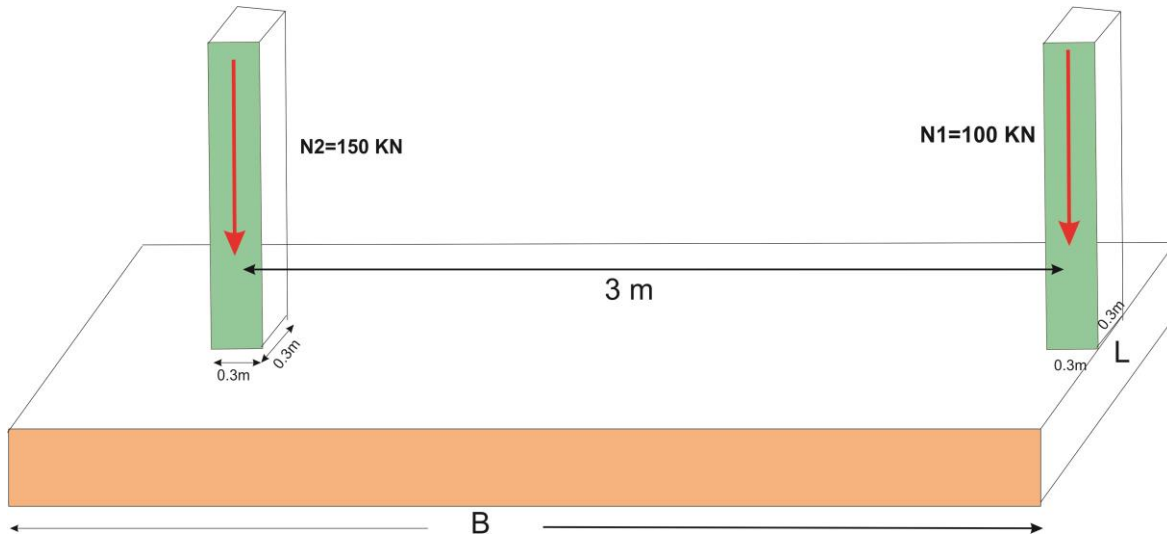


Eccentric combined footing design

Example: A rectangular eccentric combined footing shown in the figure is required to be fully designed. The allowable bearing capacity of the underlying soil is $q_a = 50 \text{ KN/m}^2$. The distance between the two column is 3m. $f_c = 25 \text{ Mpa}$, $f_y = 450 \text{ Mpa}$



The first step is to transmit the forces system to the center. This is may be done as follows:-
For simplify the problem, suppose the center of the right column is at the edge of the footing.

