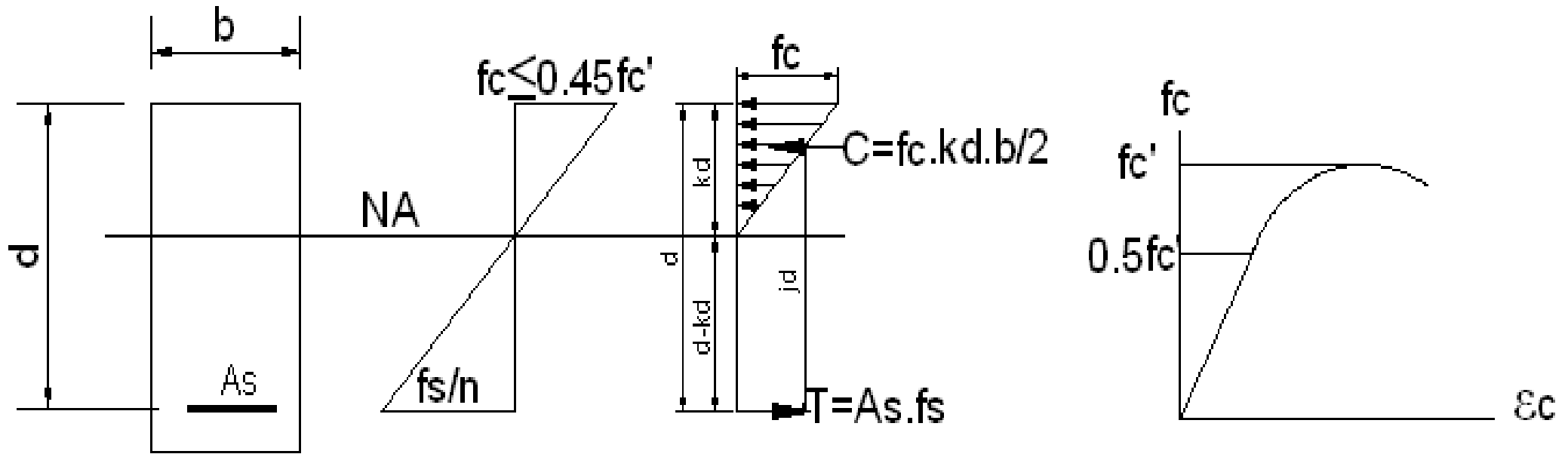


# Working Stress Design Method

## Singly Reinforced Concrete beams:



Based on cracked-elastic section:

$$[ f_{ct} \geq f_r = 0.62\sqrt{f_c'} , \quad f_{c_{comp}} \leq 0.5f_c' ]$$

$$f_{c_{comp}} \leq 0.45f_c'$$

$$f_s \leq 0.5f_y \neq \begin{cases} 140MPa & \text{for } f_y = 300MPa \\ 170MPa & \text{for } f_y = 400MPa \end{cases}$$

$$n = \frac{Es}{Ec}$$

$$\sum M_{NA}$$

$$b \cdot kd \cdot \frac{kd}{2} = n \cdot As \cdot (d - kd),$$

$$\rho = \frac{As}{bd}$$

$$b \cdot \frac{(kd)^2}{2} = n \cdot \rho b d \cdot (d - kd)$$

$$b \cdot \frac{(kd)^2}{2} = n \cdot \rho b d^2 \cdot (1 - k)$$

$$\frac{(k)^2}{2} = n\rho - n\rho k$$

$$(k)^2 + 2n\rho k - 2n\rho = 0 \rightarrow k = \sqrt{(n\rho)^2 + 2n\rho} - n\rho$$

$$C = \frac{fckdb}{2}$$

$$T = A_s f_s$$

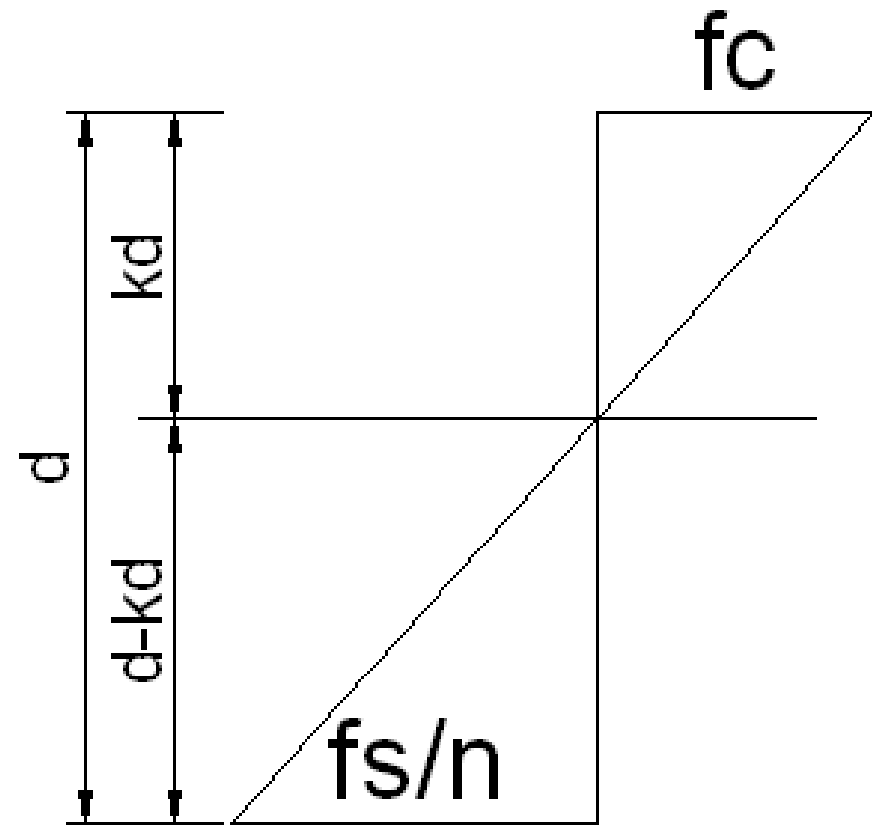
$$M_c = C \cdot jd = \frac{fckdb}{2} \cdot jd$$

$$M_c = C \cdot jd = \frac{f_c \cdot k_j \cdot b \cdot d^2}{2}$$

$$M_s = T \cdot jd = A_s \cdot f_s \cdot jd$$

$$jd = d - \frac{jd}{3} \rightarrow j = 1 - \frac{k}{3}$$

$$\frac{f_c}{k d} = \frac{f_c + \frac{f_s}{n}}{d} \rightarrow k = \frac{1}{1 + \frac{f_s}{n f_c}}$$



Ex1:

If  $M=150\text{kN.m}$ ,  $n=8$ ,  $A_s=4000\text{mm}^2$ ,  $d=500\text{mm}$ ,  $b=300\text{mm}$ ,  
find stresses in steel and concrete.

