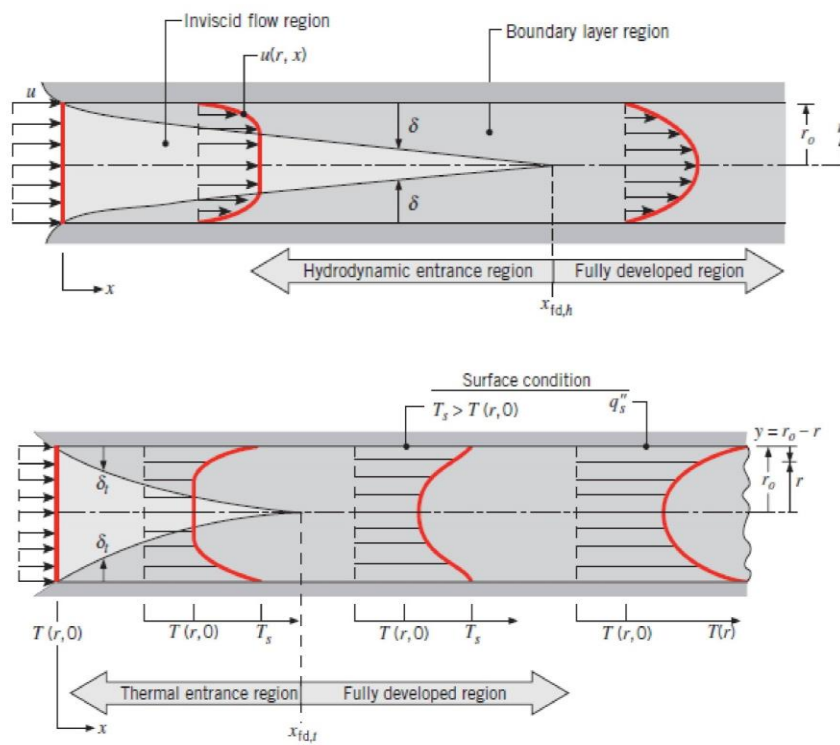


Chapter six

Empirical and practical Relation for Forced-Convection heat transfer

Convection heat transfer for internal flow [flow in conduits]

Conduits "pipe-tube-duct"



For pipes: [circular cross section area]

$$Re = \frac{\rho v D}{\mu} = \frac{v D}{\nu} = \frac{4 \dot{m}}{\pi D \mu} = \frac{\dot{m}}{A \mu} = \frac{4 \rho \dot{V}}{\pi D \mu} = \frac{4 \dot{V}}{\pi D \nu}$$

D: internal diameter for pipe , m

v: Fluid velocity m/s

\dot{V} : Volume flow rate m³/s

\dot{m} : mass flow rate kg/s

ν : kinematic viscosity (m²/s)

μ : dynamic viscosity of fluid (N s/m²)

ρ : fluid density kg/ m³

For pipes :

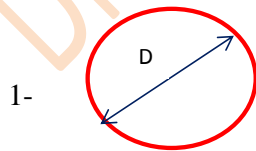
$Re < 2300$, **Laminar Flow**

$Re > 2300$, **Turbulent Flow**

For non-circular cross sectional area,

We use what is called hydraulic diameter (D_H) in calculation, (Re and Nu ... etc.).

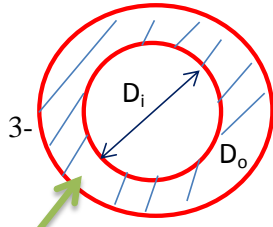
$$D_H = \frac{4A}{P} = \frac{4 \cdot \text{cross sectional area}}{\text{wet perameter}}$$