$$M = 50B - (450 - 75B) = 125B - 450 \quad \text{clockwise}$$

$$q = \frac{N}{LB} + \frac{6M}{LB^2}$$

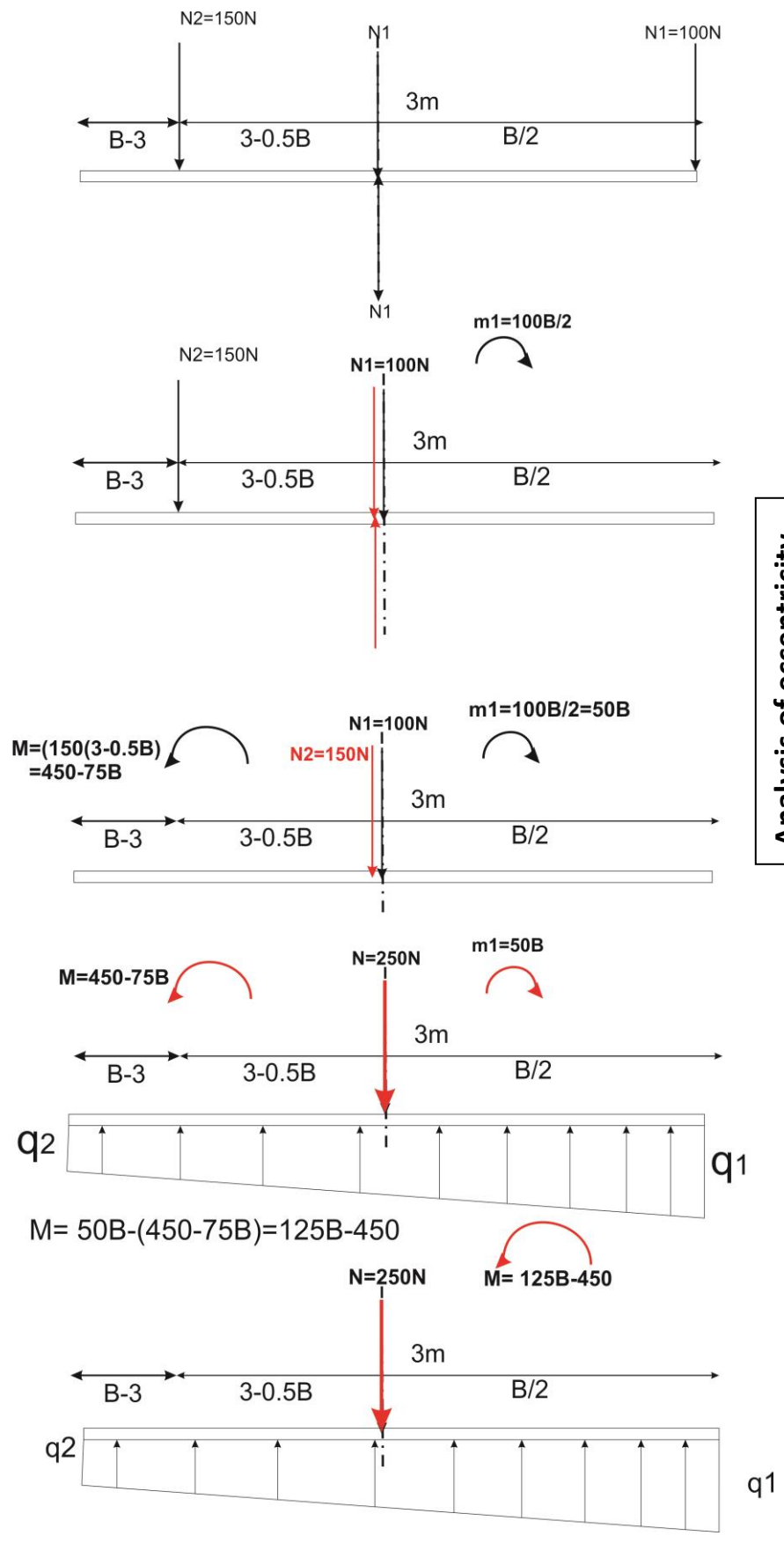
$$q_1 = \frac{250}{LB} + \frac{6(125B-450)}{LB^2}$$

$$q_2 = \frac{250}{LB} - \frac{6(125B-450)}{LB^2}$$

Let the footing is rectangular and suppose $B=2L$, this leads to

$$q_1 = \frac{250}{L*2L} + \frac{6(125*2L-450)}{L*(2L)^2} = \frac{125}{L^2} + \frac{6(250L-450)}{4L^3}$$

$$q_2 = \frac{250}{L*2L} - \frac{6(125B-450)}{LB^2} = \frac{125}{L^2} - \frac{6(250L-450)}{4L^3}$$



Analysis of eccentricity

In all cases q_2 is larger than q_1 , therefore q_2 should be used for footing dimension design

