

## Serviceability requirements:

*Design* → { → *strength requirements*  
→ *servceability requirements*

## servceability requirements

1. Control of cracking
2. Control of deflection

## Control of cracking:

Types of cracks:

1. Flexural cracks
2. Diagonal tension cracks(shear cracks)
3. Shrinkage cracks

## Flexural cracks

Factors affecting crack width:

1. Proper distribution of flexural reinforcements reduce crack width.
2. The use of deformed bars reduce crack width.
3. Crack width is directly proportional to steel stress( $f_s$ ).
4. Crack width increases as concrete cover increases.

To limit surface cracks to a width that is generally acceptable in practice, the ACI code provision for spacing of reinforcement closest to a surface in tension shall not exceed that given by:

$$S = \frac{95000}{f_s} - 2.5C_c \leq 300 \left( \frac{252}{f_s} \right) \dots ACI eq10 - 4, sec10.6.4$$

**S**:C/C spacing of flexural tension reinforcement *nearest* to the extreme *tension* face,(mm),[where there is only one bar nearest to the extreme tension face, S is the width of the extreme tension face]

**Cc**: clear cover from the nearest surface in tension to the surface of the flexural tension reinforcement, mm

**fs**: calculated stress in reinforcement at service loads, MPa

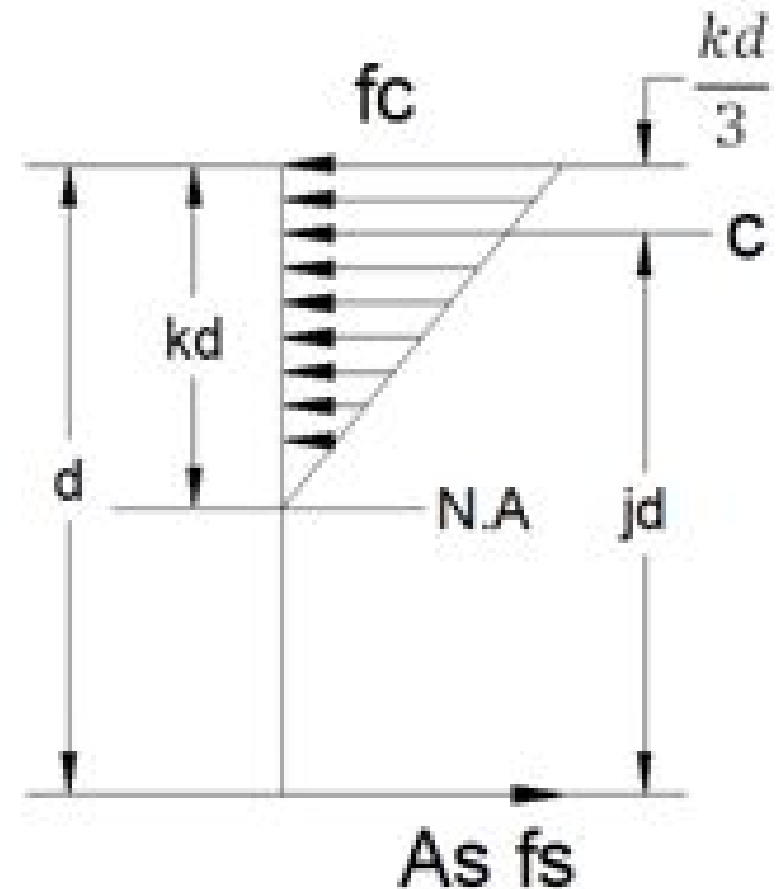
