	
0.9	51.37	10.17	3.48	1.46	0.67	0.31	0.15	0.07	0.04

$C_s=0.07$

$$\Delta P = \frac{1}{2} \cdot C_s \rho \cdot C^2$$

$$\Delta P(F1) =$$

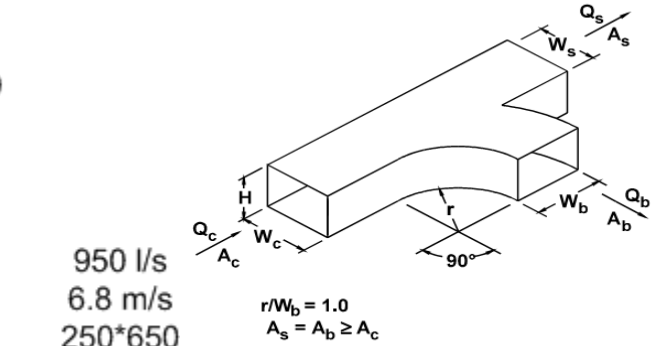
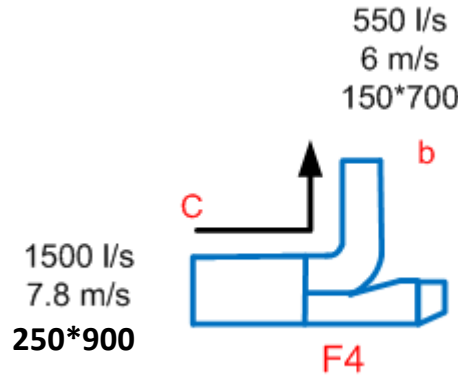
$$\frac{1}{2} \cdot 0.07 \times 1.204 \times 8.5^2 = 3.044$$



Fitting F4

SR5-1 Smooth Wye of Type $A_s + A_b \geq A_c$, Branch 90° to Main, Diverging

1. $Q_c = 1500$ lit/s
2. $A_c = 0.25 \times 0.9 = 0.225$ m²
3. $A_s = 0.65 \times 0.25 = 0.1625$
4. $Q_b = 550$ lit/s
5. $A_b = 0.15 \times 0.7 = 0.105$
6. $\frac{A_s}{A_c} = \frac{0.1625}{0.225} = 0.72$
7. $\frac{A_b}{A_c} = \frac{0.105}{0.25} = 0.42$
8. $\frac{Q_b}{Q_c} = \frac{550}{1500} = 0.367$