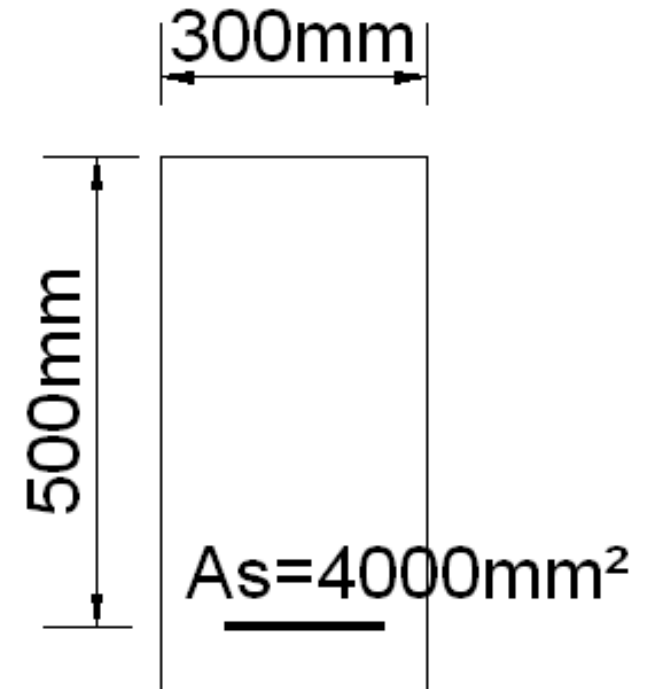
Solution:

$$\rho = \frac{4000}{300 * 500} = 0.0267$$

$$k = \sqrt{(n\rho)^2 + 2n\rho} - n\rho$$

$$k = \sqrt{(8 * 0.0267)^2 + 2 * 8 * 0.0267} - 8 * 0.0267 = 0.474$$

$$j = 1 - \frac{k}{3} = 1 - \frac{0.474}{3} = 0.842$$



$$M = \frac{f_c \cdot k_j \cdot b \cdot d^2}{2} \rightarrow f_c = \frac{2M}{k_j \cdot b \cdot d^2}$$

$$= \frac{2 * 150 * 10^{-3}}{0.474 * 0.842 * 0.3 * 0.5^2} = 10MPa$$

$$M = A_s \cdot f_s \cdot j \cdot d \rightarrow f_s = \frac{M}{A_s \cdot j \cdot d} = \frac{150 * 10^{-3}}{4000 * 10^{-6} * 0.842 * 0.5}$$
$$= 89MPa$$

Ex2:

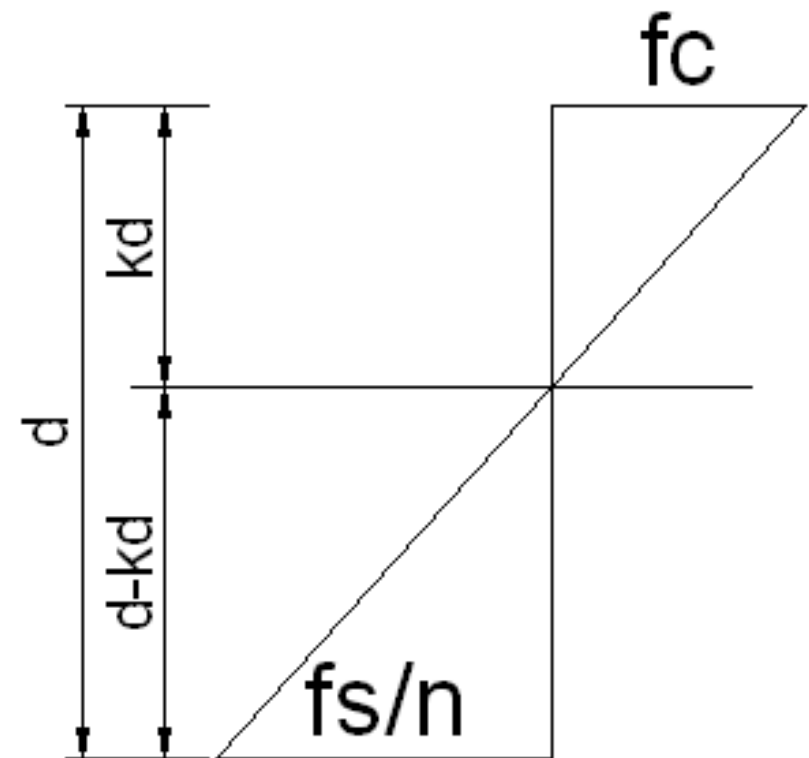
For data given in Ex1, if  $f_c' = 30\text{MPa}$ ,  $f_{s\text{allowable}} = 140\text{MPa}$ , find moment capacity of the beam.