Let;

$$\frac{125}{L^2} - \frac{6(250L-450)}{4L^3} = 50 \text{ KN/m}^2$$

$$125L + 675 - 375L = 50L^3$$

$$-200L - 50L^3 = -675$$

$L=1.835\text{m} \cong 1.85$, $B=3.67\text{m} \cong 3.7\text{m}$ Footing dimensions

$$M = 125B - 450 = 125 * 3.7 - 450 = 12.5\text{KN.m clockwise}$$

$$q_2 = \frac{125}{1.85^2} - \frac{6(250*1.85-450)}{4(1.85)^3} = 33.56\text{KN/m}^2 * 1.85\text{m} = 62 \text{ KN/m}$$

$$q_1 = \frac{125}{(1.85)^2} + \frac{6(250*1.85-450)}{4(1.85)^3} = 39.48\text{KN/m}^2$$

$$q_1 = 39.48 \frac{\text{KN}}{\text{m}^2} * 1.85 = 73\text{KN/m}$$

Checking of eccentricity

$$e = \frac{12.5}{250} = 0.062\text{m}, \quad e = \frac{B}{6} = \frac{3.7\text{m}}{6} = 0.616\text{m}$$

$$0.062 < 0.61 \quad \text{OK}$$

Shear force diagram

1- Shear force left a = $62 * 0.7 + \frac{11}{3.7} * 0.7^2 / 2 = 44.128 \text{ KN}$

2- Shear force right a = $44.128 - 150 = -105.871 \text{ KN}$

3- Shear force left d = $(62+73)/2 * 3.7 - 150 = 100\text{KN}$

4- Shear force right d = 0

Zero shear point

$$62 * X + \frac{11}{3.7} * \frac{X^2}{2} - 150 = 0$$

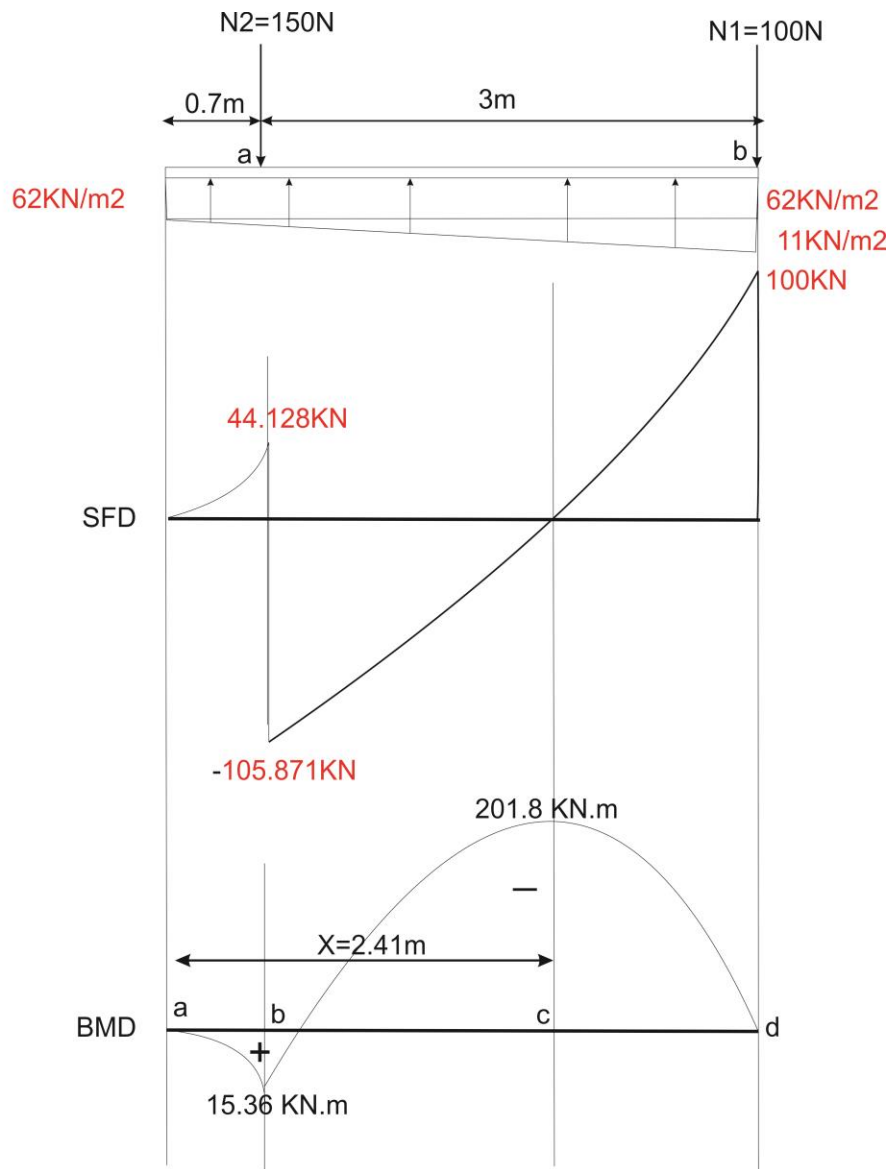
$$62X + 0.14864X^2 = 150, \quad X = 2.41(\text{Zero shear point and max moment})$$