$$D_H = \frac{4 \cdot \frac{\pi D^2}{4}}{\pi D} = D$$



$$D_H = \frac{4 \cdot LH}{2L + 2H} = \frac{2 \cdot LH}{L + H}$$

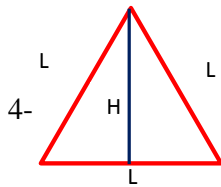


Fluid

$$\frac{(D_o - D_i)(D_o + D_i)}{D_o + D_i}$$

$$D_H = D_o - D_i$$

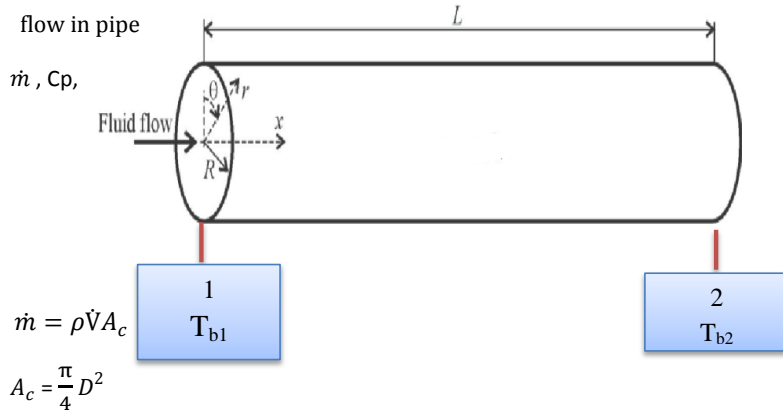
$$D_H = \frac{\frac{4 \cdot \frac{\pi}{4} (D_o^2 - D_i^2)}{\pi D_i \pi D_o}}{\frac{D_o^2 - D_i^2}{D_i \cdot D_o}} = \frac{D_o^2 - D_i^2}{D_i \cdot D_o} =$$



$$H = \sqrt{L^2 - \left(\frac{1}{2}L\right)^2} = \frac{\sqrt{3}}{2}L$$

$$D_H = \frac{4 \cdot \frac{1}{2} \cdot L \cdot H}{3 \cdot L} = \frac{4 \cdot \frac{1}{2} \cdot L \cdot \frac{\sqrt{3}}{2}L}{3 \cdot L} = \frac{L}{\sqrt{3}}$$

Sec 6-2 : Empirical Relations for pipe and tube flow



✚ 1 = درجة حرارة عند النقطة 1 T_{b1}

✚ 2 = درجة حرارة عند النقطة 2 T_{b2}

✚ Bulk temperature represents energy average or “mixing cup” condition

✚ (The bulk temperature is defined as the energy-average fluid temperature across the tube)

$$q = \dot{m}c_p(T_{b2} - T_{b1})$$

also

$$q = hA(T_w - \bar{T}_b)$$

$$\bar{T}_b = \frac{T_{b1} + T_{b2}}{2}$$

$$A = \pi dL$$

\bar{T}_b : ونقصد بها درجة حرارة المائع ولكن هنا توجد درجة حرارة عند المدخل والمخرج لذلك استخدمنا average لهما

$$Nu_d = \frac{h \cdot D_H}{k}$$

D = hydraulic diameter of pipe

1- Fully developed turbulent flow in smooth tube

$$Nu_d = 0.023 Re_d^{0.8} Pr^n$$

$$0.6 < Pr < 100$$

$$2500 < Re_d < 1.25 \times 10^5$$

All properties @ \bar{T}_b $n = \begin{cases} 0.4 & \text{for heating of the fluid.} \\ 0.3 & \text{for cooling of the fluid.} \end{cases}$

2- Turbulent flow in smooth tube suggest better results

$$Nu_d = 0.0214(Re_d^{0.8} - 100)Pr^{0.4}$$

$$0.5 < Pr < 1.5$$

$$10^4 < Re_d < 5 \times 10^6$$

$$Nu_d = 0.012(Re_d^{0.87} - 280)Pr^{0.4}$$

$$1.5 < Pr < 500$$

$$3000 < Re_d < 10^6$$

3- Fully developed Turbulent flow but there is large temperature difference (the Temp. effect is taken into consideration)

$$Nu_d = 0.027 Re_d^{0.8} Pr^{1/3} \left(\frac{\mu}{\mu_w}\right)^{0.14}$$

All properties @ \bar{T}_b except μ_w @ T_w

4 – *more accurate* Relation for fully developed flow in smooth or Rough tube (there is friction involves)

$$Nu_d = \frac{(f/8)Re_d Pr}{1.07 + 12.7(f/8)^{1/2}(Pr^{1/3} - 1)} \left(\frac{\mu_b}{\mu_w}\right)^n$$

$$0.5 < Pr < 2000$$

$$10^4 < Re_d < 5 \times 10^6$$

$$0 < \frac{\mu_b}{\mu_w} < 40$$

All properties @ $T_f = \frac{T_w - \bar{T}_b}{2}$ except

μ_b @ \bar{T}_b and μ_w @ T_w

$n = 0.11$ If $T_w > \bar{T}_b$

$n = 0.25$ If $T_w < \bar{T}_b$

$n = 0$ For constant heat flux

5- Turbulent in entrance region (the flow is not developed)

$$Nu_d = 0.036 Re_d^{0.8} Pr_r^{1/3} \left(\frac{d}{L}\right)^{0.55}$$

$$10 < \frac{L}{d} < 400$$

L = length of tube

d = diameter of tube

All properties are evaluated @ \bar{T}_b

6- Fully developed **Laminer** flow in tube @ constant wall temperature

$$Nu_d = 366 + \frac{0.668 \left(\frac{d}{L}\right) Re_d Pr}{1 + 0.04 \left[\left(\frac{d}{L}\right) Re_d Pr\right]^{2/3}} \quad Tw = \text{constant}$$