Solution:

$$f_{c\text{allowable}} = 0.45f_c' = 0.45 * 30 = 13.5\text{MPa}$$

assume steel failure  $f_s = 140\text{MPa}$

$$\begin{aligned} \frac{f_c}{kd} &= \frac{\frac{f_s}{n}}{d - kd} \rightarrow \frac{f_c}{0.474 * 500} \\ &= \frac{\frac{140}{8}}{500 - 0.474 * 500} \end{aligned}$$



$$f_c = 15.8 \text{ MPa} > f_{c_{allow}} = 13.5 \text{ MPa} \rightarrow$$

$\therefore$  concrete failure,  $f_c = 13.5 \text{ MPa}$

$$\frac{f_c}{kd} = \frac{\frac{f_s}{n}}{d - kd} \rightarrow \frac{13.5}{0.474 * 500} = \frac{\frac{f_s}{8}}{500 - 0.474 * 500}$$

$$f_s = 120 \text{ MPa} < f_{s_{allow}} = 140 \text{ MPa}$$

$$M_c = C \cdot jd = \frac{f_c \cdot k \cdot j \cdot b \cdot d^2}{2} = \frac{13.5 * 0.474 * 0.842 * 0.3 * 0.5^2}{2}$$

$$= 0.202 \text{ MN} \cdot \text{m}$$

$$\text{OR } M_s = T \cdot jd = A_s \cdot f_s \cdot jd = 4000 * 10^{-6} ** 120 * 0.842 * 0.5 = 0.202 \text{ MN} \cdot \text{m}$$



### Ex3: Design of concrete beam.

If  $M=300\text{kN.m}$ ,  $f_c'=30\text{MPa}$ ,  $f_s=140\text{MPa}$ ,  $n=10$ ,  $f_y=300\text{MPa}$ .

Solution:

$$f_{c_{\text{allowable}}}=0.45f_c'=0.45*30=13.5\text{MPa}$$

$$k = \frac{1}{1 + \frac{f_s}{n f_c}} = \frac{1}{1 + \frac{140}{10*13.5}} = 0.49 \quad \text{balanced failure}$$

$$j = 1 - \frac{k}{3} = 1 - \frac{0.49}{3} = 0.84$$

$$M = \frac{f_c \cdot k \cdot j \cdot b \cdot d^2}{2} \rightarrow 0.3 = \frac{13.5 * 0.49 * 0.84 * b d^2}{2} \rightarrow b d^2$$
$$= 108 * 10^{-3} m^3$$

Assume  $d=2b \rightarrow b=d/2$

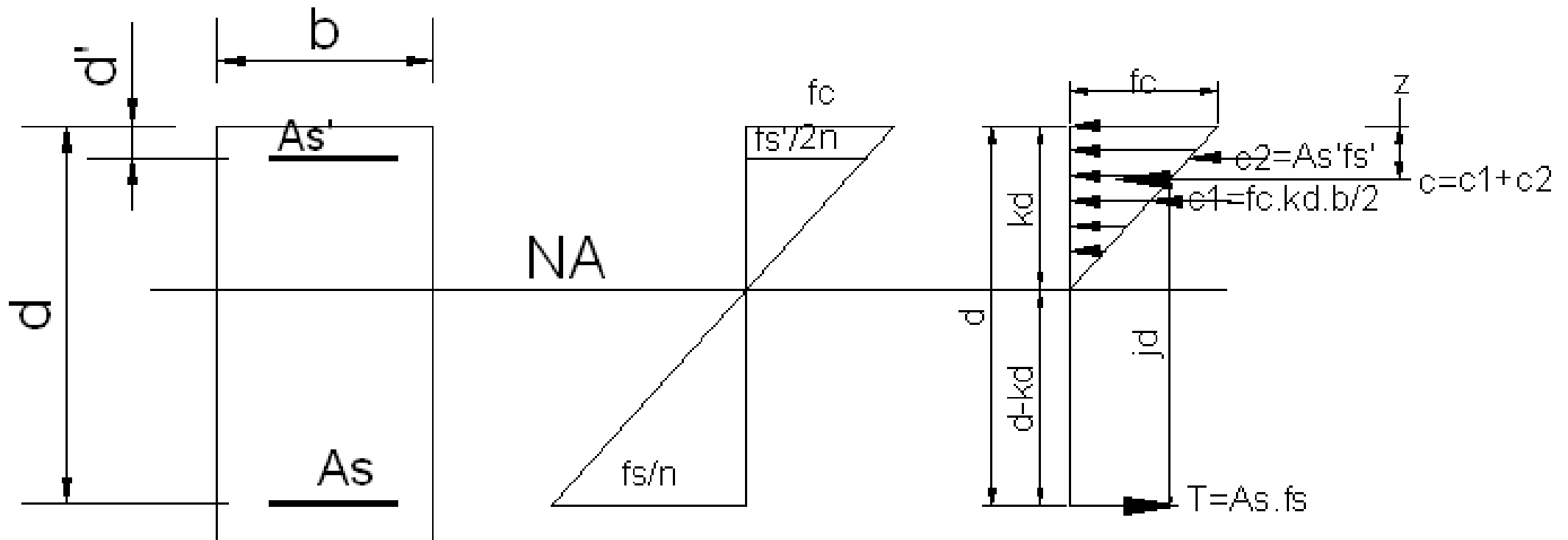
$$\frac{d^3}{2} = 108 * 10^{-3} \rightarrow d = 600mm, \quad b = 300mm$$

$$M = A_s \cdot f_s \cdot j \cdot d \rightarrow 0.3 = A_s * 140 * 0.84 * 0.5 \rightarrow A_s \\ = 4251mm^2$$

use  $7\emptyset 28 = 4312mm^2$

$$\rho = \frac{4251}{300 * 600} = 0.0226 > \rho_{min} = \frac{1.4}{300} = 0.0046 \text{ O.K}$$

# Doubly Reinforced Beams:



$$A_{s'} \xrightarrow{\text{transformed to concrete}} (2n - 1)A_{s'}$$

$$A \xrightarrow{\text{transformed to concrete}} nA_s$$

$$\sum M_{NA}$$

$$b * kd * \frac{kd}{2} + (2n - 1)As' * (kd - d') = nAs(d - kd)$$

$$\rho = \frac{As}{bd}, \quad \rho' = \frac{As'}{bd}$$

$$\frac{b(kd)^2}{2} + (2n - 1)\rho'bd(kd - d') = n\rho bd(d - kd)$$

$$k = \sqrt{2(2n - 1)\rho' \frac{d'}{d} + 2n\rho + n^2(2\rho' + \rho - \frac{\rho'}{n})^2 - n(2\rho' + \rho - \frac{\rho'}{n})}$$