Maximum moment

$$M_a = 62 * \frac{0.7^2}{2} + \frac{11}{3.7} * \frac{0.7^3}{6} = 15.36 \text{KN.m}$$

$$M_{max} = 62 * \frac{2.41^2}{2} + \frac{11}{3.7} * 2.41 * \frac{2.41}{2} * \frac{2.41}{3} - 150 * 1.71$$

$$M_{max} = 47.74 + 6.9357 - 256.5 = 201.8 \text{KN.m}$$



SFD and BMD

H determination

$$v_U = 0.8\sqrt{f_c} = 0.8\sqrt{25} = 4 \text{ N/mm}^2$$

$$d = \frac{2N_U}{\text{perimeter} \cdot v_U} = \frac{2 \cdot 1.6 \cdot 150 \cdot 1000}{1200 \cdot 4} = 200 \text{ mm}, \text{ take } d = 300 \text{ mm minimum}$$

$$H = 300 + 50 \text{ cover} + 20 \text{ mm bar} = 370 \text{ mm}, \text{ approximate to } 400 \text{ mm}$$

$$\text{Real } d = 400 - 50 \text{ cover} - 20\phi = 330 \text{ mm}$$

Reinforcement design

Reinforcement at maximum moment

$$K = \frac{M_{max}}{f_c L d^2} = \frac{201.8 \cdot 10^6}{25 \cdot 1850 \cdot 300^2} = 0.04848$$

$$\frac{Z}{d} = 0.5 + \sqrt{0.25 - \frac{0.04848}{0.9}} = 0.942 < 0.95 \quad \text{OK}$$

$$Z = 0.942 \cdot 330 = 310.5$$

$$A_s = \frac{M}{0.95 f_y Z} = \frac{1.5 \cdot 201.8 \cdot 10^6}{0.95 \cdot 450 \cdot 310.5} = 2,280.4 \text{ mm}^2$$

