Chapter Two

Material Balances

2.1 Introduction to Material Balances

A <u>material balance</u> is nothing more than the application of the law of the <u>conservation of mass</u>: "<u>Matter is neither</u> <u>created nor destroyed</u>"

Open and Closed Systems

a. System

By <u>system</u> we mean any arbitrary portion of or a whole **process** that you want to consider for analysis. You can define a <u>system</u> such as a <u>reactor</u>, a <u>section of a pipe</u>. Or, you can define the **limits** of the **system** by drawing the <u>system boundary</u>, namely a line that encloses the portion of the process that you want to analyze.

b. Closed System

Figure 1 shows a two-dimensional view of a three-dimensional vessel holding 1000 kg of H_2O . Note that material neither enters nor leaves the vessel, that is, no material crosses the system boundary. Changes can take place inside the system, but for a <u>closed system</u>, no mass exchange occurs with the surroundings.

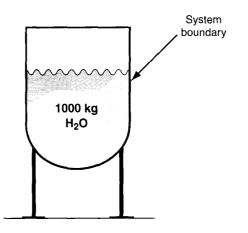


Figure 1 Closed system.

c. Open System

Figure 2 is an example of an **open system** (also called a **flow system**) because material crosses the system boundary.

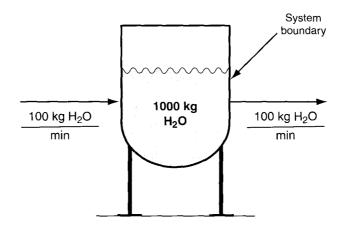


Figure 2 Open steady – state system.

Steady-State and Unsteady-State Systems

a. Steady - State System

Because the rate of addition of water is equal to the rate of removal, the amount of water in the vessel shown in <u>Figure 2</u> remains constant at its original value (1000 kg). We call such a process or system a steady – state process or a steady – state system because

- 1. The **conditions** inside the process (specifically the amount of water in the vessel in Figure 2) **remain unchanged with time**, and
- 2. The conditions of the flowing streams remain constant with time.
- * Thus, in a steady-state process, by definition all of the conditions in the process (e.g., temperature, pressure, mass of material, flow rate, etc.) remain constant with time. A continuous process is one in which material enters and/or leaves the system without interruption.
- b. Unsteady State System

Because the amount of water in the system **changes with time** (Figure 3), the **process** and **system** are deemed to be an **unsteady – state** (transient) process.

For an unsteady-state process, not all of the conditions in the process (e.g., temperature, pressure, mass of material, etc.) remain constant with time, and/or the flows in and out of the system can vary with time.

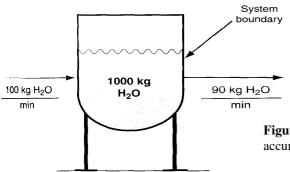


Figure 3 Initial conditions for an open unsteady – state system with accumulation.

★ Figure 4 shows the system after 50 minutes of accumulation (Fifty minutes of accumulation at 10 kg/min amounts to 500 kg of total accumulation).

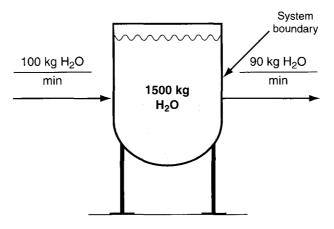


Figure 4 The condition of the open unsteady – state system with accumulation after 50 minutes.

* Figures 5 and 6 demonstrate <u>negative accumulation</u>.

Note that the amount of water in the system decreases with time at the rate of **10 kg/min**. Figure 6.6 shows the system after **50 minutes** of operation.

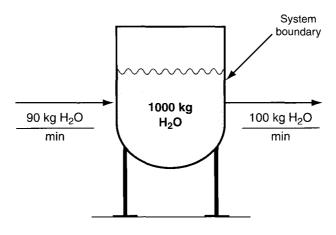


Figure 5 Initial conditions for an unsteady - state process with negative accumulation.

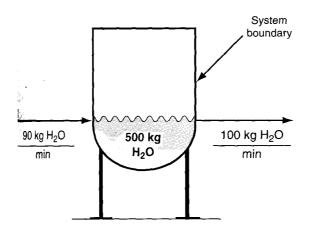


Figure 6 Condition of the open unsteady – state system with negative accumulation after 50 minutes.

* The material balance for a single component process is

Equation 6.1 can apply to <u>moles</u> or any <u>quantity</u> that is <u>conserved</u>. As an example, look at <u>Figure 6.7</u> in which we have converted all of the mass quantities in <u>Figure 2</u> to their equivalent values in moles.

