

2<sup>nd</sup> year / Air conditioning 1 Assist. Prof. Dr. Esam M. Mohamed 2023-2024

Lecture four

## Sensible heat ratio (S.H.R)



Process 1-2 indicates the total heating or cooling process.

While process 1-a indicates the part of heat used for sensible heating or cooling and process a-2 indicates the part of heat used for <u>latent heating or cooling</u>.

Therefore, the sensible heat ratio (SHR) is given by,

 $SHR = \frac{sensible \ heat}{sensible \ heat + latient \ heat} = \frac{h_a - h_1}{(h_a - h_1) + (h_2 - h_a)} = \frac{h_a - h_1}{(h_2 - h_1)} = \frac{sensible \ heat}{Total \ heat}$ 

There are actually two SHR scales on the chart, the protractor shaped on the left side and a vertical axis on the right side.



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## 2-Air mixing:

When two air streams are mixed without external heating or cooling, the process is considered adiabatic, and transfer of heat & moisture is internally conserved.





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Mass conservation:
                                                             (a)
m_1 + m_2 = m_3
                             . . . . . . . . . . . .
For water vapour mass:
                                                               (b)
m_1w_1+m_2w_2=m_3w_3
                              . . . . . . . . . . . .
Enthalpy balance:
m_1h_1+m_2h_2=m_3h_3
                                                                  \bigcirc
                               . . . . . . . . . . . . . . .
subtract (m_1w_3) from both sides of equation (b):
m_1w_1 - m_1w_3 + m_2w_2 = w_3(m_3 - m_1) = w_3m_2
m_1(w_1-w_3)=m_2(w_3-w_2)
\frac{w_1 - w_3}{w_3 - w_2} \frac{m_2}{m_1}
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Similarly for enthalpy:

 $\frac{h_1 - h_3 \underline{m_2}}{h_3 - h_2} \frac{m_2}{m_1}$ 



From the above we conclude that the three states point must lie on a straight line in a coordinate system of mass and energy.

Note: length 2-3 is proportional to mass at state (1).

length 1-3 is proportional to mass at state (2).



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e.g: Moist air at 60°C d.b. & 32°C w.b. & standard atmospheric pressure mixed adiabatically with moist air at 5°C d.b. & 1°C w.b. & standard atmospheric pressure. If the masses of dry air are 3kgs & 2kgs respectively, calculate the enthalpy, specific humidity & dry bulb temperature of the mixture.

Sol:

$$\begin{split} & W=0.622*\frac{P}{P_B-P} \\ & P_1=P_{sw}-P_B.A.(t_d-t_w) \\ &=4.7596-101.325*6.66*10^{-4}*(60-32)=2.8702 \text{ kPa.} \\ & W_1=0.622*\frac{2.8702}{101.325-2.8702}=0.01813 \text{ kgw/kg d.a.} \\ & h_1=(1.007 \text{ t} -0.026)+\text{ w} (2501+1.84 \text{ t}) \\ &=(1.007*60-0.026)+(2501+1.84*60)=107.738 \text{ kJ/kg} \\ & P_2=P_{sw}-P_B.A.(t_d-t_w) \\ &= 0.6571-101.325*6.66*10^{-4}*(5-1)=0.38717 \text{ kPa} \\ & w_2=0.622*\frac{0.38717}{101.325-0.38717}=0.002385 \text{ kg/kg dry air.} \\ & h_2=(1.007*5-0.026)+0.002385(2501+1.84*5)=10.995 \text{ kJ/kg.} \\ & \text{from mass balance for moisture.} \end{split}$$

$$W_{3} = \frac{m_{1w_{1}+m_{2w_{2}}}}{m_{1}+m_{2}} \text{ from equation (b) as } m_{3} = m_{1}+m_{2}$$
$$= \frac{3*0.01813+2*0.002385}{3+2} = 0.011832 \text{ kgw/kg d.a.}$$



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Likewise, from equation ©.

 $h_3 = \frac{m_{1h_1 + m_{2h_2}}}{m_1 + m_2} = \frac{3*107.738 + 2*10.995}{3+2} = 69.0408 \text{ kJ/kg d.a.}$ 

to find the dry bulb temperature.

 $\begin{aligned} h_3 &= (1.007 \ t_3 \ -0.026) + w_3 \ (2501 + 1.84 \ t_3) \\ 69.0408 &= (1.007 \ t_3 \ -0.026) + 0.011832 \ (2501 + 1.84 \ t_3) \\ 69.0408 + 0.026 - (0.011832^*2501) = t \ (1.007 + 0.011832^*1.84) \\ t_3 &= 38.37^{\circ}C. \end{aligned}$ 

temperature may be obtained from a temperature balance for normal conditions thus.

$$m_{3}t_{3} = m_{1}t_{1} + m_{2}t_{2}$$
$$t_{3} = \frac{m_{1}t_{1} + m_{2}t_{2}}{m_{3}} = \frac{3*60 + 2*5}{5} = 38^{\circ}C$$

Note: this approach is basically wrong since it assumes air is dry. However, it gives approximate results with tolerable error.

To calculate  $t_{wb}$  [P=P<sub>sw</sub>-P<sub>B</sub>.A.(t<sub>d</sub>-t<sub>w</sub>)]