## Lecture -6-

The general procedure for use of Table 11-2 is as follows:

1. Determine the air-flow requirements and the room size.
2. Select the number, location, and type of diffuser to be used.
3. Determine the room characteristic length.
4. Select the recommended throw-to-length ratio from Table 11-2.
5. Calculate the throw.
6. Select the appropriate diffuser from catalog data such as those in Tables 11-3, 11-4, 11-5, or 11-6.
7. Make sure any other specifications are met (noise, total pressure, etc.).

Ex: The room shown in Figure (1) is part of a single-story office building located in the central United States. A perimeter air-distribution system is used. The air quantity required for the room is $\mathbf{2 5 0} \mathbf{~ c f m}$. Select diffusers for the room based on cooling.


Figure 1 Plan view of a room showing location of different types of outlets.
Solution:.
Diffusers of the type shown in Table 11-3 should be used for this application.
A diffuser should be placed under each window in the floor near the wall (Figure $c$ ) because the room has two exposed walls. This will promote mixing with the warm air entering through the window. The total air quantity is divided equally between the two diffusers $(\mathbf{2 5 0} / \mathbf{2}=\mathbf{1 2 5} \mathbf{~ c f m})$. If we assume that the room has an 8 ft ceiling and a room cooling load of $40 \mathrm{Btu} /(\mathrm{hr}-\mathrm{ft} 2)$, the room characteristic length is $\mathbf{8} \mathrm{ft}(\mathbf{1 6 / 2})$.

Table 11-2 gives a throw-to-length ratio of $\mathbf{1 . 3}$ for a straight vane diffuser. Then

$$
\frac{x 50}{L}=1.3 \rightarrow \frac{x 50}{8}=1.3 \rightarrow \underline{\boldsymbol{x 5 0}=\mathbf{1 0 . 4} \mathbf{~ f t}} \text { (throw=blow) }
$$

From Table 11-3, $\underline{\mathbf{a}} \mathbf{~} \times \mathbf{1 2} \mathbf{i n}$. diffuser with $\underline{\mathbf{1 2 5} \mathbf{~ c f m}}$ has a throw (blow), corrected for length, between

$$
x 50=13\left(\frac{3}{4}\right)=9.7 \mathrm{ft} \text { and } x 50=17\left(\frac{3}{4}\right)=12.7 \mathrm{ft}
$$

because 125 cfm lies between 111 cfm and 139 cfm .
The NC is quite acceptable and is between $\mathbf{1 2}$ and 18, uncorrected for length. The total pressure required by the diffuser is between 0.036 and 0.057 in . wg and is about

$$
\Delta P=(125 / 111)^{2} \times(0.036)=\underline{\mathbf{0 . 0 4 6}} \mathbf{i n} . \mathbf{w g}
$$

An acceptable solution is listed as follows:

| Size, in. | Capacity, cfm | Throw, ft | NC | $\Delta P_{0}$, in. wg |
| :--- | :---: | :---: | :---: | :---: |
| $4 \times 12$ | 125 | 10.5 | $<15$ | 0.046 |

The loss in total pressure for the diffuser is an important consideration. The value shown above would be acceptable for a light commercial system.

Table 11-1 Charactenistic Room Length for Several Diffusers

| Diffuser Type | Characteristic Length $L$ |
| :--- | :--- |
| High sidewall grille | Distance to wall perpendicular to jet |
| Circular ceiling diffuser | Distance to closet wall or intersecting air jet |
| Sill grille | Length of room in direction of jet flow |
| Ceiling slot diffuser | Distance to wall or midplane between outlets |
| Light troffer diffisers | Distance to midplane between outlets plus distance |
| from ceiling to top of occupied zone |  |
| Perforated, louvered ceiling diffusers | Distance to wall or midplane between outlets |

Source: Reprinted by permission from ASHRAE Handbook, Fundamentals Volume, 1997.

Table 11-2 Air Diffusion Performance Index (ADPI) Selection Guide

| Terminal Device | Room Load. $\mathrm{Bta} / \mathrm{hr}-\mathrm{ft}^{2}$ | $x_{50} / L^{a}$ for <br> Maximum <br> ADPI | $\begin{aligned} & \text { Maximum } \\ & \text { ADPI } \end{aligned}$ | For ADPI Greater Than | Range of $x_{50} / L^{a}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| High sidewall grilles | 80 (252) | 1.8 | 68 | - | - |
|  | 60 (189) | 1.8 | 72 | 70 | 1.5-2.2 |
|  | 40 (126) | 1.6 | 78 | 70 | 1.2-2.3 |
|  | 20 (63) | 1.5 | 85 | 80 | 1.0-1.9 |
| Circular ceiling diffusers | 80 (252) | 0.8 | 76 | 70 | 0.7-1.3 |
|  | 60 (189) | 0.8 | 83 | 80 | 0.7-1.2 |
|  | 40 (126) | 0.8 | 88 | 80 | 0.5-1.5 |
|  | 20 (63) | 0.8 | 93 | 90 | 0.7-1.3 |
| Sill grille, Straight vanes | 80 (252) | 1.7 | 61 | 60 | 1.5-1.7 |
|  | 60 (189) | 1.7 | 72 | 70 | 1.4-1.7 |
|  | 40 (126) | 1.3 | 86 | 80 | 1.2-1.8 |
|  | 20 (63) | 0.9 | 95 | 90 | 0.8-1.3 |
| Sill grille, Spread vanes | 80 (252) | 0.7 | 94 | 90 | 0.6-1.5 |
|  | 60 (189) | 0.7 | 94 | 80 | 0.6-1.7 |
|  | 40 (126) | 0.7 | 94 | - | - |
|  | 20 (63) | 0.7 | 94 | - | - |
| Ceiling slot diffusers (for $\left.T_{100} / L\right)^{a}$ | 80 (252) | 0.3 | 85 | 80 | $0.3-0.7$ |
|  | 60 (189) | 0.3 | 88 | 80 | $0.3-0.8$ |
|  | 40 (126) | 0.3 | 91 | 80 | 0.3-1.1 |
|  | 20 (63) | 0.3 | 92 | 80 | 0.3-1.5 |
| Light troffer diffusers | 60 (189) | 2.5 | 86 | 80 | $<3.8$ |
|  | 40 (126) | 1.0 | 92 | 90 | <3.0 |
|  | 20 (63) | 1.0 | 95 | 90 | <4.5 |
| Perforated and louvered ceiling diffusers | 11-51 (35-160) | 2.0 | 96 | 90 | 1.4-2.7 |
|  |  |  |  | 80 | 1.0-3.4 |

${ }^{a}$ For SI units, $x_{0.25} / L$ and $T_{0.5} / L$
Source: Reprinted by permission from ASHRAE Handbook, Fundamentals Volume, 1997.