If  $As' = 2n\rho'bd$

$$k = \sqrt{2n(\rho' \frac{d'}{d} + \rho) + n^2(\rho' + \rho)^2 - n(\rho' + \rho)}$$

$jd = d - z \rightarrow j = 1 - z/d$

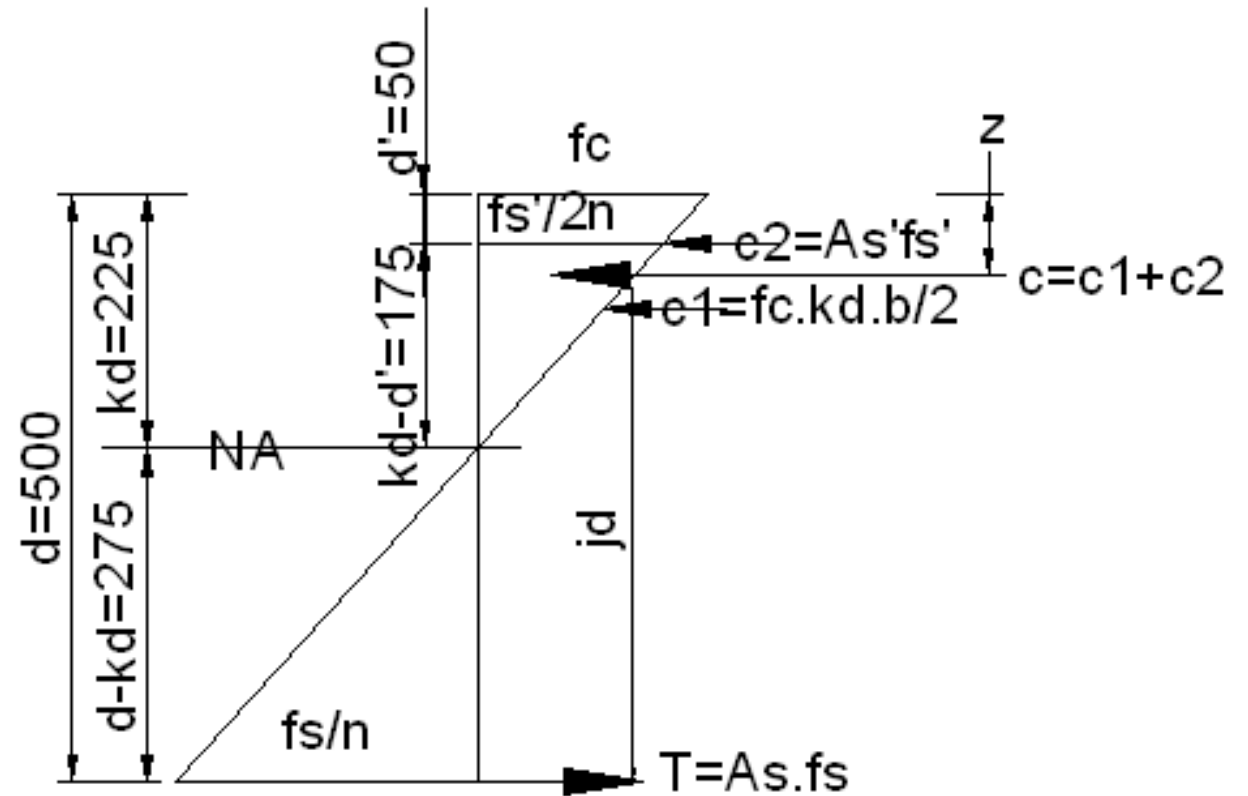
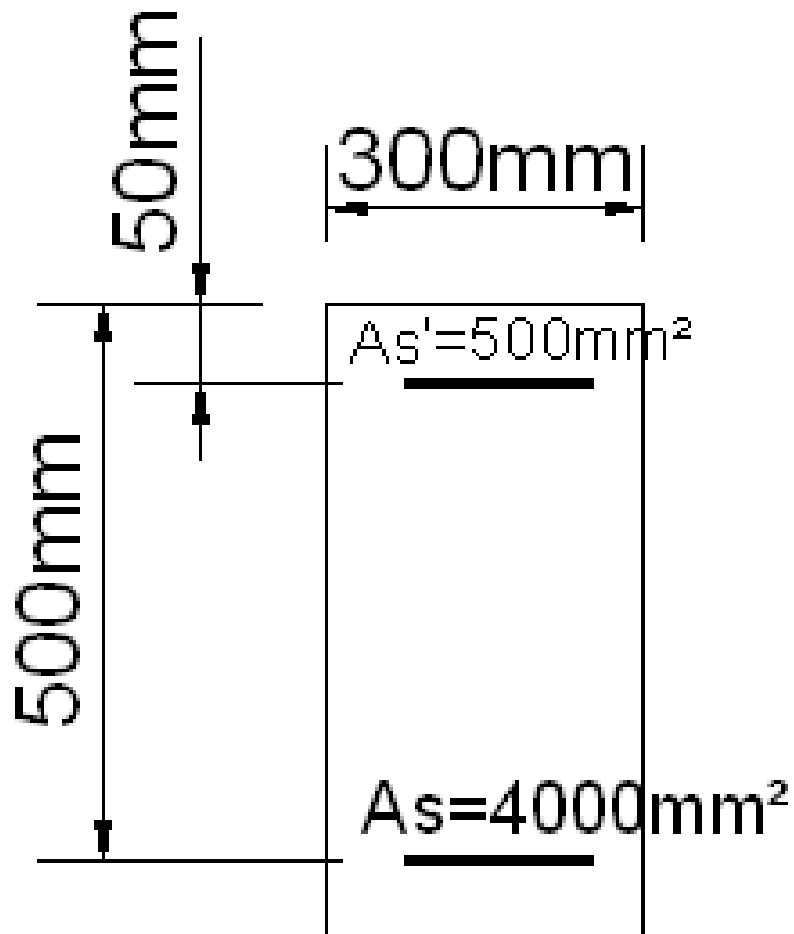
$M_s = A_s f_s jd$

$$M_c = (c_1 + c_2)(d - z) = \left( \frac{f_c k d b}{2} + A_s' f_s' \right) (d - z)$$

$$z = \frac{\frac{d}{6} k^2 + \rho' (2n - 1) \left(1 - \frac{d'}{kd}\right) d'}{\frac{k}{2} + \rho' (2n - 1) \left(1 - \frac{d'}{kd}\right)}$$

