

Calculation of Tower Height

The physical absorption process can be carried out in countercurrent flow process, which may be carried out in packed or tray column:

Packed Tower $Z =$

HOG * NOG

Where:

H : is the distance between two trays, and it is given (0.3 - 0.7 m)

Where:

HOG: is the height of transfer unit (HTU) based on gas phase, and it can be calculated from the equation

below:

$$\mathbf{HOG} = \frac{\bar{G}_s}{K_oG \cdot a} \text{ , in (meter)}$$

N : is the number of trays, and it can be calculated based on equilibrium data:

NOG: is the number of transfer unit (NTU) based on gas phase, and it can be calculated based on equilibrium data:

If the equilibrium data are *linear*, then **NOG** will be calculated using a suitable equation.

If the equilibrium data are *non-linear*, then **NOG** will be calculated graphical method.

If the equilibrium data are *linear*, then **N** will be calculated using a suitable equation.

If the equilibrium data are *non-linear*, then **N** will be calculated graphical method.

Tray Tower

$$Z = H * N$$

1. Packed tower:

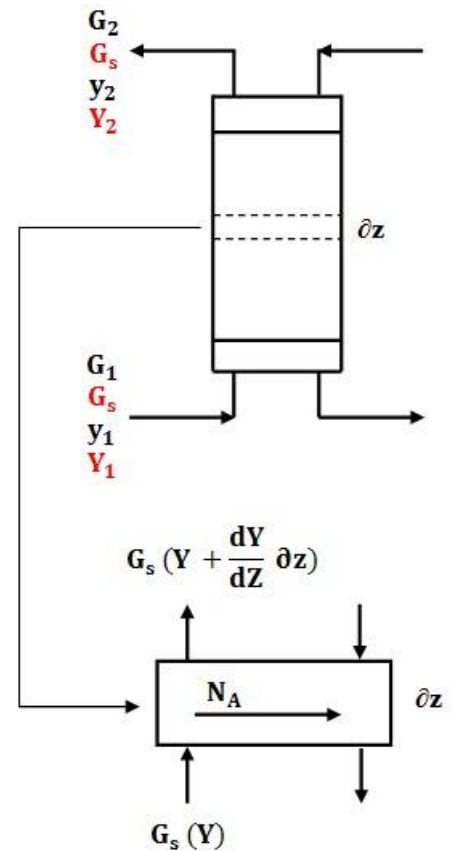
Absorption and stripping are frequently conducted in packed columns, particularly when:

- (1) the required column diameter is less than 0.6 m.
- (2) the pressure drop must be low, as for a vacuum service.
- (3) corrosion consideration favor the use of ceramic or polymeric material.
- (4) low liquid holdup is desirable.

The gas liquid contact in a packed bed column is continuous, not stage-wise, as in a plate column. The liquid flows down the column over the packing surface and the gas or vapour, counter-currently, up the column. In some gas-absorption columns co-current flow is used. The performance of a packed column is very dependent on the maintenance of good liquid and gas distribution throughout the packed bed, and this is an important consideration in packed-column design.

Calculations of the packing height based on gas phase:

Overall material balance on the solute (A) over an element (∂z) based on gas phase:



$$G_s dY = L_s dX = N_A \cdot A$$

$$N_A = G_s Y - G_s \left(Y + \frac{dY}{dZ} \partial z \right) = (K_oG)(a S \partial z)(Y - Y^*)$$

Where:

The interfacial area for transfer = $a dV = a S \partial z$

S: is the cross-sectional area of column (m^2).

a: is the surface area of interface per unit volume of column (m^2/m^3).

$$- G_s \left(\frac{dY}{dZ} \partial z \right) = (K_oG \cdot a)(S \cdot \partial z)(Y - Y^*)$$

$$G_s \frac{dY}{dZ} = -(K_oG \cdot a)(S \cdot \partial z)(Y - Y^*)$$

$$\int_0^Z dZ = \frac{-G_s}{(KoG \cdot a) \cdot S} \int_{Y_1}^{Y_2} \frac{dY}{(Y - Y^*)}$$

$$Z = \frac{(G_s/S)}{KoG \cdot a} \int_{Y_2}^{Y_1} \frac{dY}{(Y - Y^*)}$$

$$Z = \frac{G_s}{KoG \cdot a} \int_{Y_2}^{Y_1} \frac{dY}{(Y - Y^*)}$$

$$Z = HOG * NOG = HTU * NTU$$

Where:

$HOG = \frac{\bar{G}_s}{KoG \cdot a}$: height of transfer unit (HTU) based on gas phase, with the units of (m).

$NOG = \int_{Y_2}^{Y_1} \frac{dY}{(Y - Y^*)}$: number of transfer unit (NTU) based on gas phase, without units.

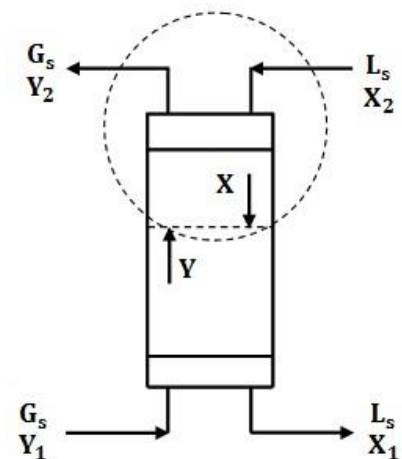
Equation of the operating line:

Solute material balance between one end of the column and any point will give:

$$G_s (Y - Y_2) = L_s (X - X_2)$$

$$Y = \frac{L_s}{G_s} X - X_2 + Y_2$$

* The equation of operating line is a relation between mole ratio of solute in gas phase (Y) and the mole ratio of solute in liquid phase (X).



* The operating line can be drawn from two points (X_1, Y_1) and (X_2, Y_2) , or from its slope $\frac{L_s}{G_s}$ and one of the two points.