Table 11-3 Performance Data for a Typical Linear Diffiuser

| Size, in | Area $\mathrm{ft}^{2} / \mathrm{ft}$ | Total Pressure, in wg | Flow, cfm/ft | $\mathrm{NC}^{\text {b }}$ | Throw, ${ }^{\text {a }}$ ft |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Mid. | Max |
| 2 | 0.055 | 0.009 | 22 | - | 1 | 1 | 1 |
|  |  | 0.020 | 33 | - | 4 | 4 | 4 |
|  |  | 0.036 | 44 | 12 | 7 | 7 | 7 |
|  |  | 0.057 | 55 | 18 | 9 | 9 | 10 |
|  |  | 0.080 | 66 | 23 | 11 | 11 | 12 |
|  |  | 0.109 | 77 | 27 | 13 | 14 | 16 |
|  |  | 0.143 | 88 | 31 | 14 | 16 | 18 |
|  |  | 0.182 | 99 | 34 | 15 | 17 | 20 |
|  |  | 0.225 | 110 | 37 | 17 | 19 | 21 |
| 4 | 0.139 | 0.009 | 56 | - | 3 | 3 | 3 |
|  |  | 0.020 | 83 | - | 9 | 9 | 9 |
|  |  | 0.036 | 111 | 12 | 13 | 13 | 13 |
|  |  | 0.057 | 139 | 18 | 16 | 16 | 17 |
|  |  | 0.080 | 167 | 23 | 20 | 20 | 21 |
|  |  | 0.109 | 195 | 27 | 22 | 23 | 24 |
|  |  | 0.143 | 222 | 31 | 24 | 25 | 26 |
|  |  | 0.182 | 250 | 34 | 27 | 27 | 27 |
|  |  | 0.225 | 278 | 37 | 30 | 30 | 30 |
| 6 | 0.221 | 0.009 | 88 | - | 5 | 5 | 5 |
|  |  | 0.020 | 133 | - | 10 | 10 | 10 |
|  |  | 0.036 | 177 | 13 | 15 | 15 | 15 |
|  |  | 0.057 | 221 | 19 | 18 | 18 | 18 |
|  |  | 0.080 | 265 | 24 | 23 | 23 | 23 |
|  |  | 0.109 | 310 | 28 | 25 | 25 | 25 |
|  |  | 0.143 | 354 | 32 | 28 | 28 | 28 |
|  |  | 0.182 | 398 | 35 | 31 | 31 | 31 |
|  |  | 0.225 | 442 | 38 | 32 | 32 | 32 |
|  | $\begin{aligned} & \text { Active Length } \\ & \mathrm{ft} \end{aligned}$ | Multiplier Factor for Throw Value at Terminal Velocity, ff/min |  |  |  |  |  |
|  |  | 150 | 100 |  |  |  |  |
|  |  |  | 0.6 |  |  |  |  |
|  | 10 or continuous | $\text { Is } \quad 1.6$ | 1.4 |  |  |  |  |
|  | $\begin{aligned} & \text { Active Length, } \\ & \mathrm{ft} \end{aligned}$ | $\underset{\text { NC }}{\text { NCrection }}$ | Active Le ft | $\underset{\text { Corre }}{\mathrm{N}}$ |  | -si | $\cdots$ |
|  | 1 | -10 | 10 |  |  |  |  |
|  | 2 | -7 | 15 | + |  |  |  |
|  | 4 | -4 | 20 | $+3$ |  |  |  |
|  | 6 | -2 | 25 | +4 |  |  |  |
|  | 8 | -1 | 30 | + |  |  |  |

${ }^{a^{a}}$ Minimmm throw values refer to a terminal velocity of $150 \mathrm{ft} / \mathrm{min}$, middle to $100 \mathrm{ft} / \mathrm{min}$, and maximum to $50 \mathrm{ft} / \mathrm{min}$, for a 4 ft active section with a cooling temperature differential of 20 F . The multiplier factors listed at the bottom are applicable for other lengths.
${ }^{5}$ Based on a room absorption of 80 dB referred to $10^{-12} \mathrm{~W}$, and a 10 ft active section. Source: Reprinted by permission of Environmental Elements Corporation, Dallas, TX.

Table 11-4 Performance Data for a Typical Round Ceiling Diffuser

| Size, <br> in. | Neck Velocity, ftmin | Velocity Pressure, in wg | Total Pressure, in. wg | Flow <br> Rate, cfm | Ractius of Diffusion ${ }^{4}$ ft |  |  | $\mathrm{NC}^{+}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Mm. | Mid. | Max. |  |
| 6 | 400 | 0.010 | 0.026 | 80 | 2 | 2 | 4 | - |
|  | 500 | 0.016 | 0.041 | 100 | 2 | 3 | 5 | - |
|  | 600 | 0.023 | 0.059 | 120 | 2 | 4 | 6 | 14 |
|  | 700 | 0.031 | 0.079 | 140 | 3 | 4 | 7 | 19 |
|  | 800 | 0.040 | 0.102 | 160 | 3 | 5 | 8 | 23 |
|  | 900 | 0.051 | 0.130 | 180 | 4 | 5 | 9 | 26 |
|  | 1000 | 0.063 | 0.161 | 200 | 4 | 6 | 10 | 30 |
|  | 1200 | 0.090 | 0.230 | 235 | 5 | 7 | 11 | 35 |
| 8 | 400 | 0.010 | 0.033 | 140 | 2 | 4 | 6 | - |
|  | 500 | 0.016 | 0.052 | 175 | 3 | 4 | 7 | 15 |
|  | 600 | 0.023 | 0.075 | 210 | 4 | 5 | 9 | 21 |
|  | 700 | 0.031 | 0.101 | 245 | 4 | 6 | 10 | 26 |
|  | 800 | 0.040 | 0.130 | 280 | 5 | 7 | 11 | 31 |
|  | 900 | 0.051 | 0.166 | 315 | 5 | 8 | 13 | 34 |
|  | 1000 | 0.063 | 0.205 | 350 | 6 | 9 | 14 | 37 |
|  | 1200 | 0.090 | 0.292 | 420 | 7 | 11 | 17 | 44 |
| 10 | 400 | 0.010 | 0.027 | 220 | 3 | 4 | 7 | - |
|  | 500 | 0.016 | 0.043 | 270 | 3 | 5 | 8 | 11 |
|  | 600 | 0.023 | 0.062 | 330 | 4 | 6 | 10 | 17 |
|  | 700 | 0.031 | 0.084 | 380 | 5 | 7 | 11 | 21 |
|  | 800 | 0.040 | 0,108 | 435 | 5 | 8 | 13 | 26 |
|  | 900 | 0.051 | 0.138 | 490 | 6 | 9 | 15 | 30 |
|  | 1000 | 0.063 | 0.170 | 545 | 7 | 10 | 16 | 33 |
|  | 1200 | 0.090 | 0.243 | 655 | 8 | 12 | 20 | 39 |
| 12 | 400 | 0.010 | 0.026 | 315 | 3 | 5 | 8 | - |
|  | 500 | 0.016 | 0.042 | 390 | 4 | 6 | 10 | 11 |
|  | 600 | 0.023 | 0.060 | 470 | 5 | 7 | 12 | 17 |
|  | 700 | 0.031 | 0.081 | 550 | 6 | 8 | 13 | 22 |
|  | 800 | 0.040 | 0.105 | 630 | 6 | 10 | 15 | 26 |
|  | 900 | 0.051 | 0.134 | 705 | 7 | 11 | 17 | 30 |
|  | 1000 | 0.063 | 0.166 | 785 | 8 | 12 | 19 | 33 |
|  | 1200 | 0.090 | 0.236 | 940 | 10 | 14 | 23 | 39 |
| 18 | 400 | 0.010 | 0.030 | 710 | 5 | 7 | 12 | - |
|  | 500 | 0.016 | 0.048 | 885 | 6 | 9 | 15 | 15 |
|  | 600 | 0.023 | 0.069 | 1060 | 7 | 11 | 18 | 21 |
|  | 700 | 0.031 | 0.093 | 1240 | 9 | 13 | 21 | 26 |
|  | 800 | 0.040 | 0.120 | 1420 | 10 | 15 | 24 | 30 |
|  | 900 | 0.051 | 0.153 | 1590 | 11 | 17 | 27 | 34 |
|  | 1000 | 0.063 | 0.189 | 1770 | 12 | 19 | 30 | 37 |
|  | 1200 | 0.090 | 0.270 | 2120 | 15 | 22 | 36 | 43 |
| a. | -mn | anan | ama | *nan | , | n | $\cdots$ |  |