Ex1:

If  $M=150\text{kN.m}$ ,  $n=8$ , find  $f_s'$ ,  $f_s$ ,  $f_c$



Solution:

$$\rho = \frac{A_s}{bd} = \frac{4000}{300 * 500} = 0.027, \quad \rho' = \frac{A_s'}{bd} = \frac{500}{300 * 500}$$
$$= 0.0033$$

$$k = \sqrt{2(2n - 1)\rho' \frac{d'}{d} + 2n\rho + n^2(2\rho' + \rho - \frac{\rho'}{n})^2 - n(2\rho' + \rho - \frac{\rho'}{n})}$$



$$k = \left[ 2(2 * 8 - 1) * 0.0033 * \frac{50}{500} + 2 * 8 * 0.027 + 8^2 \left( 2 * 0.0033 + 0.027 - \frac{0.0033}{8} \right)^2 \right]^{\frac{1}{2}} - 8 \left( 2 * 0.0033 + 0.027 - \frac{0.0033}{8} \right) = 0.45$$

$$kd = 0.45 * 500 = 225 \text{ mm}$$

$$\frac{f_c}{kd} = \frac{\frac{f_{s'}}{2n}}{kd - d'} \rightarrow \frac{f_c}{225} = \frac{\frac{f_{s'}}{2 * 8}}{175} \rightarrow f_{s'} = 12.44 f_c$$

$$c1 = \frac{f_c * kd * b}{2} = \frac{f_c * 0.225 * 0.3}{2} = 0.03375 f_c$$

$$c2 = A_{s'} f_{s'} = 500 * 10^{-6} * 12.44 f_c = 6.22 * 10^{-3} f_c$$

$$c = c1 + c2 = 0.03375fc + 6.22 * 10^{-3}fc = 0.03997fc$$

$$\sum M_{top\ fiber} = 0$$

$$c1 * \frac{kd}{3} + c2 * d' = c * z$$

$$z = \frac{c1 * \frac{kd}{3} + c2 * d'}{c}$$

$$= \frac{0.03375fc * \frac{0.225}{3} + 6.22 * 10^{-3}fc * 0.05}{0.03997fc} = 0.0711m$$

OR

$$z = \frac{\frac{d}{6} k^2 + \rho'(2n - 1)\left(1 - \frac{d'}{kd}\right)d'}{\frac{k}{2} + \rho'(2n - 1)\left(1 - \frac{d'}{kd}\right)}$$

$$= 71.1 \text{ mm}$$

$$jd = d - z = 500 - 71.1 = 428.9 \text{ mm}$$

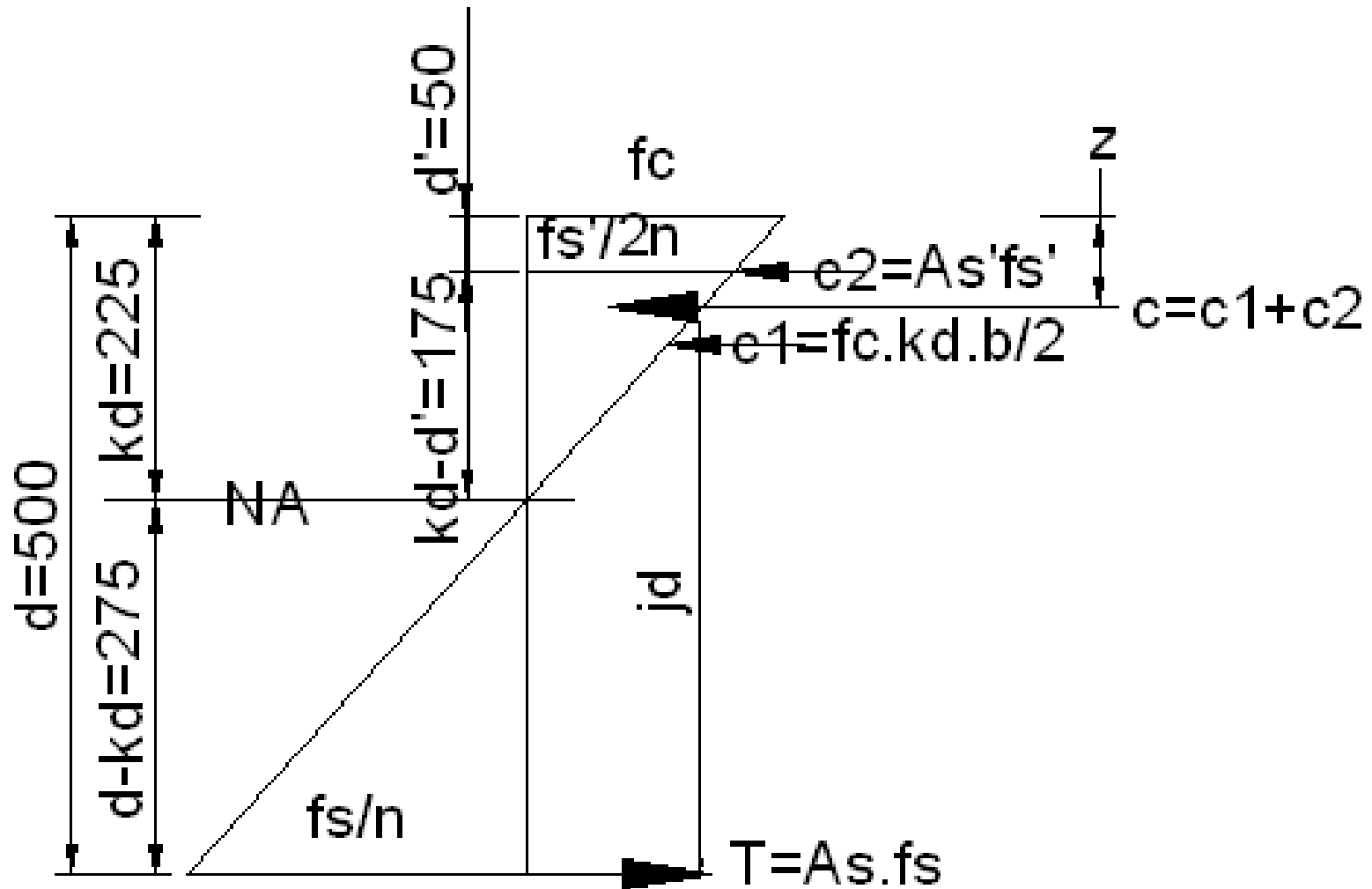
$$M = A_s f_s j d \rightarrow f_s = \frac{150 * 10^{-3}}{4000 * 10^{-6} * 0.4289} = 87.43 \text{ MPa}$$

