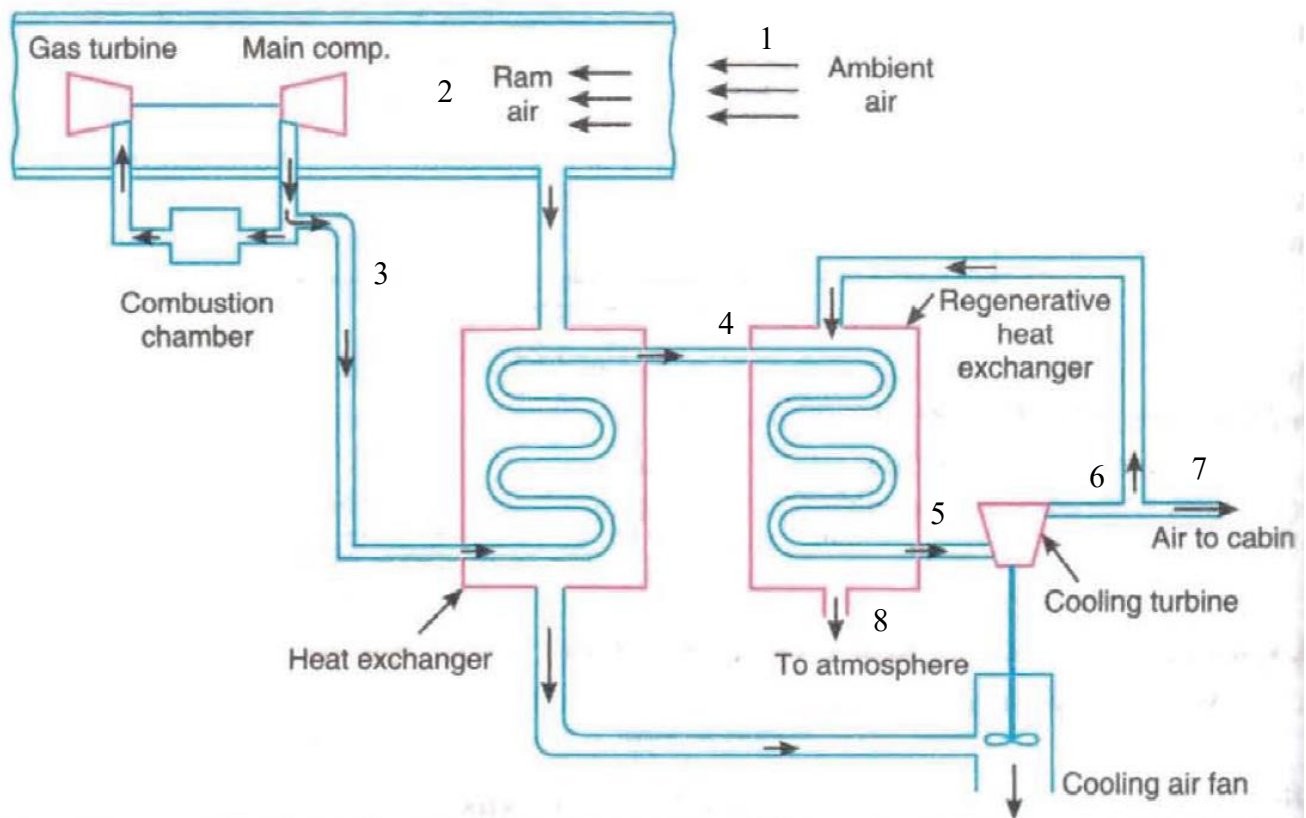
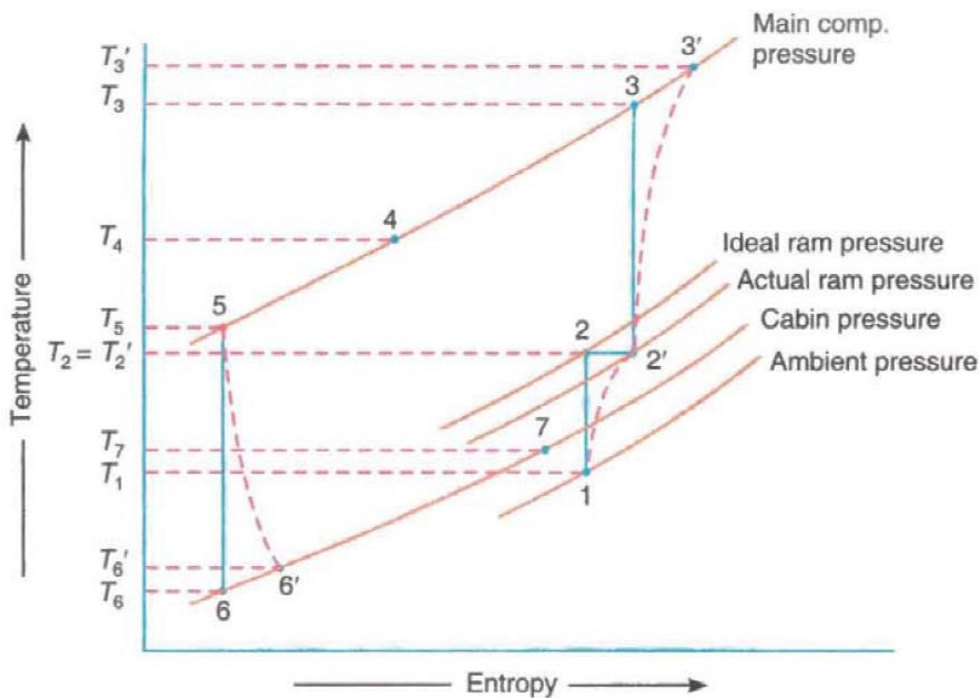