Table 11-4 Performance Data for a Typical Round Ceiling Diffuser (continued)


[^0]Table 11-5 Performance Data for an Adjustable-Type, High Sidewall Diffiser

| Sizes, in | $\begin{aligned} & A_{i T} \\ & \mathrm{fi}^{2} \end{aligned}$ | Flow, Rate, cm | Veloc. ft/min | Veloc. Press., in wg | Total Pressure, in wg |  |  | NC | Deff, deg | Throw, ft |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $0^{\circ}$ | 22, $\frac{1}{2}^{\circ}$ | $45^{\circ}$ |  |  | Min. | Mid. | Max. |
| $8 \times 4$ | 0.18 | 70 | 400 | 0.010 | 0.017 | 0.019 | 0.029 | - | 0 | 6 | 8 | 15 |
| $7 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 5 | 6 | 12 |
| $6 \times 6$ |  |  |  |  |  |  |  |  | 45 | 3 | 4 | 8 |
| $10 \times 4$, | 0.22 | 90 |  |  |  |  |  | - | 0 | 7 | 10 | 17 |
| $8 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 6 | 8 | 14 |
| $7 \times 6$ |  |  |  |  |  |  |  |  | 45 | 3 | 5 | 9 |
| $12 \times 4$, | 0.26 | 105 |  |  |  |  |  | - | 0 | 7 | 11 | 19 |
| $10 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 6 | 9 | 15 |
| $8 \times 6$ |  |  |  |  |  |  |  |  | 45 | 4 | 5 | 9 |
| $16 \times 4$, | 0.34 | 135 |  |  |  |  |  | - | 0 | 8 | 12 | 21 |
| $12 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 6 | 10 | 17 |
| $10 \times 6$ |  |  |  |  |  |  |  |  | 45 | 4 | 6 | 11 |
| $18 \times 4$, | 0.39 | 155 |  |  |  |  |  | - | 0 | 9 | 13 | 23 |
| $14 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 7 | 10 | 18 |
| $12 \times 6$, |  |  |  |  |  |  |  |  | 45 | 4 | 6 | 11 |
| $8 \times 4$, | 0.18 | 90 | 500 | 0.016 | 0.028 | 0.031 | 0.047 | - | 0 | 7 | 11 | 17 |
| $7 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 6 | 9 | 14 |
| $6 \times 6$ |  |  |  |  |  |  |  |  | 45 | 4 | 5 | 9 |
| $10 \times 4$, | 0.22 | 110 |  |  |  |  |  | - | 0 | 8 | 12 | 19 |
| $8 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 6 | 10 | 15 |
| $7 \times 6$ |  |  |  |  |  |  |  |  | 45 | 4 | 6 | 10 |
| $12 \times 4$, | 0.26 | 130 |  |  |  |  |  | - | 0 | 9 | 13 | 21 |
| $10 \times 5,$ |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 7 | 10 | 17 |
| $8 \times 6$ |  |  |  |  |  |  |  |  | 45 | 4 | 7 | 10 |
| $16 \times 4$, | 0.34 | 170 |  |  |  |  |  | - | 0 | 10 | 15 | 24 |
| $12 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 8 | 12 | 19 |
| $10 \times 6$ |  |  |  |  |  |  |  |  | 45 | 5 | 8 | 11 |
| $18 \times 4$, | 0.39 | 195 |  |  |  |  |  | - | 0 | 11 | 16 | 25 |
| $14 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 9 | 13 | 20 |
| $12 \times 6$, |  |  |  |  |  |  |  |  | $45^{2}$ | 5 | 8 | 13 |

Table 11-5 Performance Data for an Adjustable-Type, Figh Sidewall Diffiner (contimued)