$$f_s = \frac{M}{A_s j d}$$

$$j = 1 - \frac{k}{3}$$

$$k = \sqrt{(2n\rho) + (n\rho)^2} - n\rho$$

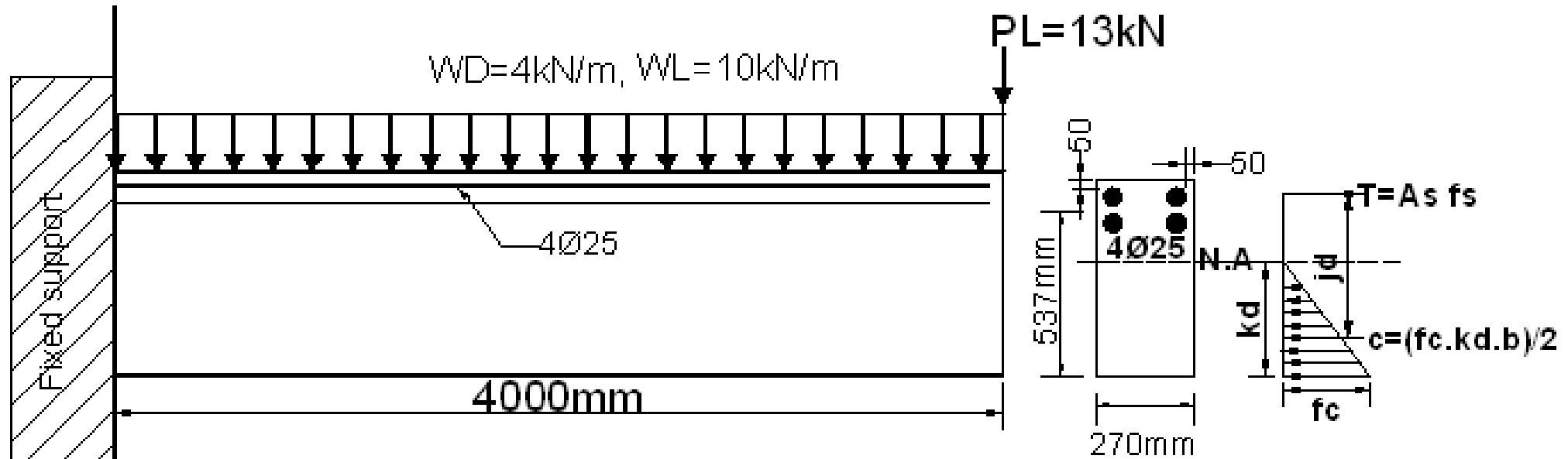
**\*ACI code allow to use fs=0.6fy**

**\* Cracks are to be checked for service load**



## EX1:

$f_y=300\text{MPa}$ ,  $f_c'=20\text{MPa}$ . Determine if beam meets the crack control criteria in the ACI code.



Solution:

$$\rho = \frac{4 * 491}{270 * 537} = 0.0135$$

$$E_s = 200000MPa$$

$$E_c = 4700\sqrt{f_c'} = 4700\sqrt{20} = 21019MPa$$

$$n = \frac{E_s}{E_c} = \frac{200000}{21019} = 9$$

$$k = \sqrt{(2n\rho) + (n\rho)^2} - n\rho$$

$$k = \sqrt{(2 * 9 * 0.0135) + (9 * 0.0135)^2} - 9 * 0.0135 = 0.38$$

$$j = 1 - \frac{k}{3} = 1 - \frac{0.38}{3} = 0.87$$

$$jd = 0.87 * 537 = 469\text{mm}$$

$$M_{ext} = 13 * 4 + (4 + 10) * 4 * \frac{4}{2} = 164\text{kN.m}$$

$$f_s = \frac{M}{A_s jd} = \frac{0.164}{1963 * 10^{-6} * 0.469}$$

$$= 178\text{MPa compare with } 0.6f_y = 180\text{MPa}$$

$$C_c = 50\text{mm}$$

$$S_{max_{c/c}} = \frac{95000}{f_s} - 2.5C_c = \frac{95000}{178} - 2.5 * 50 = 409mm$$

$$\leq 300 \left( \frac{252}{f_s} \right) = 300 \left( \frac{252}{178} \right) = 425mm$$