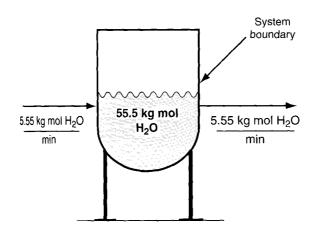


Figure 7 The system in Figure 2 with the flow rates shown in kg mol.

If the process is in the **steady state**, the **accumulation** term by definition is **<u>zero</u>**, and **Equation 6.1** simplifies to a famous truism

What goes in must come out (In = Out) ...6.2

If you are analyzing an unsteady-state process, the accumulation term over a time interval can be calculated as

$$\{Accumulation\} = \begin{cases} Final material \\ in the system \end{cases} - \begin{cases} Initial material \\ in the system \end{cases}$$
(6.3)

The **times** you select for the final and initial conditions can be anything, but you usually select an **interval** such as **1 minute** or **1 hour** rather than specific times.

★ When you combine Equations 6.1 and 6.3 you get the <u>general material balance</u> for a component in the system in the <u>absence of reaction</u>

	Final material		Initial material)	Flow into		Flow out of	
<	in the system	} – {	in the system	} = <	the system	} -	the system	,6.4
	at t ₂		at t ₁	J	$ from t_1 to t_2 $	ļ	$(\mathbf{from} \ \mathbf{t}_1 \ \mathbf{to} \ \mathbf{t}_2)$	

Example 1

Will you save money if instead of buying premium 89 octane gasoline at \$1.269 per gallon that has the octane you want, you blend sufficient 93 octane supreme gasoline at \$1.349 per gallon with 87 octane regular gasoline at \$1.149 per gallon?

Solution

Choose a **basis** of **1** gallon of **89** octane gasoline, the desired product. The system is the gasoline tank.

- For simplicity, assume that **no gasoline exists** in the tank at the start of the blending, and **one gallon exists** in the tank at the end of the blending.
- This arrangement corresponds to an unsteady-state process. Clearly it is an open system.

The initial number of gallons in the system is zero and the final number of gallons is one.

Let \mathbf{x} = the number of gallons of 87 octane gasoline added, and \mathbf{y} = the number of gallons of 93 octane added to the blend. Since $\mathbf{x} + \mathbf{y} = \mathbf{1}$ is the total flow into the tank,

 $\therefore y = 1 - x$

According to Equation (6.4) the balance on the octane number is

Accumulation Inputs
$$\frac{89 \text{ octane}}{|\text{I gal}|} \frac{|\text{I gal}|}{|\text{I gal}|} = 0 = \frac{87 \text{ octane}}{|\text{I gal}|} \frac{x \text{ gal}}{|\text{I gal}|} + \frac{|93 \text{ octane}|}{|\text{I gal}|} \frac{(1-x) \text{ gal}}{|\text{I gal}|}$$

The solution is x = 2/3 gal and thus y = 1 - x = 1/3 gal.

The cost of the blended gasoline is (2/3)(\$1.149) + (1/3)(\$1.349) = \$1.216

A value less than the cost of the 89 octane gasoline (\$1.269).

Multiple Component Systems

Suppose the input to a vessel contains more than one component, such as 100 kg/min of a 50% water and 50% sugar (sucrose, $C_{12}H_{22}O_{11}$, MW = 342.3) mixture (see Figure 8). The mass balances with respect to the sugar and water, balances that we call component balances.

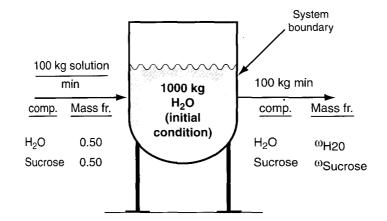


Figure 8 An open system involving two components.

For Example, look at the mixer shown in Figure 9, an apparatus that mixes two streams to increase the concentration of NaOH in a dilute solution. **The mixer is a steady – state open system**. Initially the mixer is empty, and after 1 hour it is empty again.

Basis = 1 hour for convenience. As an alternate to the **basis** we selected you could select $\underline{F_1} = 9000 \text{ kg/hr}$ as the basis, or $F_2 = 1000 \text{ kg/hr}$ as the basis; the numbers for this example would not change – just the units would change. Here are the components and total balances in kg:

	Flow	v in		Accum
Balances	F ₁	F ₂	Flow out	
NaOH	450	500	950	= 0
H ₂ O	8,550	500	9,050	= 0
H ₂ O Total	9,000	1,000	10,000	= 0

We can convert the kg shown in Figure 6.9 to kg moles by dividing each compound by its respective molecular weight (NaOH = 40 and $H_2O = 18$).