| Sizes, in | $\frac{A_{\mathrm{f}}}{}$ | Flow, Rate, cfim | Veloc. $\mathrm{ft} / \mathrm{min}$ | Veloc. <br> Press., in $w g$ | Total Pressure, in wg |  |  | NC | Defl, deg | Throw, fir |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $0^{8}$ | $22 \frac{1}{2}^{\circ}$ | $45^{\circ}$ |  |  | Min. | Mid. | Max |
| $8 \times 4$, | 0.18 | 110 | 600 | 0.022 | 0.038 | 0.043 | 0.064 | 10 | 0 | 9 | 13 | 19 |
| $7 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 7 | 10 | 15 |
| $6 \times 6$ |  |  |  |  |  |  |  |  | 45 | 4 | 7 | 10 |
| $10 \times 4$, | 0.22 | 130 |  |  |  |  |  | 10 | 0 | 9 | 15 | 21 |
| $8 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 7 | 12 | 17 |
| $7 \times 6$ |  |  |  |  |  |  |  |  | 45 | 5 | 7 | 10 |
| $12 \times 4$, | 0.26 | 155 |  |  |  |  |  | 11 | 0 | 10 | 16 | 23 |
| $10 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 8 | 13 | 18 |
| $8 \times 6$ |  |  |  |  |  |  |  |  | 45 | 5 | 8 | 11 |
| $16 \times 4$, | 0.34 | 205 |  |  |  |  |  | 12 | 0 | 12 | 19 | 26 |
| $12 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 10 | 15 | 21 |
| $10 \times 6$ |  |  |  |  |  |  |  |  | 45 | 6 | 9 | 13 |
| $18 \times 4$, | 0.39 | 235 |  |  |  |  |  | 13 | 0 | 13 | 19 | 28 |
| $14 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 10 | 15 | 22 |
| $12 \times 6$, |  |  |  |  |  |  |  |  | 45 | 7 | 10 | 14 |
| $8 \times 4$, | 0.18 | 125 | 700 | 0.030 | 0.052 | 0.058 | 0.088 | 15 | 0 | 10 | 15 | 20 |
| $7 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 8 | 12 | 16 |
| $6 \times 6$ |  |  |  |  |  |  |  |  | 45 | 5 | 7 | 10 |
| $10 \times 4$, | 0.22 | 155 |  |  |  |  |  | 15 | 0 | 11 | 16 | 23 |
| $8 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 9 | 13 | 18 |
| $7 \times 6$ |  |  |  |  |  |  |  |  | 45 | 6 | 8 | 11 |
| $12 \times 4$, | 0.26 | 180 |  |  |  |  |  | 16 | 0 | 12 | 17 | 24 |
| $10 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 10 | 14 | 19 |
| $8 \times 6$ |  |  |  |  |  |  |  |  | 45 | 6 | 9 | 12 |
| $16 \times 4$, | 0.34 | 240 |  |  |  |  |  | 17 | 0 | 14 | 20 | 28 |
| $12 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 11 | 16 | 22 |
| $10 \times 6$ |  |  |  |  |  |  |  |  | 45 | 7 | 10 | 14 |
| $18 \times 4$, | 0.39 | 275 |  |  |  |  |  | 18 | 0 | 15 | 22 | 30 |
| $14 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 12 | 18 | 24 |
| $12 \times 6$, |  |  |  |  |  |  |  |  | 45 | 8 | 11 | 15 |
| $8 \times 4$, | 0.18 | 145 | 800 | 0.040 | 0.069 | 0.078 | 0.117 | 19 | 0 | 11 | 16 | 22 |
| $7 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 9 | 13 | 18 |
| $6 \times 6$ |  |  |  |  |  |  |  |  | 45 | 6 | 8 | 11 |
| $10 \times 4$, | 0.22 | 175 |  |  |  |  |  | 19 | 0 | 13 | 17 | 24 |
| $8 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 10 | 14 | 19 |
| $7 \times 6$ |  |  |  |  |  |  |  |  | 45 | 6 | 9 | 12 |
| $12 \times 4$, | 0.26 | 210 |  |  |  |  |  | 20 | 0 | 14 | 19 | 26 |
| $10 \times 5$, |  |  |  |  |  |  |  |  | $22 \frac{1}{2}$ | 11 | 15 | 21 |
| $8 \times 6$ |  |  |  |  |  |  |  |  | 45 | 7 | 9 | 13 |
| $16 \times 4$. | 0.34 | 270 |  |  |  |  |  | 21 | 0 | 16 | 22 | 30 |

Table 11-5 Performance Data for an Adjustable-Type, High Sidewall Diffiser (continued)


[^1]Example 2: Suppose the room of Figure 1 is located in the southern latitudes where overhead systems are recommended. Select a round ceiling diffuser system and a high sidewall system. Also select a return grille.

Given: 250 cfm air quantity Required:
Select a round ceiling diffuser, select high sidewall grille, and select a return grille.


Figure 1
Solution: The data of Table 11.1 with information from Table 11.2 and 11.4 will be used to select a ceiling diffuser. The characteristic length is 7 or 8 ft and the throw-to-length ratio is 0.8 ; then

$$
\mathrm{x}_{50} / \mathrm{L}=0.8 \quad \rightarrow \quad \mathrm{x}_{50}=0.8 \times(7)=5.6 \mathrm{ft}
$$

Using correction factor: $\quad \mathrm{X}_{50}=5.6 / 0.75=7.5$
The best choice would be

| Size, in | Throw, ft | NC | $\Delta P_{0}$, in. wg |
| :---: | :---: | :---: | :---: |
| 10 | $71 / 2$ | 10 | 0.035 |

The throw is larger than desired, but the throw-to-length ratio is within the range to give a minimum ADPI of 76 percent. Figure 1a shows this application.

A high sidewall diffuser may be selected from Table 11.2. In this case the throw-to-length ratio should be about 1.8 and the characteristic length is 14 ft ; then
$\mathrm{x}_{50} / \mathrm{L}=1.8 \quad \rightarrow \quad \mathrm{x}_{50}=1.8 \times(14)=25.2 \mathrm{ft}$
At 240 cfm , pressure drop at $221 / 2$ degree spread would be 0.058 :
At 250 cfm , pressure drop at $221 / 2$ degree spread would be acceptable

$$
\Delta P=\left(\frac{250}{240}\right)^{2} \times 0.058=0.063 \text { in. } \mathrm{wg}
$$

The best choice would be

| Size, in | Throw, ft | NC | $\Delta P_{0}$, in. wg |
| :---: | :---: | :---: | :---: |
| $16 \times 4$ |  |  |  |
| $12 \times 5$ | 25 | 18 | 0.063 |
| $10 \times 6$ |  |  |  |

## RETURN GRILLES

Velocities thru return grilles depend on (1) the static pressure loss allowed and (2) the effect on occupants or materials in the room. In determining the pressure loss, computations should be based on the free velocity thru the grille, not on the face velocity, since the orifice coefficient may approach 0.7. In general the following velocities may be used (see table 1-7):

Table 1-7 Recommended return velocities for different applications.