SR5-1 Smooth Wye of Type $A_s + A_b \geq A_c$, Branch 90° to Main, Diverging

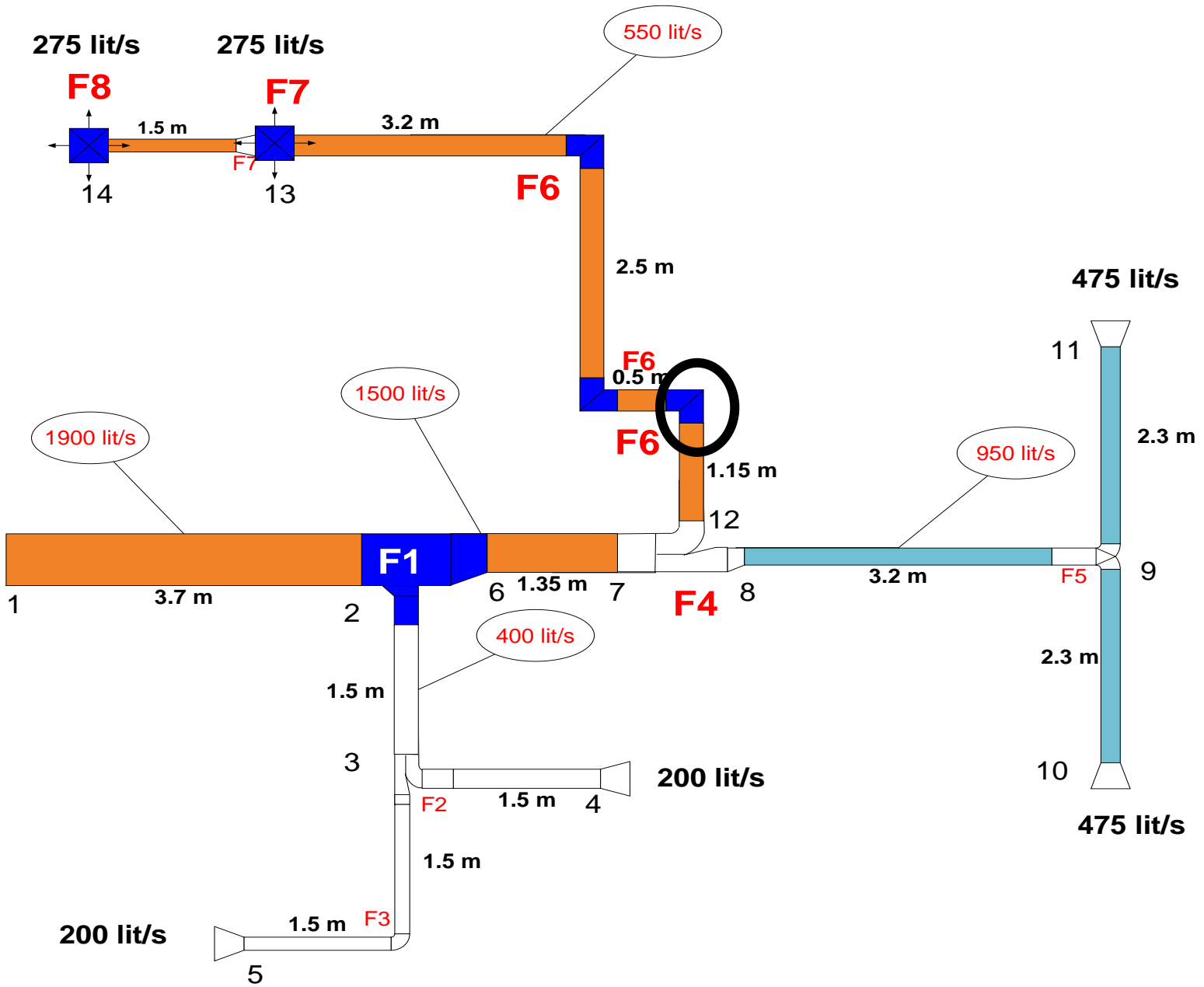
		C_o Values									
		Q_b/Q_c									
A_s/A_c	A_b/A_c	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	
0.50	0.25	3.44	0.70	0.30	0.20	0.17	0.16	0.16	0.17	0.18	
	0.50	11.00	2.37	1.06	0.64	0.52	0.47	0.47	0.47	0.48	
	1.00	60.00	13.00	4.78	2.06	0.96	0.47	0.31	0.27	0.26	
0.75	0.25	2.19	0.55	0.35	0.31	0.33	0.35	0.36	0.37	0.39	
	0.50	13.00	2.50	0.89	0.47	0.34	0.31	0.32	0.36	0.43	
	1.00	70.00	15.00	5.67	2.62	1.36	0.78	0.53	0.41	0.36	
1.00	0.25	3.44	0.78	0.42	0.33	0.30	0.31	0.40	0.42	0.46	
	0.50	15.50	3.00	1.41	0.62	0.48	0.42	0.40	0.42	0.46	
	1.00	67.00	13.75	5.11	2.31	1.28	0.81	0.59	0.47	0.46	

- $\Delta P = \frac{1}{2} \cdot C_s \rho \cdot C^2$

- $\Delta P(F4) = \frac{1}{2} \cdot 0.47 \times 1.204 \times 7.8^2$

- = 17.2 Pa.