NaOH:
$$\frac{450}{40} = 11.25$$
 $\frac{500}{40} = 12.50$ $\frac{950}{40} = 23.75$
H₂O: $\frac{8550}{18} = 475$ $\frac{500}{18} = 27.78$ $\frac{9050}{18} = 502.78$

Then the component and total balances in kg mol are:

	Flow	v in		Accum.	
Balances	F ₁	F ₂	Flow out		
NaOH	11.25	12.50	23.75	= 0	
H_2O	475	27.78	502.78	= 0	
Total	486.25	40.28	536.53	= 0	

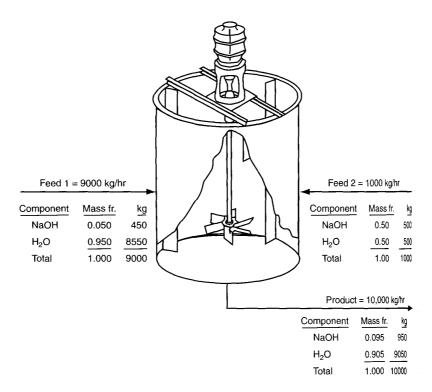


Figure 9 Mixing of a dilute stream of NaOH with a concentrated stream of NaOH. Values below the stream arrows are based on 1 hour of operation.

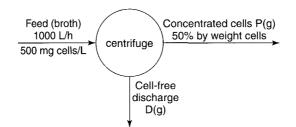
Example 2

Centrifuges are used to separate particles in the range of 0.1 to 100 μ m in diameter from a liquid using centrifugal force. Yeast cells are recovered from a broth (a liquid mixture containing cells) using a tubular centrifuge (a cylindrical system rotating about a cylindrical axis). Determine the amount of the cell-free discharge per hour if 1000 L/hr is fed to the centrifuge, the feed contains 500 mg cells/L, and the product stream contains 50 wt.% cells. Assume that the feed has a density of 1 g/cm³.

Solution

This problem involves a steady state, open (flow) system without reaction.

Basis = 1 hour





M.B. on cells

In (mass) = Out (mass)

$$\frac{1000 \text{ L feed}}{1 \text{ L feed}} \left| \frac{500 \text{ mg cells}}{1 \text{ L feed}} \right| \frac{1 \text{ g}}{1000 \text{ mg}} = \frac{0.5 \text{ g cells}}{1 \text{ g } P} \left| \frac{P \text{ g}}{1 \text{ g}} \right|$$

P = 1000 g

M.B. on fluid

In (mass) = Out (mass)

$$\frac{1000 \text{ L}}{1 \text{ L}} \left| \frac{1000 \text{ cm}^3}{1 \text{ L}} \right| \frac{1 \text{ g fluid}}{1 \text{ cm}^3} = \frac{1000 \text{ g } P}{1 \text{ g } P} \left| \frac{0.50 \text{ g fluid}}{1 \text{ g } P} + D \text{ g fluid} \right|$$

 $D = (10^6 - 500) g$

Accounting for Chemical Reactions in Material Balances

Chemical reaction in a system requires the augmentation of Equation 6.4 to take into account the effects of the reaction. To illustrate this point, look at Figure 10, which shows a steady – state system in which HC1 reacts with NaOH by the following reaction:

$$NaOH + HCl \rightarrow NaC1 + H_2O$$

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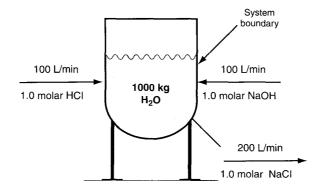


Figure 10 Reactor for neutralizing HC1 with NaOH.

Equation 4 must be augmented to include terms for the <u>generation</u> and <u>consumption</u> of components by the chemical reaction in the system as follows

$$\begin{cases} Accumulation \\ within the \\ system \end{cases} = \begin{cases} Input \\ through \\ the system \\ boundaries \end{cases} - \begin{cases} Output \\ through \\ the system \\ boundaries \end{cases} + \begin{cases} Generation \\ within the \\ system \end{cases} - \begin{cases} Consumption \\ within the \\ system \end{cases} \qquad \dots 6.5$$