$Nu_d = 3.66$ If tube is sufficiently long ,

7 – for **Laminer** flow in tube

$$Nu_d = 1.86 (Re_d Pr)^{1/3} \left(\frac{d}{L}\right)^{1/3} \left(\frac{\mu}{\mu_w}\right)^{0.4} \quad Tw = \text{constan}, \quad Re_d Pr \frac{d}{L} > 10$$

All properties @ \bar{T}_b except μ_w @ T_w

This equation can't be used for $L \gg \gg d$ (entirely long tube)

Problem 6-6: water at the rate of 3kg/s is heated from 5 to 15 °C by passing it through a 5 cm ID copper tube. The tube wall temperature is maintained at 90°C. What is the length of the tube?

Solution

$$\dot{m} = \frac{3\text{kg}}{\text{s}}, \quad T_{b1} = 5^\circ\text{C}, T_{b2} = 15^\circ\text{C}, D = 0.05\text{m}$$

$$T_k = 90^\circ\text{C}, \quad \text{find tube length } L?$$

$$q = hA(T_v - \bar{T}_b) = h(\pi dL)(T_v - \bar{T}_b)$$

$$l = \frac{q}{h\pi d h(T_w - \bar{T}_b)}$$

$$1- \bar{T}_b = \frac{T_{b1} + T_{b2}}{2} = \frac{5 + 15}{2} = 10^\circ\text{C}$$

$$T_b = 10^\circ$$

From table A - 9

$$C_p = 4.195 \frac{\text{Kj}}{\text{Kg}\cdot\text{C}}$$

$$2- \rho = 999.2 \text{ Kg/m}^3$$

$$\mu = 1.31 \times 10^{-3} \text{ Kg/m}\cdot\text{S}$$

$$K = 0.585 \text{ w/m}\cdot\text{C}$$

$$Pr = 9.4$$

$$3- q = \dot{m} c_p (T_{b2} - T_{b1}) = 3 \times 4195 \times (15 - 5) = 125850 \text{ w}$$

$$4- Re_d = \frac{\rho V D}{\mu} = \frac{4\dot{m}}{\pi D \mu} = \frac{4 \times 3}{\pi \times 0.05 \times 1.31 \times 10^{-3}} \Rightarrow Re_d = 58316 \text{ Turbulent}$$

5- Fully developed turbulent flow in smooth tube, table 6.8

$$6- Nu_d = 0.023 Re_d^{0.8} Pr^n \quad n = 0.4 \Rightarrow \text{heating}$$

$$Nu_d = 0.023 (58316)^{0.8} (9.4)^{0.4} = 366.1$$

$$Nu_d = \frac{hD}{k} \Rightarrow h = \frac{Nu \cdot k}{D} = \frac{366 \cdot 1 \times 0.535}{0.05} = 4283.4$$

$$7 - L = \frac{q}{h\pi d(T_w - \bar{T}_b)} = \frac{125850}{4283.4 \times \pi \times 0.05(90 - 10)}$$

$$L = 2.338 \text{ m} \quad \text{OR}$$

* using another relation هذه المعادلة تعطي دقة اكثر بالحل

$$Nu_d = 0.012(Re_d^{0.87} - 280)Pr^{0.4} \quad 1.5 < Pr < 500$$

$$3000 < Re < 10^6$$

$$Nu_d = 0.012((58316)^{0.87} - 280)(9.4)^{0.4}$$

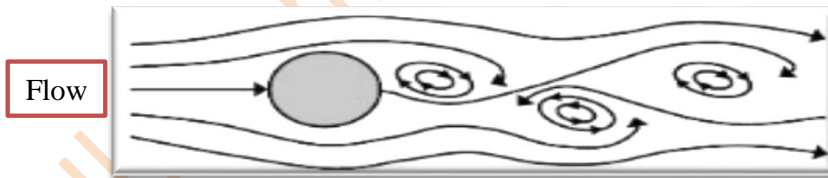
$$Nu_d = 403.5$$

$$Nu_d = \frac{hD}{k} \Rightarrow h = \frac{Nu_d \cdot k}{D} = \frac{403.5 \times 0.585}{0.05} = 4721.5$$

$$l = \frac{q}{h \cdot \pi d(T_w - \bar{T}_b)} = \frac{125850}{4721.5 \times \pi \times 0.05(90 - 10)}$$

$$l = 2.121 \text{ m}$$

Sec 5-3 Flow across cylinders and spheres



For cross flow over circular cylinders :

$$Nu_{df} = c Re_d^n Pr_f^{1/3} = \frac{hd}{k_f} \quad Pr \geq 0.7, 0.4 < Re_d < 400000,$$

[Comment [M1]: الخواص تحسب بدلالة T_f

هذه ترمز الى استخدام الخواص بدلالة درجه حراره (film) f :

$$T_f = \frac{T_w + T_\infty}{2}$$

$$Nu_{df} = \frac{hd}{k_f} = C \left(\frac{u_\infty d}{v_f} \right)^n Pr_f^{1/3} \quad [6-17]$$

C, n from table 6-2

$$Re_d = \frac{u_f d}{v_f}$$

Table 6-2 | Constants for use with Equation (6-17), based on References 8 and 9.