$$M_c = c \cdot j d \rightarrow 150 * 10^{-3} = 0.03997 f_c * 0.4289 \rightarrow f_c = 8.75 \text{ MPa}$$

$$f_s' = 12.44 f_c = 12.44 * 8.75 = 108.85 \text{ MPa}$$

## EX2:

For data given in ex1, if  $f_s=140\text{MPa}$ ,  $f_c'=25\text{MPa}$ ,  $n=8$ , find moment capacity.



Solution:

Assume steel failure,  $f_s=140\text{MPa}$

$$\frac{f_c}{kd} = \frac{\frac{f_s}{n}}{d - kd} \rightarrow \frac{f_c}{225} = \frac{\frac{140}{8}}{275} \rightarrow f_c = 14.3\text{MPa} > f_{c_{all}}$$
$$= 0.45 * 25 = 11.25\text{MPa} \rightarrow \therefore \text{concrete failure}$$

$$\frac{f_c}{kd} = \frac{\frac{f_s}{n}}{d - kd} \rightarrow \frac{11.25}{225} = \frac{\frac{f_s}{8}}{275} \rightarrow f_s = 110\text{MPa} > f_{s_{all}}$$
$$= 140\text{MPa}$$

$$\frac{f_c}{kd} = \frac{\frac{fs'}{2n}}{d - d'} \rightarrow \frac{11.25}{225} = \frac{\frac{fs'}{2*8}}{175} \rightarrow fs' = 140MPa = fs_{all}$$
$$= 140MPa$$

$$M = Asfsjd = 4000 * 10^{-6} * 110 * 10^3 * 0.4289$$
$$= 189 kN.m$$

OR

$$M = cjd = 0.03997fc.jd = 0.03997 * 11.25 * 10^3 * 0.4289$$
$$= 189kN.m$$

Ex3:

If  $M=300\text{kN.m}$ ,  $f_c'=30\text{MPa}$ ,  $f_s=140\text{MPa}$ ,  $n=8$ , design beam for flexure.

Solution:

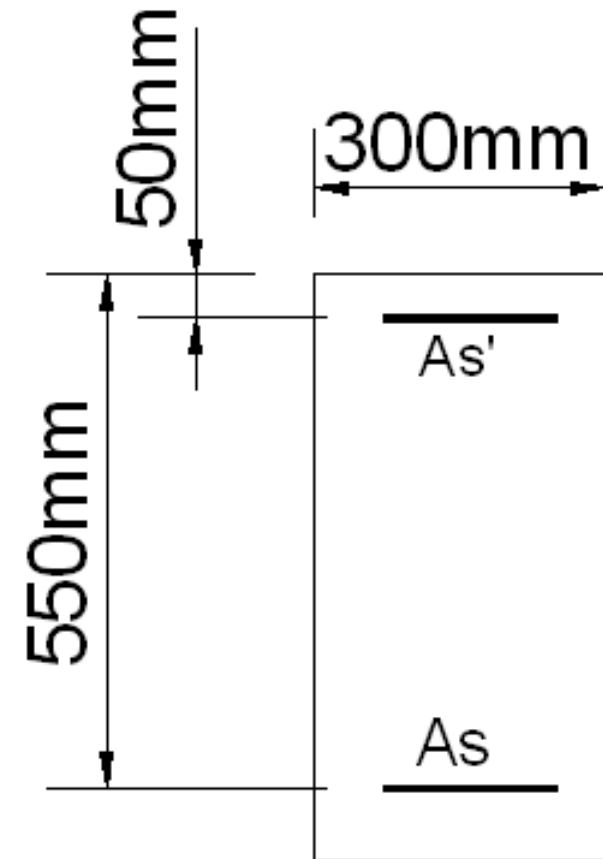
Assume singly RC beam and balanced failure

$$f_{c \text{ allowable}} = 0.45 * 30 = 13.5 \text{MPa}$$

$$k = \frac{1}{1 + \frac{f_s}{n f_c}} = \frac{1}{1 + \frac{140}{8 * 13.5}} = 0.44$$

$$k d = 0.44 * 550 = 242 \text{mm}$$

$$j = 1 - k/3 = 1 - 0.44/3 = 0.85$$



$$jd = 0.85 * 550 = 467 \text{ mm}$$

$$M = \frac{f_c \cdot k \cdot d \cdot b \cdot jd}{2} \rightarrow 0.3 = \frac{f_c * 0.242 * 0.3 * 0.467}{2} \rightarrow f_c$$

$$= 17.6 \text{ MPa} > f_{c_{all}} = 13.5 \text{ MPa} \rightarrow$$

*\therefore compression reinforcement is required*

$$M = A_s f_s j d$$

$$0.3 = A_s * 140 * 0.467 \rightarrow A_s = 4.584 * 10^{-3} \text{ m}^2$$
$$= 4584 \text{ mm}^2$$



$$M_c = \frac{f_c \cdot k_d \cdot b \cdot j d}{2} = \frac{13.5 * 10^3 * 0.242 * 0.3 * 0.467}{2}$$