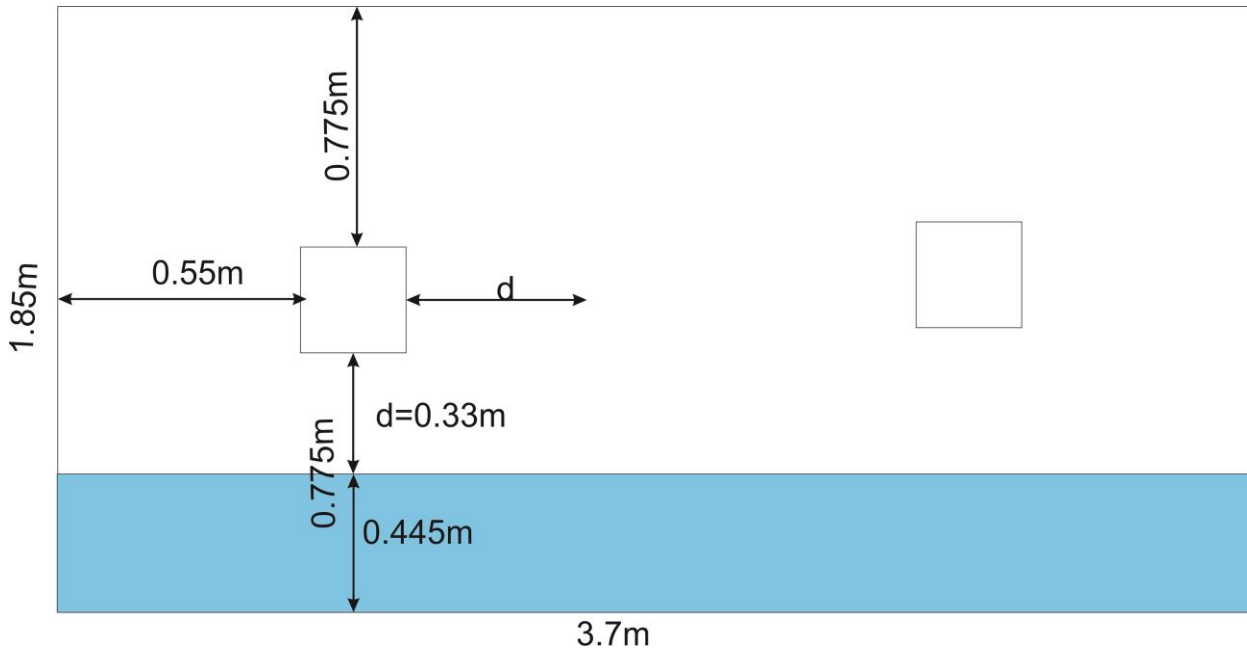
$$\text{Minimum reinforcement} = 0.13 L d = 0.13 \cdot 1850 \cdot 330 / 100 = 793.65 \text{ mm}^2 \quad \text{OK}$$

$$\text{No of bars} = \frac{2,280.4}{314.1} = 7.26, \text{ use } 8 \phi 20 \text{ for Negative side.}$$

$$\text{Spacing} = \frac{185}{8} = 23.125, \text{ use } 20 \text{ cm}, \text{ use } 9\phi 20 \text{ to keep the distance between the bars}$$

20cm

Shear Check



$$\text{Shear force } v = \frac{\frac{39.5\text{KN}}{m} + 33.5\text{KN/m}}{2} * 3.7\text{m} * 0.445\text{m} = 60 \text{ KN}$$

$$\text{Shear stress} = \frac{v}{Bd} = \frac{60 * 1000}{3700 * 330} = 0.049$$

$$V_C = [0.79 \left(\frac{100A_S}{Ld} \right)^2 \frac{400}{d} \left(\frac{f_c}{25} \right)^{\frac{1}{3}}] / 1.25$$

If $\frac{400}{d} < 1$ take it 1

$$V_C = [0.79 \left(\frac{100 * 2,280.4}{1850 * 330} \right)^2 \frac{400}{330} \left(\frac{25}{25} \right)^{\frac{1}{3}}] / 1.25 = 0.10688 > 0.049 \text{ OK}$$

Check Punching

$$\text{Perimeter of punching, } U = 300 * 4 + 8 * 1.5 * 330 = 5,160\text{mm}$$

$$A_p = 1.85^2 - (3 * 0.33 + 0.3)^2 = 1.7584\text{m}^2$$

$$\text{Punching force, } V_p = 1.785 * \frac{33.5 + \frac{6}{3.7} * 1.85}{2} = 32.57\text{KN}$$

$$\text{Punching stress, } v_p = \frac{32.57 * 1000}{5160 * 330} = 0.019\text{n/mm}^2 < V_C$$