\left.| GRILLE LOCATION | FPM OVER |
| :--- | :--- |
| GROSS AREA |  |$\right]$

- Thru undercut area

Table 11 .6 Performance Data for One Type of Return Grille

| $\because$ |  | Core Velocity. fpm | 200 | 300 | 400 | 500 | 600 | 700 | 800 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Velocity Pressure, in. wg | 0.002 | 0.006 | 0.010 | 0.016 | 0.023 | 0.031 | 0040 |
| $\begin{aligned} & A^{\delta} \\ & \mathrm{ft}^{2} \end{aligned}$ | Sizes, in. | Static Pressure. in. wg | -0.011 | -0.033 | -0.055 | -0.088 | -0.126 | -0.170 | -0, |
| 0.34 | $16 \times 4$ | cfm | 70 | 100 | 135 | 170 | 205 | 240 |  |
|  | $10 \times 6$ | $\mathrm{NCa}^{\circ}$ |  |  | 13 | 20 | 25 | 30 | 270 33 |
| 0.39 | $18 \times 4$ | cfm | 80 | 115 | 155 | 195 | 235 | 275 | 33 310 |
|  | $12 \times 6$ | NC |  |  | 14 | 21 | 26 |  | 310 34 |
| 0.46 | $20 \times 4$ | cfm | 90 | 140 | 185 | 230 | 275 | 320 | 34 370 |
|  | $14 \times 6$ | NC |  |  | 15 |  | 27 | 320 32 | 370 35 |
|  | $10 \times 8$ $24 \times 4$ | cfm | 105 | 155 |  |  |  |  |  |
| 0.60 | $16 \times 6$ | ${ }_{\mathrm{NCm}}$ | 105 | 155 | 210 16 | 260 23 | 310 28 |  | 415 |
|  | $28 \times 4$ | cfm | 120 | 180 | 240 | 300 | 360 | 33 420 | 36 480 |
|  | $18 \times 6$ $12 \times 8$ | NC |  |  | 17 | 24 | 29 | 34 | 480 37 |
| 0.69 | $30 \times 4$ | cfm | 140 | 205 | 275 | 345 |  |  |  |
|  | $20 \times 6$ $14 \times 8$ | NC |  |  | 17 | 24 | 29 | 485 34 | 550 37 |
|  | $12 \times 10$ |  |  |  |  |  |  |  |  |
| 0.81 | $36 \times 4$ | cfm | 160 | 245 | 325 | 405 |  |  |  |
|  | $22 \times 6$ $16 \times 8$ | NC |  | 10 | 18 | 25 | 485 | $\begin{aligned} & 565 \\ & 35 \end{aligned}$ | $\begin{gathered} 650 \\ 38 \end{gathered}$ |
|  | $14 \times 10$ |  |  |  |  |  |  |  |  |
| 0.90 | $40 \times 4$ | cfm | 180 | 270 | 360 | 450 |  |  |  |
|  | $26 \times 6$ $18 \times 8$ | NC |  | 11 | 19 | 26 | 54 31 | $\begin{gathered} 630 \\ 36 \end{gathered}$ | $\begin{gathered} 720 \\ 39 \end{gathered}$ |
|  | $16 \times 10$ |  |  |  |  |  |  |  |  |
|  | $12 \times 12$ |  |  |  |  |  |  |  |  |
| 1.07 | $48 \times 4$ | cfm | 215 | 320 |  |  |  |  |  |
|  | $30 \times 6$ $18 \times 10$ | NC |  | 12 | 20 | 535 27 | $\begin{gathered} 640 \\ 32 \end{gathered}$ | $\begin{gathered} 750 \\ 37 \end{gathered}$ | 855 40 |
|  | $14 \times 12$ |  |  |  |  |  |  |  |  |
| 1.18 | $34 \times 6$ | cfm | 235 |  |  |  |  |  |  |
|  | $24 \times 8$ | NC |  | $\begin{aligned} & 355 \\ & 13 \end{aligned}$ | $\begin{aligned} & 470 \\ & 21 \end{aligned}$ | $590$ | $710$ | 825 | 945 |
|  | $20 \times 10$ |  |  |  |  |  | $33$ | 38 | 41 |
|  | $16 \times 12$ |  |  |  |  |  |  |  |  |
| 1.34 | $60 \times 4$ | cfm | 270 | 400 | 535 |  |  |  |  |
|  | $36 \times 6$ $18 \times 12$ | NC |  | 13 | 21 | $\begin{gathered} 670 \\ 28 \end{gathered}$ | $805$ | 940 38 | 1070 |
|  | $16 \times 14$ |  |  |  |  |  |  |  |  |
| 1.60 | $30 \times 8$ | cfm | 320 |  |  |  |  |  |  |
|  | $24 \times 10$ | NC | 320 | $480$ | 640 | 800 | 960 | 1120 | 1280 |
|  | $22 \times 12$ |  |  | 14 | 22 | 29 | 34 | 39 | 42 |
|  | $18 \times 14$ |  |  |  |  |  |  |  |  |

Thble 11.6 verformance Data for One Type of Return Grille (continued)


${ }^{4}$ Based on a room absorption of 8 dB , with respect to $10^{-12}$ watts, and one return.


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Example: Small store dimensions: $32 \times 23 \times 16 \mathrm{ft}$ Ceiling - flat
Load - equally distributed
Air quantity - 2000 cfm
Temp difference - 25 F
Find: Number of outlets, Size of outlets,

## Solution:

-The minimum blow is $75 \%$ of the room width for the given condition of equally distributed heat load. Therefore, the minimum blow necessary is: $23 \times 0.75=17.3 \mathrm{ft}$

- The maximum blow is the width of the room $=32 \mathrm{ft}$
- The blow of 17.5 to 34 ft .
- No. of outlets $=\frac{2000}{500}=4$
- nominal size 24 in. $x 6$ in
$\mathrm{k}=\frac{2000}{32 \times 16}=3.9$