$$= 229 \text{ kN.m}$$

$$M' = M_t - M_c = 300 - 229 = 71 \text{ kN.m}$$

$$M' = A_s' f_s' (d - d') \rightarrow A_s' = \frac{71}{140 * 10^3 * (0.55 - 0.05)}$$

$$= 1.014 * 10^{-3} \text{ m}^2 = 1014 \text{ mm}^2$$

*use 9Ø25 + 1Ø20 = 4733 mm<sup>2</sup> tension reinf.*

*use 4Ø20 = 1256 mm<sup>2</sup> compression reinf.*

$$\rho = \frac{A_s}{bd} = \frac{4733}{300 * 550} = 0.0287, \quad \rho' = \frac{A_s'}{bd} = \frac{1256}{300 * 550}$$

$$= 0.0076$$

$$k = \sqrt{2(2n - 1)\rho' \frac{d'}{d} + 2n\rho + n^2(2\rho' + \rho - \frac{\rho'}{n})^2 - n(2\rho' + \rho - \frac{\rho'}{n})}$$

$$k = \left[ 2(2 * 8 - 1) * 0.0076 * \frac{50}{500} + 2 * 8 * 0.0287 + 8^2 \left( 2 * 0.0076 + 0.0287 - \frac{0.0076}{8} \right)^2 \right]^{\frac{1}{2}} - 8 \left( 2 * 0.0076 + 0.0287 - \frac{0.0076}{8} \right) = 0.429$$

$$kd = 0.429 * 550 = 236 \text{ mm}$$

$$z = \frac{\frac{d}{6} k^2 + \rho'(2n - 1) \left(1 - \frac{d'}{kd}\right) d'}{\frac{k}{2} + \rho'(2n - 1) \left(1 - \frac{d'}{kd}\right)}$$

$$z = \frac{\frac{550}{6} * 0.429^2 + 0.0076(2 * 8 - 1) \left(1 - \frac{50}{236}\right) * 50}{\frac{0.429}{2} + 0.0076(2 * 8 - 1) \left(1 - \frac{50}{236}\right)}$$

$$= 70.2 \text{ mm}$$

$$jd = d - z = 550 - 70.2 = 480 \text{ mm}$$

$$M = A_s f_s j d \rightarrow f_s = \frac{M}{A_s j d} = \frac{0.3}{4733 * 10^{-6} * 0.48} = 132 \text{ MPa}$$

$$< f_{s_{all}} = 140 \text{ MPa O.K}$$

$$\frac{\frac{f_s}{n}}{d - kd} = \frac{f_c}{kd} \rightarrow \frac{\frac{132}{8}}{550 - 236} = \frac{f_c}{236} \rightarrow f_c = 12.4 \text{MPa} < f_{c_{all}}$$

$$= 13.5 \text{MPa O.K}$$

$$\frac{\frac{f_{s'}}{2n}}{kd - d'} = \frac{f_c}{kd} \rightarrow \frac{\frac{f_{s'}}{2 \cdot 8}}{236 - 50} = \frac{f_c}{236} \rightarrow f_{s'} = 156.4 \text{MPa}$$

$$> f_{s_{all}} = 140 \text{MPa N.G}$$

Increase  $A_{s'}$  gradually, till  $f_{s'} \leq f_{s_{all}}$

use  $2\emptyset 25 + 2\emptyset 22 = 1740 \text{mm}^2$  compression reinf.

$$\rho = \frac{A_s}{bd} = \frac{4733}{300 * 550} = 0.0287, \quad \rho' = \frac{A_s'}{bd} = \frac{1740}{300 * 550}$$

$$= 0.0105$$

$$k = \sqrt{2(2n - 1)\rho' \frac{d'}{d} + 2n\rho + n^2(2\rho' + \rho - \frac{\rho'}{n})^2 - n(2\rho' + \rho - \frac{\rho'}{n})}$$

$$k = \left[ 2(2 * 8 - 1) * 0.0105 * \frac{50}{500} + 2 * 8 * 0.0287 + 8^2 \left( 2 * 0.0105 + 0.0287 - \frac{0.0105}{8} \right)^2 \right]^{\frac{1}{2}} - 8 \left( 2 * 0.0105 + 0.0287 - \frac{0.0105}{8} \right) = 0.411$$

$$kd = 0.411 * 550 = 226 \text{mm}$$

$$z = \frac{\frac{d}{6} k^2 + \rho'(2n - 1) \left( 1 - \frac{d'}{kd} \right) d'}{\frac{k}{2} + \rho'(2n - 1) \left( 1 - \frac{d'}{kd} \right)}$$

$$z = \frac{\frac{550}{6} * 0.411^2 + 0.0105(2 * 8 - 1) \left(1 - \frac{50}{226}\right) * 50}{\frac{0.411}{2} + 0.0105(2 * 8 - 1) \left(1 - \frac{50}{226}\right)}$$

$$= 65.8 \text{ mm}$$

$$jd = d - z = 550 - 65.8 = 484 \text{ mm}$$

$$M = A_s f_s j d \rightarrow f_s = \frac{M}{A_s j d} = \frac{0.3}{4733 * 10^{-6} * 0.484}$$

$$= 131 \text{ MPa} < f_{s \text{ all}} = 140 \text{ MPa O.K}$$

$$\frac{\frac{f_s}{n}}{d - kd} = \frac{f_c}{kd} \rightarrow \frac{\frac{131}{8}}{550 - 226} = \frac{f_c}{226} \rightarrow f_c = 11.42 \text{ MPa}$$