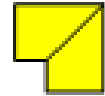
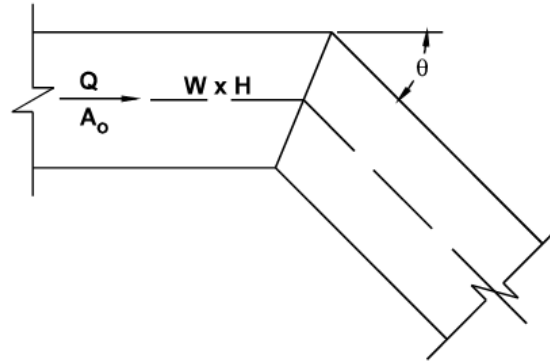
$C_s = 0.47$



Fitting F6

CR3-6 Elbow, Mitered

θ	C_o Values										
	H/W										
	0.25	0.50	0.75	1.00	1.50	2.00	3.00	4.00	5.00	6.00	8.00
20	0.08	0.08	0.08	0.07	0.07	0.07	0.06	0.06	0.05	0.05	0.05
30	0.18	0.17	0.17	0.16	0.15	0.15	0.13	0.13	0.12	0.12	0.11
45	0.38	0.37	0.36	0.34	0.33	0.31	0.28	0.27	0.26	0.25	0.24
60	0.60	0.59	0.57	0.55	0.52	0.49	0.46	0.43	0.41	0.39	0.38
75	0.89	0.87	0.84	0.81	0.77	0.73	0.67	0.63	0.61	0.58	0.57
90	1.30	1.27	1.23	1.18	1.13	1.07	0.98	0.92	0.89	0.85	0.83