Re_{df}	C	n
0.4–4	0.989	0.330
4–40	0.911	0.385
40–4000	0.683	0.466
4000–40,000	0.193	0.618
40,000–400,000	0.0266	0.805

Other formula

$$Nu_d = 0.3 + \frac{0.62 Re_d^{1/2} Pr_f^{1/3}}{[1 + (0.4/Pr_f)^{2/3}]^{1/4}} \left[1 + \left(\frac{Re_d}{282000} \right)^{5/8} \right]^{4/5} \quad Pr_f > 0.2$$

$$10^2 < Re_d < 10^7$$

properties @ T_f

Example 6-7 : Air at 1 atm and 35°C flows across 0.5 cm diameter cylinder @ a velocity of 50 m/s . The cylinder surface is maintained at a Temperature of 50 °C.

Calculate the heat loss per unit length of the cylinder .

Sol:

$$q = hA(T_w - T_\infty) = h(\pi dL)(T_w - T_\infty)$$

$P = 1 \text{ atm}$, air, $T_\infty = 35^\circ\text{C}$, $d = 5 \text{ cm}$, $u = 50 \text{ m/s}$, $T_w = 150^\circ\text{C}$ find $\frac{q}{L}$?

$$1 - T_f = \frac{T_w + T_\infty}{2} = \frac{150 + 35}{2} = 92.5^\circ\text{C} = 365.5\text{K}$$

$$(2) \rho = \frac{P}{RT} = \frac{1.0132 \times 10^5}{287(365.5)} = 0.996 \frac{\text{kg}}{\text{m}^3}$$

(3) from table A-5 $\Rightarrow @T_f = 365.5 \text{ K}$

$$\mu_f = 2.14 \times 10^{-3} \frac{\text{kg}}{\text{m} \cdot \text{s}}, k_f = 0.0312 \frac{\text{W}}{\text{m} \cdot \text{C}}, Pr_f = 0.695$$

$$(5) Re_d = \frac{\rho_f u_\infty \cdot d}{\mu_f} = \frac{0.996 \times 50 \times 0.05}{2.14 \times 10^{-3}} = 1.129 \times 10^5$$

By using the following relation, (eq 6.17)

$$Nu_{d_f} = c Re_d^n Pr_f^{1/3} \quad \text{From Table (6-2) } C = 0.0266, n = 0.805$$

$$Nu_{d_f} = 0.0266 \times (1.129 \times 10^5)^{0.805} (0.695)^{1/3} = 275.1$$

$$Nu_{d_f} = \frac{hd}{k_f}, h = \frac{275.1 \times 0.0312}{0.05} = 171.7 \text{ W/m}^2 \cdot ^\circ\text{C}$$

$$\frac{q}{L} = h\pi d(T_w - T_\infty) = 171.7 \times \pi \times 0.05(150 - 35)$$

$$\frac{q}{L} = 3100 \text{ W/m}$$

Or

By using Relation (2)(b)

$$Nu_d = 0.3 + \frac{0.62 Re_d^{1/2} Pr^{1/3}}{[1 + (0.4/Pr)^{2/3}]^{1/4}} \left[1 + \left(\frac{Re_d}{282000} \right)^{1/2} \right] \quad 2 \times 10^4 < Re < 4 \times 10^5, Pr > 0.2$$

$$Nu_d = 0.3 + \frac{0 \cdot 62 (1.129 + 10^5)^{1/2} (0.695)^{1/3}}{[1 + (0.4/0.695)^{2/3}]^{1/4}} \left(1 + \left(\frac{1.129 + 10^5}{282000} \right)^{1/2} \right)$$

$$Nu_d = 264.47$$

$$Nu_{df} = \frac{hd}{k_f}, \quad h = \frac{264.47 \cdot 0.0312}{0.05} = 165.03 \text{ W/m}^2 \cdot ^\circ\text{C}$$

$$\frac{q}{L} = h\pi d(T_w - T_\infty) = 165.03 \times \pi \times 0.05(150 - 35)$$

$$\frac{q}{L} = 2981.15 \text{ W}$$