## TABLE 1-B - WALL OUTLET RATINGS, FOR COOLING ONLY

For Flat Ceilings

| OUHIT VELOgTY |  | 24 PFP |  |  |  |  | DP Prm |  |  |  |  | Sthem |  |  |  |  | 790 PM |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STALC Passut <br>  |  | $\begin{gathered} 5+I=0,2244^{2}=\pi 1 \\ i y^{\prime \prime}=0 \end{gathered}$ |  |  |  |  | $s I=g 1, n H^{4}=D 13$ |  |  |  |  |  |  |  |  |  | $\begin{gathered} 4-1-9 y_{1} 32 x^{4}-n 61 \\ 4 \end{gathered}$ |  |  |  |  |
| Sthic Phsume with HELGAC FATL |  |  |  |  |  |  | $\begin{gathered} 51 \mathrm{n}=\frac{\pi 4,25}{45}=045 \end{gathered}$ |  |  |  |  |  |  |  |  |  | $\frac{I r i}{}=\frac{175,12 h^{4}-16}{4 s^{t}-3}$ |  |  |  |  |
| Hem, Fie -1 Oytin G-1 Pit Aral | Yent <br> Linn |  | $\left.\frac{4}{\omega \mid} \right\rvert\,$ | Temp Din [i] |  |  |  | $\begin{aligned} & \text { el } \\ & \text { (n) } \end{aligned}$ |  |  |  | AirOuneuntata |  | Tump Pin ${ }^{\text {¢ }}$ |  |  |  | $\begin{aligned} & 1+4 \\ & 4 n \end{aligned}$ | Temp Dili (i) |  |  |
|  |  |  |  | 13 | 30 | 15 |  |  | 11 | 28 | 3 |  |  | 15 | N | 3 |  |  | 11 | 30 | 21 |
|  |  |  |  | Min Cly |  |  |  |  | Hinclan |  |  |  |  | Hinclay |  |  |  |  | Ming |  |  |
| $\begin{aligned} & 4=4 \\ & \mid 16.51 \end{aligned}$ | $\frac{12}{45^{4}}$ | 46 | $\begin{aligned} & 34 \\ & \frac{2}{45} \end{aligned}$ | $\begin{aligned} & 6.5 \\ & 4.4 \\ & 60 \end{aligned}$ | $\begin{aligned} & 70 \\ & i s \\ & 06 \end{aligned}$ | $\left.\begin{array}{\|l\|} \hline 70 \\ 4.4 \\ 4 \end{array} \right\rvert\,$ | 44 | $\begin{aligned} & 70 \\ & 31 \\ & 39 \end{aligned}$ | $\begin{aligned} & 74 \\ & 64 \\ & 64 \end{aligned}$ | $\begin{aligned} & 71 \\ & 70 \\ & 19 \end{aligned}$ | $\begin{aligned} & 49 \\ & 76 \\ & 70 \end{aligned}$ | 5 | $\begin{aligned} & 160 \\ & 75 \\ & 50 \end{aligned}$ | $\begin{aligned} & 74 \\ & 74 \end{aligned}$ | $\begin{aligned} & 10 \\ & 75 \\ & 63 \end{aligned}$ | $\begin{aligned} & 15 \\ & 70 \end{aligned}$ | 4 | $\begin{array}{\|c} 170 \\ 1100 \\ 000 \end{array}$ | $\begin{array}{\|l\|} \hline 13 \\ 4 . \\ 4 \\ \hline \end{array}$ | $\begin{aligned} & 10 \\ & 70 \\ & 70 \end{aligned}$ | $\begin{aligned} & 60 \\ & 10 \\ & 70 \end{aligned}$ |
| $\begin{aligned} & \text { He4 } \\ & \text { (17) } \end{aligned}$ | Hrather $21 \%$ 45 | 7 7 | $\frac{34}{14}$ | $\begin{aligned} & 6.5 \\ & 6.9 \\ & 60 \end{aligned}$ | $\begin{aligned} & 70 \\ & 40 \\ & 40 \end{aligned}$ | $\left\|\begin{array}{l} 75 \\ 75 \\ 5.9 \end{array}\right\|$ | ir | $\begin{aligned} & i 4 \\ & i 5 \end{aligned}$ | $\begin{aligned} & 74 \\ & 81 \\ & 41 \end{aligned}$ | $\begin{aligned} & 75 \\ & i 5 \\ & \hline 5 \end{aligned}$ | $\begin{aligned} & 10 \\ & 76 \\ & 76 \end{aligned}$ | FI | $\begin{aligned} & 10.5 \\ & 10 \\ & 34 \end{aligned}$ | $\begin{aligned} & 7.4 \\ & y_{6} \\ & 45 \end{aligned}$ | $\begin{aligned} & 10 \\ & 55 \\ & 65 \end{aligned}$ | $\frac{15}{75}$ | 112 | $\begin{aligned} & 110 \\ & 100 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 18 \\ & 78 \\ & 3 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 90 \\ & 10 \\ & 70 \end{aligned}$ |
| $\begin{aligned} & B=4 \\ & B 4 \Delta+1 \end{aligned}$ | 4hint N14 4 | 44 | $\frac{34}{14}$ | $\begin{aligned} & 64 \\ & 49 \\ & 60 \end{aligned}$ | $\begin{aligned} & 50 \\ & 49 \\ & 64 \end{aligned}$ | $\left.\begin{aligned} & 24 \\ & 70 \\ & 4 i \end{aligned} \right\rvert\,$ | 4 | $\begin{aligned} & 74 \\ & 59 \\ & 19 \end{aligned}$ | $\begin{aligned} & 79 \\ & 76 \\ & 45 \end{aligned}$ | $\begin{aligned} & 24 \\ & 80 \\ & 40 \end{aligned}$ | $\begin{aligned} & 10 \\ & 70 \\ & 70 \end{aligned}$ | b1 | $\begin{aligned} & 110 \\ & 1.1 \\ & 3 . \end{aligned}$ | $\begin{aligned} & 10 \\ & 70 \\ & 40 \end{aligned}$ | $\begin{aligned} & 10 \\ & 75 \\ & 75 \end{aligned}$ | $\frac{14}{75}$ | 13 | $\begin{gathered} 110 \\ 140 \\ 100 \end{gathered}$ | $\begin{aligned} & 14 \\ & 74 \\ & 48 \end{aligned}$ | $\begin{aligned} & 10 \\ & \frac{10}{10} \end{aligned}$ | $\begin{aligned} & 78 \\ & 78 \end{aligned}$ |
| $\begin{aligned} & 14.4 \\ & 15151 \end{aligned}$ | $\frac{8194}{24}$ | 4 | $\begin{aligned} & \frac{y}{y} \\ & \frac{1}{2} \end{aligned}$ | $\begin{aligned} & 78 \\ & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 76 \\ & 65 \\ & 65 \end{aligned}$ | $\begin{aligned} & 78 \\ & 78 \\ & 48 \end{aligned}$ | 解 | $\begin{aligned} & 79 \\ & 40 \\ & 10 \end{aligned}$ | $\begin{aligned} & 78 \\ & 78 \\ & 63 \end{aligned}$ | $\begin{aligned} & 74 \\ & 70 \\ & 45 \end{aligned}$ | $\frac{10}{70}$ | 17 | $\begin{aligned} & 118 \\ & 41 \\ & 14 \end{aligned}$ | $\begin{aligned} & 40 \\ & 65 \end{aligned}$ | $\begin{aligned} & 18 \\ & 78 \\ & 78 \end{aligned}$ | $\begin{aligned} & 14 \\ & 70 \end{aligned}$ | 1 H | $\begin{aligned} & 100 \\ & 180 \\ & 100 \end{aligned}$ | $\frac{15}{35}$ | $\begin{aligned} & 90 \\ & 70 \\ & 70 \end{aligned}$ | 4 78 7 |