F6

550 l/s
6 m/s
150*700

$C_s = 1.3$

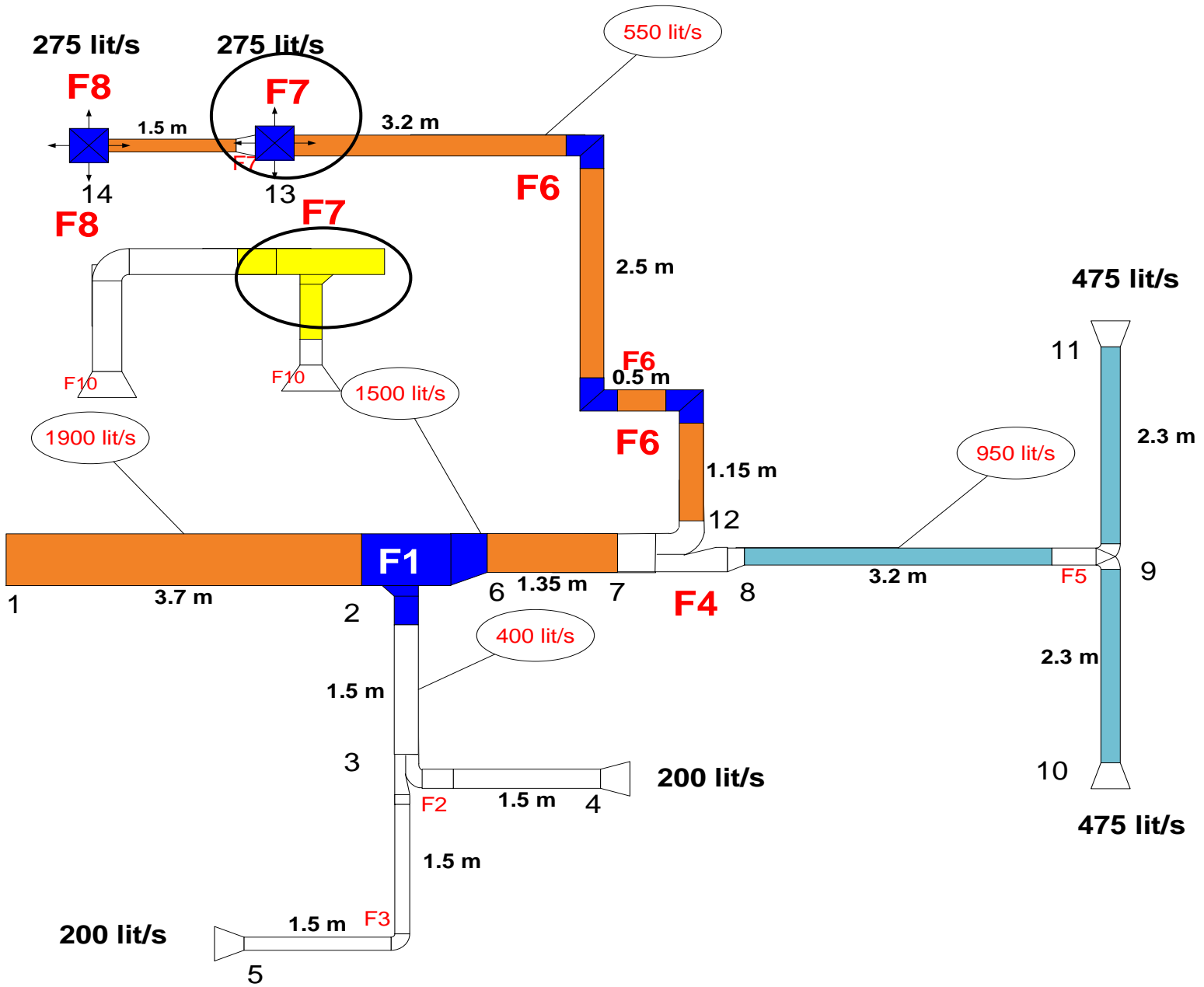
$H = 150$ mm

$W = 700$ mm

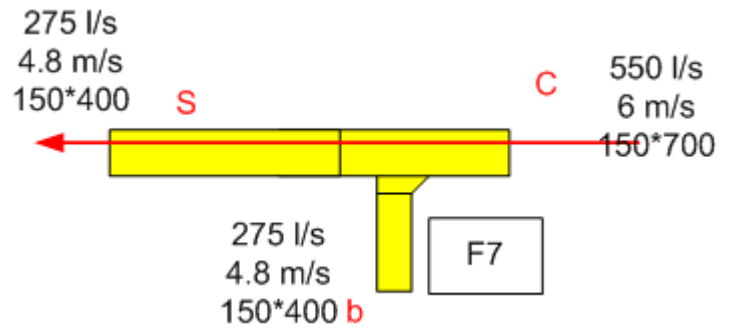
$$\frac{H}{W} = \frac{150}{700} = 0.21$$

$$\Delta P = \frac{1}{2} \cdot C_s \rho \cdot C^2$$

$$\Delta P(F6) = \frac{1}{2} \cdot 1.3 \times 1.204 \times 6^2 = 28.17 \text{ Pa.}$$



Fitting F7

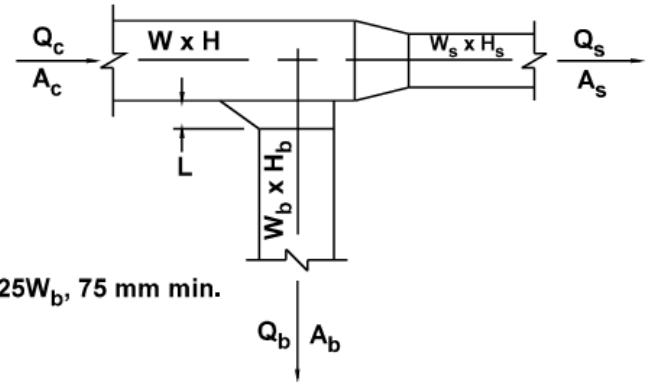


SR5-13 Tee, 45 Degree Entry Branch, Diverging

1. $Q_c = 550 \text{ lit/s}$
2. $A_c = 0.7 \times 0.15 = 0.105 \text{ m}^2$
3. $Q_s = 275 \text{ lit/s}$
4. $A_s = 0.4 \times 0.15 = 0.06$

