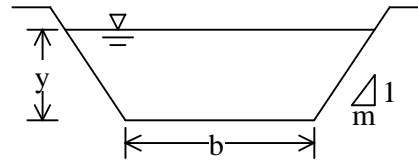


8.2.2.2 Trapezoidal section

$$B = b + 2 * m * y$$

$$A = (b + m * y) * y$$

$$P = b + 2 * y * \sqrt{1 + m^2}$$



By eliminating b from P,

$$P = \frac{A}{y} + (2 * \sqrt{1 + m^2} - m) * y$$

For a minimum value of P, $\delta P = 0$,

i.e. $\frac{dP}{dy} = 0$ and $\frac{dP}{dm} = 0$

From $\frac{dP}{dy} = 0$, $y^2 = \frac{A}{\sqrt{3}}$

From $\frac{dP}{dm} = 0$, $m = \frac{1}{\sqrt{3}}$

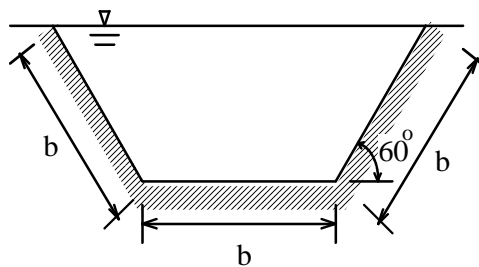
It implies the side slope of the channel is 60° to horizontal.

$$b = \frac{A}{y} - my = \sqrt{3}y - \frac{y}{\sqrt{3}} = \frac{2\sqrt{3}}{3} y$$

and $P = \frac{2\sqrt{3}}{3} y + \frac{4}{\sqrt{3}} y = 2\sqrt{3}y$

i.e. $P = 3 * b$

The optimum section is given as follow:

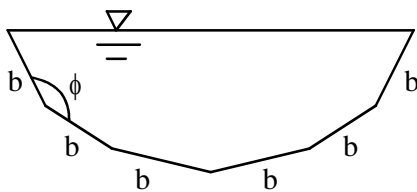


8.2.2.3 Other sections

N-side Channel

- ◆ from the conclusion of the previous two sections
 - reflection of the rectangular optimum section about the water surface will form a **square** of side b .
 - reflection of the trapezoidal optimum section about the water surface will form a regular **hexagon** of side b .

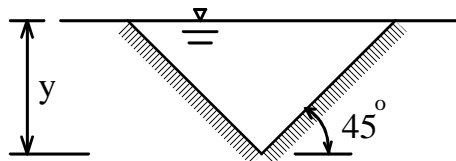
- ◆ For a N-side channel, the optimum hydraulic section should be in a form of half a **2N-side regular polygon**.



$$\phi = \left(\frac{N-1}{N} \right) * 180^\circ$$

Triangular Section

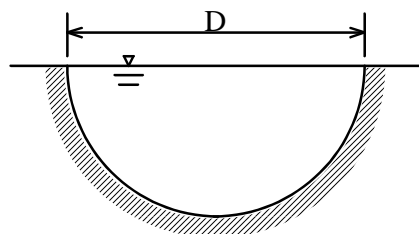
- ◆ $N = 2$, hence $\phi = 90^\circ$



Circular Section

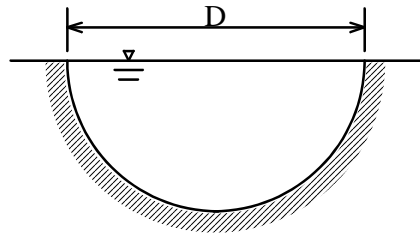
- ◆ From the result of N-side channel, it can be concluded that the optimum section of a circular channel is a **semi-circle**.

- ◆ It is the most optimum section for all the possible open-channel cross-section.



Worked examples

1. An open channel is to be designed to carry $1 \text{ m}^3/\text{s}$ at a slope of 0.0065. The channel material has an n value of 0.011. Find the optimum hydraulic cross-section for a semi-circular section.

**Answer**

The optimum circular section is a semi-circular section with diameter D which can discharge $1 \text{ m}^3/\text{s}$.

For a semi-circular section,

$$A = \pi * D^2 / 8$$

$$P = \pi * D / 2$$

$$R = A / P \\ = D / 4$$

As $n = 0.011$, $S = 0.0065$ and $Q = 1 \text{ m}^3/\text{s}$.

$$Q = \frac{A}{n} * R^{2/3} * S^{1/2}$$

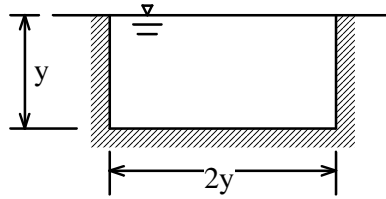
$$\text{i.e. } 1 = \frac{\pi * D^2}{8 * 0.011} * \left(\frac{D}{4}\right)^{2/3} * \sqrt{0.0065}$$

$$D^{8/3} = \frac{8 * 0.011}{\pi} * 4^{2/3} * 0.0065^{-1/2}$$

$$D = 0.951 \text{ m}$$

The diameter of this optimum section is 951mm.

