## Total settlement of pile

The total settlement of a pile under a vertical working load $Q_{W}$ is given by:
$\mathrm{S}_{\mathrm{e}}=\mathrm{S}_{\mathrm{e}(1)}+\mathrm{S}_{\mathrm{e}(2)}+\mathrm{S}_{\mathrm{e}(3)}$
$\mathrm{S}_{\mathrm{e}(1)}$ : Elastic settlement of pile
$\mathrm{S}_{\mathrm{e}(2)}$ : Settlement of pile caused by the load at the pile tip
$\mathrm{S}_{\mathrm{e}(3)}$ : Settlement of pile caused by the load transmitted along the pile shaft


If the pile material is assumed to be elastic, the deformation of the pile shaft can be evaluated, in accordance with the fundamental principles of mechanics of materials, as

$$
S_{e(1)}=\frac{\left(Q_{W b}+\xi Q_{W S}\right) L}{A_{b} E_{P}}
$$

$Q_{W b}$ : Working load at the pile base
$\mathrm{Q}_{\mathrm{ws}}$ : load carried by frictional (skin) resistance under working load condition
$A_{p}$ : Area of cross section of pile.
L: length of pile
$\mathrm{E}_{\mathrm{P}}$ : modulus of elasticity of the pile material
The magnitude of varies between 0.5 and 0.67 and will depend on the nature of the distribution of the unit friction (skin) resistance $f$ along the pile shaft.
The settlement of a pile caused by the load carried at the pile end may be expressed in the form:

$$
S_{e(2)}=\frac{q_{W b} D}{E_{S}}\left(1-\mu_{S}^{2}\right) I_{W b}
$$

Where:
D: width or diameter of pile.
$q_{W b}$ : Base load per unit area $=\frac{Q_{W b}}{A_{b}}$
$E_{s}$ : Modulus of elasticity of the soil at or under the base
$\mu_{s}$ : Poisson's ratio of soil.
$I_{W b}$ : Influence factor $\approx 0.85$
The settlement of a pile caused by the load carried by the pile shaft is given by a relation

$$
S_{e(3)}=\left(\frac{Q_{W S}}{P L}\right) \frac{D}{E_{S}}\left(1-\mu_{S}^{2}\right) I_{W S}
$$

Where
$I_{W S}$ : is influence factor.

$$
I_{W S}=2+0.35 \sqrt{\frac{L}{D}}
$$

Table 1 Typical prestressed concrete pile in use

| Pile shape ${ }^{\text {a }}$ | $\underset{(\mathrm{mm})}{D}$ | Area of cross section (cm ${ }^{2}$ ) | Perimeter (mm) | Number of strands |  | Minimum effective prestress force (kN) | $\begin{gathered} \text { Section } \\ \text { modulus } \\ \left(\mathrm{m}^{3} \times 10^{-3}\right) \end{gathered}$ | Design bearing capacity (kN) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Strength of concrete (MN/m²) |  |
|  |  |  |  | 12.7 -mm | 11.1-mm |  |  |  |
|  |  |  |  | diameter | diameter | 34.5 |  | 41.4 |
| S | 254 | 645 | 1016 | 4 | 4 | 312 |  | 2.737 | 556 | 778 |
| O | 254 | 536 | 838 | 4 | 4 | 258 | 1.786 | 462 | 555 |
| S | 305 | 929 | 1219 | 5 | 6 | 449 | 4.719 | 801 | 962 |
| O | 305 | 768 | 1016 | 4 | 5 | 369 | 3.097 | 662 | 795 |
| S | 356 | 1265 | 1422 | 6 | 8 | 610 | 7.489 | 1091 | 1310 |
| O | 356 | 1045 | 1168 | 5 | 7 | 503 | 4.916 | 901 | 1082 |
| S | 406 | 1652 | 1626 | 8 | 11 | 796 | 11.192 | 1425 | 1710 |
| O | 406 | 1368 | 1346 | 7 | 9 | 658 | 7.341 | 1180 | 1416 |
| S | 457 | 2090 | 1829 | 10 | 13 | 1010 | 15.928 | 1803 | 2163 |
| O | 457 | 1729 | 1524 | 8 | 11 | 836 | 10.455 | 1491 | 1790 |
| S | 508 | 2581 | 2032 | 12 | 16 | 1245 | 21.844 | 2226 | 2672 |
| O | 508 | 2136 | 1677 | 10 | 14 | 1032 | 14.355 | 1842 | 2239 |
| S | 559 | 3123 | 2235 | 15 | 20 | 1508 | 29.087 | 2694 | 3232 |
| O | 559 | 2587 | 1854 | 12 | 16 | 1250 | 19.107 | 2231 | 2678 |
| S | 610 | 3658 | 2438 | 18 | 23 | 1793 | 37.756 | 3155 | 3786 |
| O | 610 | 3078 | 2032 | 15 | 19 | 1486 | 34.794 | 2655 | 3186 |