5. $\frac{A_s}{A_c} = \frac{0.06}{0.105} = 0.57$

6. $\frac{Q_s}{Q_c} = \frac{275}{550} = 0.5$

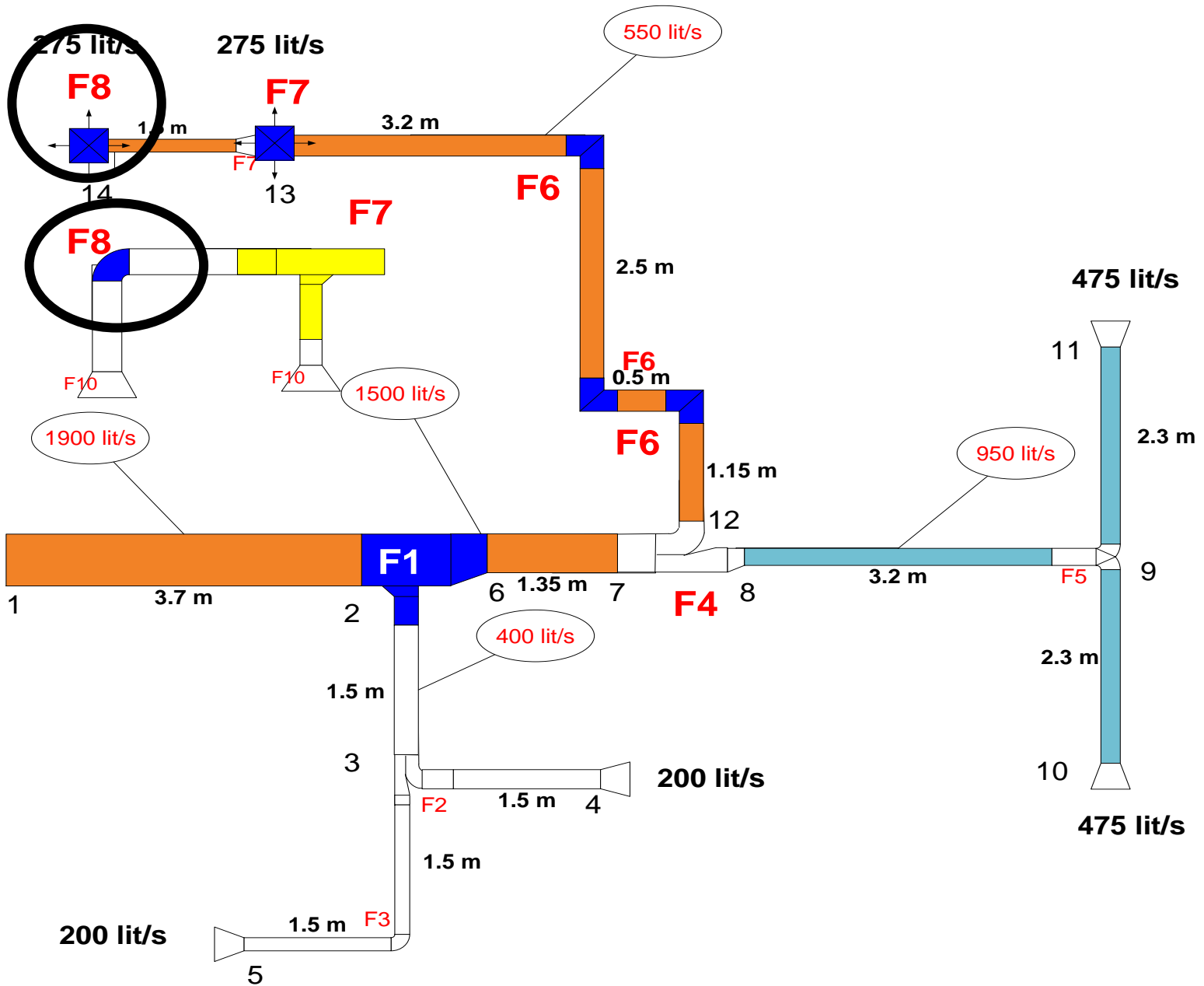


C_s Values

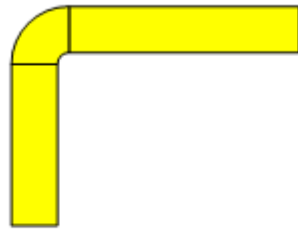
A_s/A_c	Q_s/Q_c									
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	
0.1	0.04									
0.2	0.98	0.04								
0.3	3.48	0.31	0.04							
0.4	7.55	0.98	0.18	0.04						
0.5	13.18	2.03	0.49	0.13	0.04					
0.6	20.38	3.48	0.98	0.31	0.10	0.04				
0.7	29.15	5.32	1.64	0.60	0.23	0.09	0.04			
0.8	39.48	7.55	2.47	0.98	0.42	0.18	0.08	0.04		
0.9	51.37	10.17	3.48	1.46	0.67	0.31	0.15	0.07	0.04	

$C_s = 0.1$

- $\Delta P = \frac{1}{2} \cdot C_s \rho \cdot C^2$
- $\Delta P(F7) = \frac{1}{2} \cdot 0.1 \times 1.204 \times 6^2 = 2.167 \text{ Pa.}$

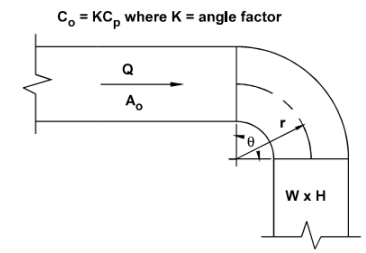


F8



275 l/s
4.8 m/s
150*400

275 l/s
4.8 m/s
150*400



$$H/W = 150/400 = 0.375$$

$$r/W = 1.5$$

$$\theta = 90$$

$$C_p = 0.22$$

$$K = 1$$