$$< f_{c \text{ all}} = 13.5 \text{ MPa O.K}$$

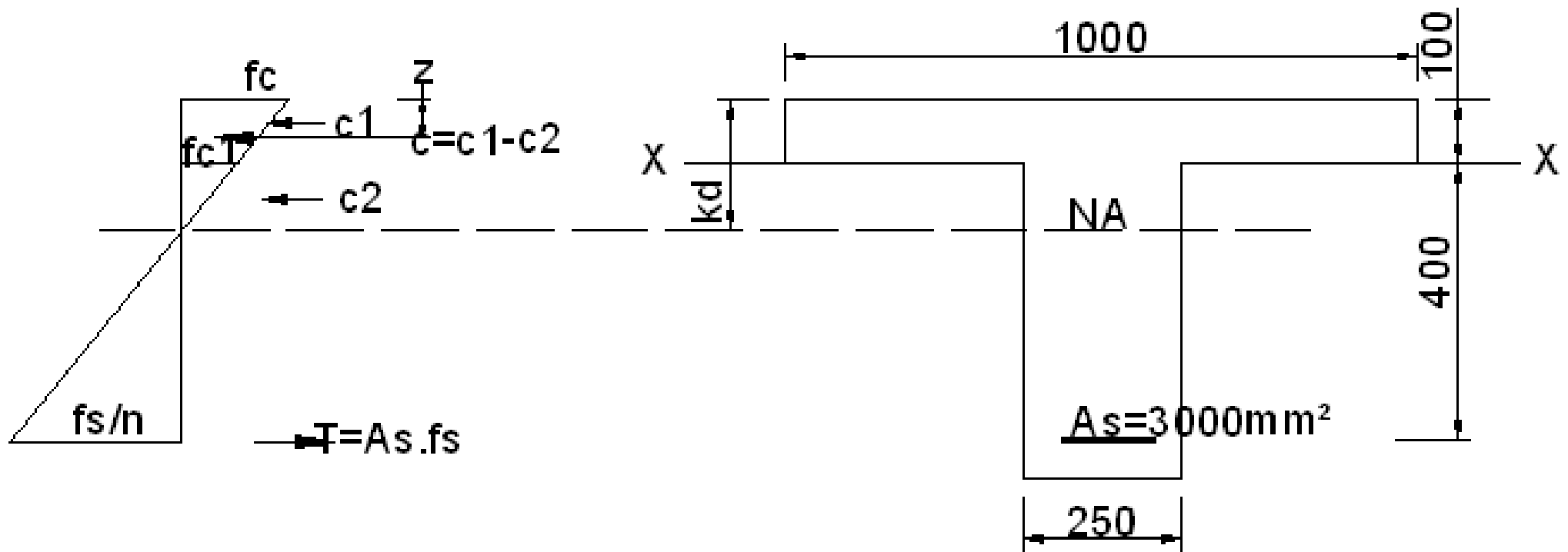


$$\frac{\frac{f_s'}{2n}}{kd - d'} = \frac{fc}{kd} \rightarrow \frac{\frac{f_s'}{2*8}}{226 - 50} = \frac{fc}{226} \rightarrow f_s' = 140MPa \leq f_{s_{all}}$$
$$= 140MPa \text{ O.K}$$

## T-Beam Section:

EX1:

If  $M=200\text{kN.m}$ ,  $n = \frac{E_s}{E_c} = 12$ , find  $f_c$  and  $f_s$ .



Solution:

Assume N.A at x-axis

$$\sum M_{x-x}$$

$$\text{moment of comp. area} = 1000 * 100 * \frac{100}{2} = 5 * 10^6 \text{mm}^3$$

$$\text{moment of ten. area} = 12 * 3000 * 400 = 14.4 * 10^6 \text{mm}^3$$

Since *moment of ten. area* > *moment of comp. area* →

*NA within web*

$$\sum M_{NA} = 0$$

$$1000 * kd * \frac{kd}{2} - (kd - 100)(1000 - 250)\left(\frac{kd - 100}{2}\right)$$

$$= nAs(d - kd)$$

$$1000 * \frac{kd^2}{2} - (kd - 100)^2 * 375 = 12 * 3000(500 - kd)$$

$$\rightarrow kd = 165\text{mm} > hf$$

$$c1 = \frac{fc}{2} * kd * b = \frac{fc}{2} * 165 * 1000 = 82500fc$$

$$\frac{fc}{kd} = \frac{fc1}{kd - hf} \rightarrow \frac{fc}{165} = \frac{fc1}{165 - 100} \rightarrow fc1 = 0.39fc$$

$$c2 = \frac{0.39fc}{2} * (kd - hf)(b - bw)$$

$$= \frac{0.39fc}{2} * (165 - 100)(1000 - 250) = 9506fc$$

$$c = c1 - c2 = 82500fc - 9506fc = 72994fc$$

$$\sum M_{top\ fiber} = 0$$

$$c1 * \frac{kd}{3} - c2 * \left( hf + \frac{kd - hf}{3} \right) = c * z$$

$$82500fc * \frac{165}{3} - 9506fc * \left( 100 + \frac{165 - 100}{3} \right)$$

$$= 72994fc * z \rightarrow z = 46.3mm$$

$$jd = d - z = 500 - 46.3 = 453.7 \text{ mm}$$

$$M = A_s f_s jd \rightarrow f_s = \frac{0.2}{3000 * 10^{-6} * 0.4537} = 147 \text{ MPa}$$

$$M = c jd \rightarrow 0.2 = 72994 f_c * 0.4537 \rightarrow f_c = 6.04 \text{ MPa}$$

## EX2:

For data given in ex1, if  $f_s=140\text{MPa}$ ,  $f_c'=30\text{MPa}$ , find moment capacity.

Solution:

$$f_c = 6.04\text{MPa} < f_{c_{all}} = 0.45f_c' = 0.45 * 30 = 13.5\text{MPa}$$

$$f_s = 147\text{MPa} > f_{s_{all}} = 140\text{MPa} \rightarrow \therefore \text{steel failure}$$

$$\begin{aligned} M &= A_s f_s j d = 3000 * 10^{-6} * 140 * 10^3 * 0.4537 \\ &= 190\text{kN.m} \end{aligned}$$

OR

$$\frac{f_c}{k d} = \frac{\frac{f_s}{n}}{d - k d} \rightarrow \frac{f_c}{165} = \frac{\frac{140}{12}}{500 - 165} \rightarrow f_c = 5.74\text{MPa}$$

$$M = c j d = 72994 * 5.74 * 0.4537 * 10^{-3} = 190\text{kN.m}$$