The regenerative air cooling system

The regenerative air cooling system is shown in Figure inserted below. It is a modification of a simple air cooling system with the addition of a regenerative heat exchanger. The high pressure and high temperature air from the main compressor is first cooled by the ram air in the heat exchanger. The air is further cooled in the regenerative heat exchanger with a portion of the air bled after expansion in the cooling turbine. This type of cooling system is used for supersonic aircrafts and rockets.



The T-s diagram for the regenerative air cooling system is shown in Figure inserted below. The various processes are as follows:



1. The process 1–2 represents isentropic ramming of air and process 1– 2' represents actual ramming of air because of internal friction due to irreversibilities.

2. The process 2'–3 represents isentropic compression of air in the main compressor and the process 2'–3' represents actual compression of air because of internal friction due to irreversibilities.
3. The process 3'–4 represents cooling of compressed air by ram air in the heat exchanger.
4. The process 4–5 represents cooling of air in the regenerative heat exchanger.
5. The process 5–6 represents isentropic expansion of air in the cooling turbine upto the cabin pressure and the process 5–6' represents actual expansion of air in the cooling turbine.
6. The process 6'–7 represents heating of air upto the cabin temperature T_7 .

If Q tonnes of refrigeration is the cooling load in the cabin, then the quantity of air required for the refrigeration purpose will be



$$m_a = \frac{210 Q}{c_p (T_7 - T_{6'})} \text{ kg / min}$$

Let

m_1 = Total mass of air bled from the main compressor, and

m_2 = Mass of cold air bled from the cooling turbine for regenerative heat exchanger.

For the energy balance of regenerative heat exchanger, we have

$$m_2 c_p (T_8 - T_{6'}) = m_1 c_p (T_4 - T_5)$$

$$\therefore m_2 = \frac{m_1 (T_4 - T_5)}{(T_8 - T_{6'})}$$

where

T_8 = Temperature of air leaving to atmosphere from the regenerative heat exchanger.