$$\Delta P = \frac{1}{2} \cdot K C_p \rho \cdot C^2$$

$$= \frac{1}{2} \times 1 \times 0.22 \times 1.204 \times 4.8^2$$

$$= 3.05 \text{ Pa.}$$

CR3-1 Elbow, Smooth Radius, Without Vanes

		C _p Values										
		H/W										
r/W		0.25	0.50	0.75	1.00	1.50	2.00	3.00	4.00	5.00	6.00	8.00
0.50		1.53	1.38	1.29	1.18	1.06	1.00	1.00	1.06	1.12	1.16	1.18
0.75		0.57	0.52	0.48	0.44	0.40	0.39	0.39	0.40	0.42	0.43	0.44
1.00		0.27	0.25	0.23	0.21	0.19	0.18	0.18	0.19	0.20	0.21	0.21
1.50		0.22	0.20	0.19	0.17	0.15	0.14	0.14	0.15	0.16	0.17	0.17
2.00		0.20	0.18	0.16	0.15	0.14	0.13	0.13	0.14	0.14	0.15	0.15
		Angle Factor K										
θ		0	20	30	45	60	75	90	110	130	150	180
K		0.00	0.31	0.45	0.60	0.78	0.90	1.00	1.13	1.20	1.28	1.40

Pressure loss due fittings

- $\Delta P_{t,f} = 3.044 + 17.2 + 3(28.17) + 2.167 + 3.05 = 110 \text{ Pa}$
- Pressure loss due duct length = duct length * Friction loss per meter
- $= 13.9 * 1.2 = 17 \text{ Pa}$
- $\Delta P_t = 110 + 17 = 127 \text{ Pa}$.