2. Find the optimum rectangular section from the last example.



Answer

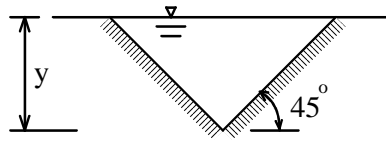
$$\begin{aligned} A &= 2*y^2 \\ P &= 4*y \\ R &= A/P = y/2 \end{aligned}$$

By Manning equation,

$$\begin{aligned} Q &= \frac{A}{n} * R^{2/3} * S^{1/2} \\ 1 &= \frac{2*y^2}{0.011} * \left(\frac{y}{2}\right)^{2/3} * \sqrt{0.0065} \\ y^{8/3} &= \frac{1*0.011*2^3}{2*\sqrt{0.0065}} \\ y &= 0.434 \text{ m} \end{aligned}$$

The optimum rectangular section has dimension of width 0.868m and depth 0.434m.

3. Find the optimum triangular section from the last example.



Answer

$$A = y^2$$

$$P = 2\sqrt{2} * y$$

$$R = A/P = \frac{y}{2\sqrt{2}}$$

By Manning equation,

$$Q = \frac{A}{n} * R^{2/3} * S^{1/2}$$

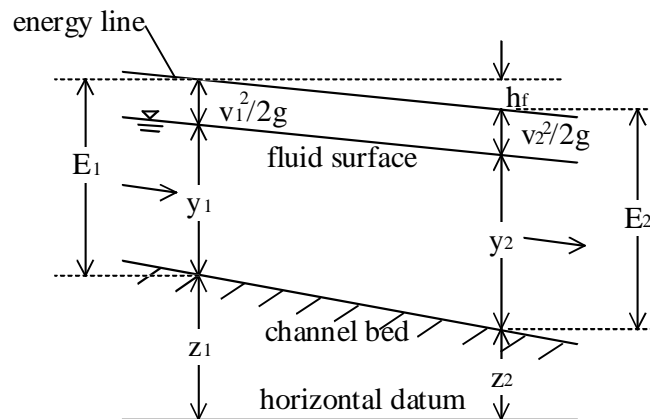
$$1 = \frac{y^2}{0.011} * \left(\frac{y}{2\sqrt{2}} \right)^{2/3} * \sqrt{0.0065}$$

$$y^{8/3} = \frac{0.011 * (2\sqrt{2})^{2/3}}{\sqrt{0.0065}}$$

$$y = 0.614 \text{ m}$$

The optimum triangular section is a right angle triangle with depth 0.614 m.

8.3 Non-Uniform flow - Specific Energy in Open Channel & Critical Flow



- ◆ In open channel, the solution of many problems are greatly assisted by the concept of **specific energy**, i.e.

$$E = \frac{v^2}{2g} + y \quad (8.3)$$

In terms of flow rate, Q ,

$$E = \frac{1}{2g} \left(\frac{Q}{A}\right)^2 + y \quad (8.4)$$

- ◆ The minimum energy will be given as

$$\frac{dE}{dy} = 0 \quad (8.5)$$

8.3.1 Rectangular Channel

- ◆ Let $q = \frac{Q}{b} = v \cdot y$ (8.6)

q - the discharge per unit width of a rectangular channel

$$\therefore E = \frac{q^2}{2gy^2} + y \quad (8.7)$$

- ◆ By assuming q is constant

$$\frac{dE}{dy} = 1 - \frac{q^2}{gy^3} = 0 \quad (8.8)$$

$$\begin{aligned} \text{or } y &= y_c \\ &= \left(\frac{q^2}{g}\right)^{1/3} \end{aligned} \quad (8.9)$$

y_c - critical depth at which the energy is minimum.

- ◆ The corresponding energy, E is

$$E_{\min} = \frac{3}{2} y_c \quad (8.10)$$

- ◆ From (8.6), $v = \frac{q}{y}$.

Substitute into (8.8),

$$\begin{aligned} 1 - \frac{v_c^2}{gy_c} &= 0 \\ \frac{v_c^2}{gy_c} &= 1 \end{aligned} \quad (8.11)$$

$$\text{or } v_c = \sqrt{gy_c} \quad (8.12)$$

- ◆ Since Froude number, Fr is defined as

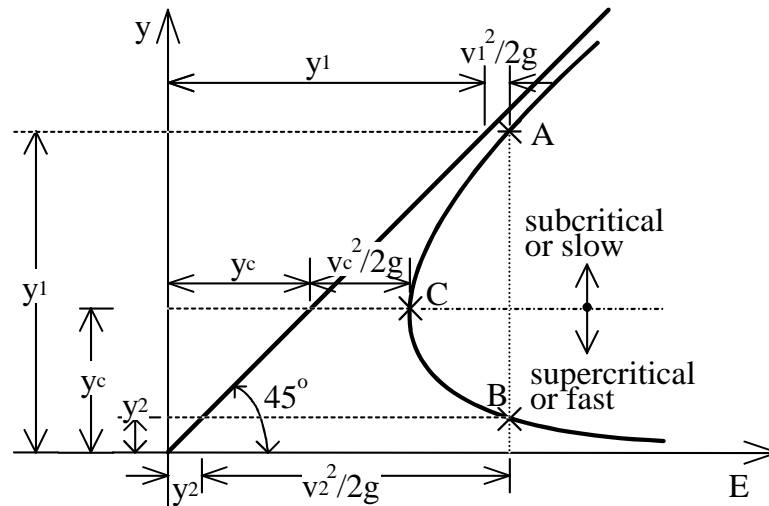
$$Fr = \frac{v}{\sqrt{gy_{\text{ave}}}} \quad (8.13)$$