${ }^{\mathrm{a}} \mathrm{S}=$ square section; $\mathrm{O}=$ octagonal section


## Example:

The allowable working load on a prestressed concrete pile 21-m long that has been driven into sand is 502 kN . The pile is octagonal in shape with $\mathrm{D}=356 \mathrm{~mm}$. Skin resistance carries 350 kN of the allowable load, and point bearing carries the rest. Use $E_{P}=21 * \frac{10^{6} \mathrm{KN}}{m 2}, E_{S}=25 * 10^{3} \mathrm{KN} / \mathrm{m} 2, \mu_{s}=0.35$ and $\xi=0.65$. Determine the settlement of the pile.
Ans:

$$
S_{e(3)}=\left(\frac{Q_{W S}}{P L}\right) \frac{D}{E_{S}}\left(1-\mu_{S}^{2}\right) I_{W S}
$$

$$
\begin{aligned}
& S_{e(\mathbf{1})}=\frac{\left(Q_{W b}+\xi Q_{W S}\right) L}{A_{b} E_{P}} \\
& \text { For } \mathrm{D}=356 \mathrm{~mm} 2, A_{b}=1045 \mathrm{~mm} 2, \mathrm{P}=1.168 \mathrm{~m} \\
& Q_{u}=502 \mathrm{KN} \text {, and } Q_{w s}=350 \mathrm{KN} \text {, therefore } Q_{w b}=152 \mathrm{KN} \\
& S_{e(1)}=\frac{\left(Q_{W b}+\xi Q_{W S}\right) L}{A_{b} E_{P}}=\frac{(152+0.65 * 350) 21 \mathrm{~m}}{0.1045 * 21 * 10^{6} \mathrm{KN} / \mathrm{m} 2}=3.63 \mathrm{~mm} \\
& S_{e(2)}=\frac{q_{W b} D}{E_{S}}\left(1-\mu_{S}^{2}\right) I_{W b} \\
& q_{w b}=\frac{Q_{w b}}{A_{b}}=\frac{152 \mathrm{KN}}{0.1045 \mathrm{M} 2}=1454.5 \mathrm{KN} / \mathrm{m} 2, I_{w b}=0.85 \\
& S_{e(2)}=\frac{1454.5 * 0.356}{25 * 10^{3}}\left(1-0.35^{2}\right) 0.85=15.5 \mathrm{~mm}
\end{aligned}
$$

$I_{W S}=2+0.35 \sqrt{\frac{L}{D}}=2+0.35 \sum \frac{21}{0.356}=4.688$
$S_{e(3)}=\left(\frac{350}{1.168 * 21}\right) \frac{0.356}{25 * 10^{3}}\left(1-0.35^{2}\right) 4.688=0.83 \mathrm{~mm}$
$\mathbf{S}_{\mathrm{e}}=\mathbf{S}_{\mathrm{e}(\mathbf{1})}+\mathbf{S}_{\mathrm{e}(\mathbf{2})}+\mathbf{S}_{\mathrm{e}(\mathbf{3})}$
$S_{e}=3.63+15.5+0.83=19.96>25 \mathrm{~mm}$ ok
Problems:

## Problem1:

A concrete pile is 18 m long and has a cross section of $0.406 \mathrm{~m} * 0.406 \mathrm{~m}$. The pile is embedded in a sand having $\gamma=16 \mathrm{kN} / \mathrm{m} 3$ and $\varnothing=37^{\circ}$. The allowable working load is 900 kN . If 600 kN are contributed by the frictional resistance and 300 kN are from the base load, determine the elastic settlement of the pile. Given: $E_{P}=2.1 * \frac{10^{6} \mathrm{KN}}{m 2}, E_{s}=30 * 10^{3} \mathrm{KN} / \mathrm{m} 2, \mu_{s}=0.38$ and $\xi=0.57$.
Problem2:
Solve Problem 1 with the following: length of pile $=15 \mathrm{~m}$, pile cross section $=0.305 \mathrm{~m} * 0.305 \mathrm{~m}$, allowable working load $=338$ kN , contribution of frictional resistance to working load $=280 \mathrm{kN}, \quad E_{p}=21^{*} 10^{6} \mathrm{KN} / \mathrm{m} 2, \quad E_{s}=30,000 \mathrm{KN} / \mathrm{m} 2 . \mu_{s}=0.3$ and $\xi=0.62$.