| $\begin{aligned} & 30.14 \\ & 1451 \end{aligned}$ | $\begin{aligned} & \text { Whelen } \\ & \frac{15}{4} \end{aligned}$ | 77 | $\begin{aligned} & 40 \\ & 20 \\ & 10 \end{aligned}$ | $\begin{aligned} & 10 \\ & 60 \end{aligned}$ | $\begin{aligned} & 70 \\ & \frac{10}{65} \end{aligned}$ | $\left\|\begin{array}{l} \frac{7}{7} \\ 4.5 \end{array}\right\|$ | 11i | $\begin{aligned} & 40 \\ & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 75 \\ & 76 \\ & 65 \end{aligned}$ | $\frac{76}{75}$ | $\frac{10}{70}$ | 14 | $\begin{aligned} & 113 \\ & 43 \\ & 45 \end{aligned}$ | $\frac{10}{13}$ | $\begin{aligned} & 19 \\ & 78 \\ & 70 \end{aligned}$ | $\begin{aligned} & 15 \\ & 80 \\ & 70 \end{aligned}$ | 31 | $\begin{aligned} & 700 \\ & 108 \\ & 100 \end{aligned}$ | $\begin{aligned} & 19 \\ & i 5 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & 70 \end{aligned}$ | 48 <br> 78 <br> 8 |
| $\begin{aligned} & 4 \pi 54 \\ & 1509 \mid \end{aligned}$ | $\begin{gathered} 41+54 \\ 45 \\ 45 \end{gathered}$ | 01 | $\begin{aligned} & 41 \\ & 1.1 \\ & 10 \end{aligned}$ | $\begin{aligned} & 30 \\ & 55 \\ & 40 \end{aligned}$ | $\begin{aligned} & 70 \\ & 70 \\ & 83 \\ & \hline \end{aligned}$ | $\left.\begin{array}{\|} 78 \\ 78 \\ 30 \end{array} \right\rvert\,$ | 111 | $\begin{aligned} & 10 \\ & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 40 \\ & 75 \\ & 15 \end{aligned}$ | $\begin{aligned} & \frac{10}{75} \\ & 70 \end{aligned}$ | 14 | $\begin{array}{r} 113 \\ 45 \\ 6 \end{array}$ | $\begin{aligned} & 10 \\ & 15 \\ & 85 \end{aligned}$ | $\begin{aligned} & 70 \\ & 76 \\ & 76 \end{aligned}$ | $\begin{aligned} & 13 \\ & 80 \\ & 70 \end{aligned}$ | \% | $\begin{aligned} & 300 \\ & 189 \\ & 104 \end{aligned}$ | $\begin{aligned} & 19 \\ & 75 \end{aligned}$ | $\begin{aligned} & 90 \\ & 90 \\ & 70 \end{aligned}$ | 104 <br> 8.4 <br> 8 |
| $\begin{aligned} & 20 \times 4 \\ & \|14 y\| \end{aligned}$ |  | 114 | $\begin{aligned} & 42 \\ & 3.1 \\ & 3.1 \end{aligned}$ | $\begin{aligned} & 70 \\ & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 79 \\ & 76 \\ & 65 \end{aligned}$ | $\begin{aligned} & 73 \\ & 79 \\ & 49 \end{aligned}$ | 175 | $\frac{10}{40}$ | $\begin{aligned} & 24 \\ & 70 \\ & 45 \end{aligned}$ | $\begin{aligned} & 40 \\ & 78 \\ & 48 \end{aligned}$ | $\frac{10}{75}$ | 210 | $\begin{aligned} & 100 \\ & 10 \\ & 00 \end{aligned}$ | $\frac{18}{75}$ | $10$ | $\begin{aligned} & 18 \\ & 10 \end{aligned}$ | 14 | $\begin{aligned} & 710 \\ & 100 \\ & 110 \end{aligned}$ | $\begin{aligned} & 15 \\ & 75 \\ & 78 \end{aligned}$ | $\begin{aligned} & 45 \\ & 10 \\ & 70 \end{aligned}$ | 100 88 78 |
| $\begin{aligned} & 3 \ln 4 \\ & \ln 5 \mid \end{aligned}$ | $\frac{5+1 p^{2}}{25^{2}}$ | 146 | $\begin{aligned} & 44 \\ & 24 \\ & 24 \end{aligned}$ | $\begin{aligned} & 36 \\ & 4.3 \\ & 60 \end{aligned}$ | $\begin{aligned} & 75 \\ & 76 \\ & 65 \end{aligned}$ | $\begin{aligned} & 73 \\ & 70 \\ & 49 \end{aligned}$ | 114 | $\begin{aligned} & 10 \\ & 19 \\ & 4 . \end{aligned}$ | $\begin{aligned} & 79 \\ & 79 \\ & 65 \end{aligned}$ | $\frac{10}{74}$ | $\begin{aligned} & 40 \\ & 70 \end{aligned}$ | 7 | $\begin{array}{r} 120 \\ 85 \\ 65 \end{array}$ | $\begin{aligned} & 10 \\ & 75 \\ & 45 \end{aligned}$ | $\frac{75}{70}$ | $\begin{aligned} & \frac{70}{70} \\ & 70 \end{aligned}$ | H3 | $\begin{aligned} & 710 \\ & 110 \\ & 110 \end{aligned}$ | 79 | $\begin{aligned} & 15 \\ & 15 \\ & 70 \end{aligned}$ |  |
| $\frac{B+1}{64}$ | 4nopit $15^{4}$ | 13 | $\begin{aligned} & \frac{10}{14} \\ & \frac{14}{2} \end{aligned}$ | $\begin{aligned} & 24 \\ & 20 \\ & 40 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \\ & 30 \end{aligned}$ | $\left.\begin{array}{\|c\|} \hline \frac{85}{75} \\ 45 \end{array} \right\rvert\,$ | F | $\begin{aligned} & 1.4 \\ & 7 \Delta \\ & 4.1 \end{aligned}$ | $\begin{aligned} & 10 \\ & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 88 \\ & 76 \end{aligned}$ | $\begin{aligned} & i 5 \\ & 40 \\ & 70 \end{aligned}$ | 149 | $\begin{aligned} & 128 \\ & 18 \\ & 48 \end{aligned}$ | $\begin{aligned} & 15 \\ & 75 \end{aligned}$ | $\begin{aligned} & 46 \\ & i 6 \\ & 7 \% \end{aligned}$ | $\begin{aligned} & 16 \\ & 45 \end{aligned}$ | 14 | $\begin{aligned} & 70 \\ & 180 \\ & 120 \end{aligned}$ | $\begin{aligned} & 18 \\ & i 8 \\ & \hline 8 \end{aligned}$ | $\begin{gathered} 100 \\ 75 \\ 75 \end{gathered}$ | 109 |
| $\begin{aligned} & 10-18 \\ & \operatorname{Dig} \end{aligned}$ | $\frac{\operatorname{sel} 94}{235}$ | 4 | $\begin{aligned} & 45 \\ & 41 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \\ & 45 \end{aligned}$ | $\begin{aligned} & 19 \\ & 78 \\ & 70 \\ & 70 \end{aligned}$ | $\frac{89}{70}$ | $\dagger 1$ | $\begin{aligned} & 180 \\ & 7.5 \\ & 30 \end{aligned}$ | $\begin{aligned} & 10 \\ & \frac{10}{75} \end{aligned}$ | $\begin{aligned} & 8 \\ & 80 \end{aligned}$ | $\begin{aligned} & 40 \\ & i s \\ & i s \end{aligned}$ | 131 | $\begin{gathered} 180 \\ 110 \\ 70 \end{gathered}$ | $\begin{aligned} & 16 \\ & 10 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \frac{85}{55} \\ & 75 \end{aligned}$ | $\begin{aligned} & 18.8 \\ & 5 \end{aligned}$ | 14 | $\begin{aligned} & 270 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 100 \\ & 38 \\ & 78 \end{aligned}$ | $\begin{aligned} & 165 \\ & 79 \\ & 75 \end{aligned}$ | (113 |