Power required for the refrigeration system,

$$P = \frac{m_1 c_p (T_{3'} - T_{2'})}{60} \text{ kW}$$

and C.O.P. of the refrigerating system

$$= \frac{210 Q}{m_1 c_p (T_{3'} - T_{2'})} = \frac{210 Q}{P \times 60}$$

Problem. 2: A regenerative air cooling system is used for an air plane to take 20 tonnes of refrigeration load. The ambient air at pressure 0.8 bar and temperature 10°C is rammed isentropically till the pressure rises to 1.2 bar. The air bled off the main compressor at 4.5 bar is cooled by the ram air in the heat exchanger whose effectiveness is 60%. The air from the heat exchanger is further cooled to 60°C in the regenerative heat exchanger with a portion of the air bled after expansion in the cooling turbine. The cabin is to be maintained at a temperature of 25°C and a pressure of 1 bar. If the isentropic efficiencies of the compressor and turbine are 90% and 80% respectively, find :

1. Mass of the air bled from cooling turbine to be used for regenerative cooling ;
2. Power required for maintaining the cabin at the required condition ; and
3. C.O.P. of the system.



We know that for the isentropic ramming of air (process 1-2),

$$\frac{T_2}{T_1} = \left(\frac{p_2}{p_1} \right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{1.2}{0.8} \right)^{\frac{1.4-1}{1.4}} = (1.5)^{0.286} = 1.123$$

$$\therefore T_2 = T_1 \times 1.123 = 283 \times 1.123 = 317.8 \text{ K}$$

and for the isentropic compression process 2-3,

$$\frac{T_3}{T_2} = \left(\frac{p_3}{p_2} \right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{4.5}{1.2} \right)^{\frac{1.4-1}{1.4}} = (3.75)^{0.286} = 1.46$$

$$\therefore T_3 = T_2 \times 1.46 = 317.8 \times 1.46 = 464 \text{ K}$$

Isentropic efficiency of the compressor,

$$\eta_c = \frac{\text{Isentropic increase in temp.}}{\text{Actual increase in temp.}} = \frac{T_3 - T_2}{T_{3'} - T_2}$$

$$0.9 = \frac{464 - 317.8}{T_{3'} - 317.8} = \frac{146.2}{T_{3'} - 317.8}$$

$$\therefore T_{3'} = 317.8 + 146.2 / 0.9 = 480 \text{ K}$$

We know that effectiveness of the heat exchanger (η_H),

$$0.6 = \frac{T_{3'} - T_4}{T_{3'} - T_2} = \frac{480 - T_4}{480 - 317.8} = \frac{480 - T_4}{162.2}$$

$$\therefore T_4 = 480 - 0.6 \times 162.2 = 382.7 \text{ K}$$



Now for the isentropic cooling in the cooling turbine (process 5–6),

$$\frac{T_5}{T_6} = \left(\frac{p_5}{p_6} \right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{4.5}{1} \right)^{\frac{1.4-1}{1.4}} = (4.5)^{0.286} = 1.54$$

$$\therefore T_6 = T_5 / 1.54 = 333 / 1.54 = 216 \text{ K}$$

and isentropic efficiency of the cooling turbine,

$$\eta_T = \frac{\text{Actual increase in temp.}}{\text{Isentropic increase in temp.}} = \frac{T_5 - T_{6'}}{T_5 - T_6}$$

$$0.8 = \frac{333 - T_{6'}}{333 - 216} = \frac{333 - T_{6'}}{117}$$

$$\therefore T_{6'} = 333 - 0.8 \times 117 = 239.4 \text{ K}$$

1. Mass of air bled from the cooling turbine to be used for regenerative cooling

- Let
- m_a = Mass of air bled from the cooling turbine to be used for regenerative cooling,
 - m_1 = Total mass of air bled from the main compressor, and
 - m_2 = Mass of cold air bled from the cooling turbine for regenerative heat exchanger.

We know that the mass of air supplied to the cabin,

$$\begin{aligned} m_a &= m_1 - m_2 \\ &= \frac{210 Q}{c_p (T_7 - T_{6'})} = \frac{210 \times 20}{1 (298 - 239.4)} = 71.7 \text{ kg / min} \quad (i) \end{aligned}$$