Hence, the minimum energy is occurred when

$$Fr^2 = 1 \quad (8.14)$$

- ◆ For a given discharge, Q , if the flow is such that E is a min., the flow is **critical flow**.

- critical flow - flow with E_{\min}
- critical depth, y_c - the depth of the critical flow
- critical velocity - $v_c = \sqrt{gy_c}$



- ◆ If the flow with $E > E_{\min}$, there are two possible depths (y_1, y_2).
 - (y_1, y_2) are called **alternate depths**.
- ◆ C divides the curve AB into AC and CB regions.
 - AC - **subcritical** flow region
 - CB - **supercritical** flow region

	Subcritical	Critical	Supercritical
Depth of flow	$y > y_c$	$y = y_c$	$y < y_c$
Velocity of flow	$v < v_c$	$v = v_c$	$v > v_c$
Slope	Mild $S < S_c$	Critical $S = S_c$	Steep $S > S_c$
Froude number	$Fr < 1.0$	$Fr = 1.0$	$Fr > 1.0$
Other	$\frac{v^2}{2g} < \frac{y_c}{2}$	$\frac{v^2}{2g} = \frac{y_c}{2}$	$\frac{v^2}{2g} > \frac{y_c}{2}$

8.3.2 Non - Rectangular Channel

- ◆ If the channel width varies with y , the specific energy must be written in the form $E = \frac{Q^2}{2gA^2} + y$ (8.15)

- ◆ The minimum energy also occurs where

$$\frac{dE}{dy} = 0 \text{ at constant } Q$$

- ◆ Since $A = A(y)$, therefore (8.15) becomes

$$1 - \frac{2Q^2A^{-3}}{2g} \frac{dA}{dy} = 0$$

$$\text{or } \frac{dA}{dy} = \frac{gA^3}{Q^2} \quad (8.16)$$

- ◆ Since $\frac{dA}{dy} = B$ - the channel width at the free surface,

$$\therefore B = \frac{gA^3}{Q^2}$$

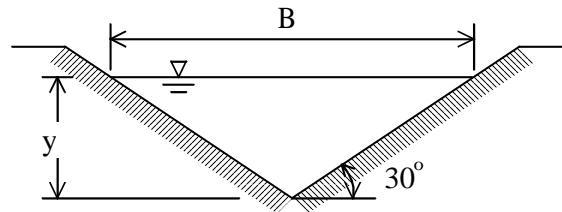
$$\text{or } A = \left(\frac{BQ^2}{g}\right)^{1/3} \quad (8.17)$$

$$\begin{aligned} v_c &= \frac{Q}{A} \\ &= \left(\frac{gA}{B}\right)^{1/2} \end{aligned} \quad (8.18)$$

- ◆ For a given channel shape, $A(y)$ & $B(y)$, and a given Q , (8.17) & (8.18) have to be solved by trial and error to find the A and then v_c .
- ◆ If a critical channel flow is also moving uniformly (at constant depth), it must correspond to a critical slope, S_c , with $y_n = y_c$. This condition can be analysed by Manning formula.

Worked examples:

1. A triangular channel with an angle of 120° made by 2 equal slopes. For a flow rate of $3 \text{ m}^3/\text{s}$, determine the critical depth and hence the maximum depth of the flow.

**Answer**

For critical flow,

$$\begin{aligned} v^2 &= g \cdot y_{\text{ave}} \\ Q^2 &= g \cdot y_{\text{ave}} \cdot A^2 \\ &= \frac{gA^3}{B} \quad \left(y_{\text{ave}} = \frac{A}{B} \right) \end{aligned}$$

For critical flow,

$$\begin{aligned} B &= 2 \cdot y \cdot \cot 30^\circ \\ \& \quad A &= y^2 \cdot \cot 30^\circ \end{aligned}$$

$$\therefore Q^2 = \frac{3g}{2} y^5$$

$$\begin{aligned} \text{Hence } y &= \left(\frac{2Q^2}{3g} \right)^{1/5} \\ &= \left(\frac{2 \cdot 3^2}{3 \cdot 9.81} \right)^{1/5} \text{ m} \\ &= \underline{0.906 \text{ m}} \end{aligned}$$

The maximum depth is 0.906 m.

~~$$\text{The critical depth, } y_c = y_{\text{ave}} = \frac{A}{B} = \frac{(B \cdot y)/2}{B} = \frac{y}{2} = \frac{0.906}{2} = 0.453 \text{ m} .$$~~