| $\begin{aligned} & 11 \times 6 \\ & 414 \end{aligned}$ | $\frac{174^{4}}{45^{4}}$ | 4 | $\begin{aligned} & 50 \\ & 48 \\ & 30 \end{aligned}$ | $\frac{75}{76}$ | $\begin{aligned} & 148 \\ & 70 \\ & 70 \end{aligned}$ | $\frac{15}{70}$ | 114 | $\begin{gathered} 11.0 \\ 4.1 \\ i .5 \end{gathered}$ | $\begin{aligned} & 10 \\ & 70 \\ & 50 \end{aligned}$ | $\begin{aligned} & \text { +0 } \\ & 70 \\ & 70 \end{aligned}$ | $\frac{14}{13}$ | 13 | $\begin{array}{r} 130 \\ 110 \\ 30 \end{array}$ | $\begin{aligned} & 18 \\ & 10 \\ & \hline 10 \end{aligned}$ | $\begin{gathered} 14 \\ 75 \end{gathered}$ | $\begin{aligned} & 180 \\ & 70 \\ & \hline 0 \end{aligned}$ | 314 | $\begin{aligned} & 310 \\ & 310 \\ & 140 \end{aligned}$ | 106 | $\begin{aligned} & 118 \\ & 18 \\ & 18 \end{aligned}$ | (115 |
| $\frac{14+4}{144}$ | $\begin{aligned} & \text { trolyH } \\ & \operatorname{IS}^{1} \end{aligned}$ | 18 | $\begin{aligned} & \frac{62}{47} \\ & \frac{12}{2} \end{aligned}$ | $\begin{aligned} & 1.6 \\ & 7.5 \end{aligned}$ | $\begin{aligned} & 10 \\ & 75 \\ & 70 \end{aligned}$ | $\frac{54}{70}$ | 141 | $\begin{gathered} 120.9 \\ 18 \\ 48 \end{gathered}$ | $\begin{aligned} & 15 \\ & 70 \\ & 70 \end{aligned}$ | $\begin{aligned} & \text { 易 } \\ & 70 \end{aligned}$ | $\begin{aligned} & 14 \\ & 75 \end{aligned}$ | 314 | $\begin{aligned} & 149 \\ & 120 \\ & 40 \end{aligned}$ | $\frac{19}{78}$ | $\begin{aligned} & 10.9 \\ & 80 \\ & 75 \end{aligned}$ | $\frac{109}{98}$ | 181 | $\begin{aligned} & 300 \\ & 710 \\ & 100 \end{aligned}$ | 119 $i 8$ 78 | $\begin{array}{\|c} 11.8 \\ 108 \\ 18 \end{array}$ | (12.4 |
| $\begin{aligned} & \operatorname{mox}_{4} 4 \\ & \nabla 15 \end{aligned}$ | $\frac{52 x^{4}}{4 y^{2}}$ | 134 | $\begin{aligned} & 34 \\ & 30 \\ & 11 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 4.0 \\ 75 \\ \hline 5 \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 1.5 \\ 7.3 \\ \hline 70 \\ \hline \end{array}$ | $\begin{aligned} & 80 \\ & 80 \\ & 7 \end{aligned}$ | 30 | $\begin{array}{\|c} 120 \\ \hline 0 \\ \hline 14 \\ \hline \end{array}$ | $\begin{aligned} & 10 \\ & 10 \\ & 70 \\ & \hline \end{aligned}$ | $\begin{aligned} & 63 \\ & \frac{1}{7} \\ & \hline \end{aligned}$ | $\begin{array}{\|c} 100 \\ 80 \\ 75 \end{array}$ | 34 | $\begin{aligned} & 170 \\ & 120 \\ & 98 \\ & \hline \end{aligned}$ | $\begin{aligned} & 13 \\ & 4.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} 100 \\ 80 \\ 100 \\ \hline \end{array}$ | 11.8 15 18 | 40 | $\begin{aligned} & 120 \\ & 140 \\ & 160 \\ & \hline \end{aligned}$ | 11.3 <br> 48 <br> 48 | $\begin{array}{r} 170 \\ 100 \\ 1.5 \\ \hline \end{array}$ | (13.0 |
| $\begin{aligned} & 7+1 \\ & (4+3) \end{aligned}$ | $\frac{5 n y 4}{124}$ | 144 | $\begin{aligned} & 70 \\ & 31 \\ & 24 \end{aligned}$ | $\begin{aligned} & 19 \\ & 75 \\ & 78 \\ & \hline \end{aligned}$ | $\begin{aligned} & 15 \\ & 10 \\ & 70 \end{aligned}$ | $\begin{aligned} & \text { pe } \\ & i 6 \\ & 7.4 \end{aligned}$ | 34 | $\begin{array}{\|c} 110 \\ 168 \\ \hline \end{array}$ | $\begin{aligned} & 20 \\ & 10 \\ & 70 \end{aligned}$ | $\frac{8.8}{84}$ | $\begin{gathered} 109 \\ 10 \\ 10 \end{gathered}$ | 334 | $\begin{array}{r} 110 \\ 130 \\ 60 \\ \hline \end{array}$ | $\begin{aligned} & 100 \\ & 3.5 \\ & 7.5 \end{aligned}$ | $\begin{array}{r} 105 \\ 00 \\ 00 \\ \hline 0.0 \end{array}$ | $\begin{array}{\|c} 110 \\ 150 \\ 1.9 \end{array}$ | 44 | $\begin{aligned} & 310 \\ & 300 \\ & 100 \end{aligned}$ | 120 <br> 100 <br> 10 | $\begin{gathered} 115 \\ 155 \\ 15 \end{gathered}$ | (196 |
|  | $\frac{7 n y}{75}$ | W | $\begin{aligned} & 78 \\ & 34 \end{aligned}$ | $\begin{array}{\|c\|} \hline \frac{3}{75} \\ \hline 2 \end{array}$ | $\begin{array}{\|l} \hline 13 \\ 10 \\ 70 \\ \hline 10 \end{array}$ | $\begin{aligned} & \frac{18}{8} \\ & 79 \end{aligned}$ | 34 | $\begin{array}{\|c} 19.0 \\ 16.0 \\ 4.1 \end{array}$ | $\begin{aligned} & 79 \\ & 70 \\ & 79 \end{aligned}$ | $\begin{array}{\|c\|} \hline 100 \\ 78 \\ 78 \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 105 \\ 05 \\ 10 \\ \hline 0 \end{array}$ | $4 \times$ | $\begin{aligned} & 190 \\ & 140 \\ & 100 \end{aligned}$ | $\begin{aligned} & 100 \\ & 70 \\ & 75 \end{aligned}$ | $\begin{array}{\|c\|} \hline 10 \\ 14 \\ 40 \\ \hline \end{array}$ | $\begin{array}{\|c} 113 \\ 189 \\ 14 \\ \hline \end{array}$ | 401 | $\begin{aligned} & 34,0 \\ & 310 \\ & 170 \end{aligned}$ | 120 100 00 | 12.3 10.5 | (13.5 |
| $\frac{\mathrm{Mn}}{\underline{4}}$ | $\frac{4 \text { 4ap }}{4 y^{4}}$ | 341 | $\begin{aligned} & 7.1 \\ & 31 \\ & 31 \end{aligned}$ | $\begin{aligned} & 14 \\ & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 40 \\ & i 0 \\ & 75 \end{aligned}$ | $\left\|\begin{array}{l} 63 \\ 73 \\ 75 \end{array}\right\|$ | 34 | $\begin{aligned} & 12.0 \\ & 188 \\ & 48 \end{aligned}$ | $\begin{aligned} & 7.5 \\ & \frac{15}{75} \end{aligned}$ | $\begin{aligned} & 106 \\ & 80 \\ & \hline 80 \end{aligned}$ | $\begin{gathered} 10.3 \\ i 5 \\ 10 \end{gathered}$ | + | $\begin{aligned} & 196 \\ & 106 \\ & 100 \end{aligned}$ | 188 | 119 0.5 10 | 128 108 14 | 73 | 159 310 100 | 180 108 15 | 110 16.8 18.8 | (14.4 |

- Inctor


[^0]:    ${ }^{a}$ Minimmm radii of diffusion are to a terminal velocity of $150 \mathrm{ft} / \mathrm{min}$, middle to $100 \mathrm{ft} / \mathrm{min}$, and maximum to $50 \mathrm{ft} / \mathrm{min}$.
    ${ }^{5}$ The NC values are based on a room absorption of 18 dB referred to $10^{-13} \mathrm{~W}(8 \mathrm{~dB}$ referred to $10^{-12} \mathrm{~W}$ ).
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[^1]:    Source: Reprinted by permission of Environmental Elements Corporation, Dallas, TX.