$$\therefore S_{max_{c/c}} = 409mm$$

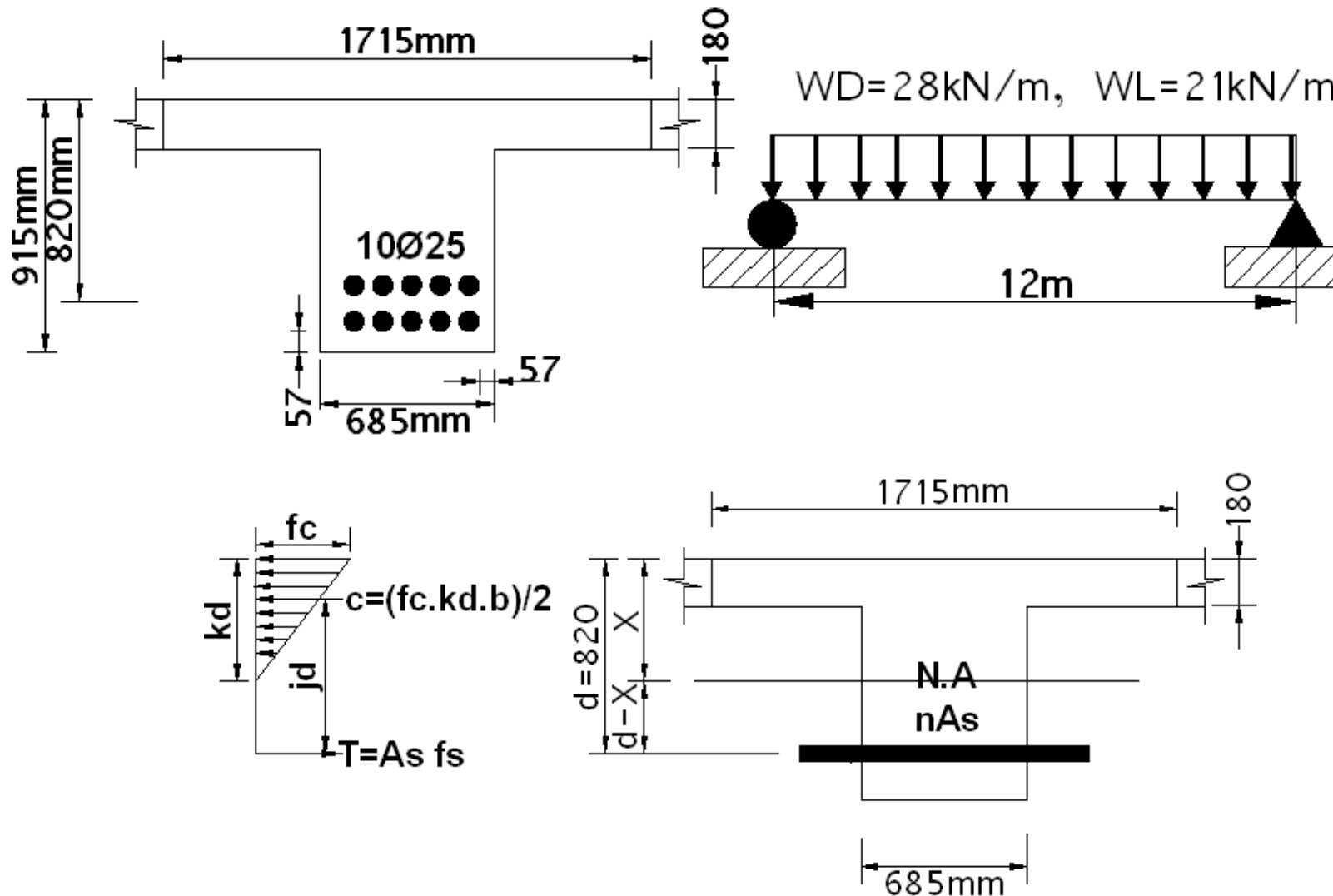
$$S_{c/c} = \frac{270 - 2 * 50 - 2 * \frac{25}{2}}{2 - 1} = 145mm < S_{max_{c/c}} = 409mm \rightarrow \therefore \text{the}$$

beam meets the crack control criteria in the ACI code



EX2:  $f_y=414\text{MPa}$ ,  $f_c'=28\text{MPa}$

Determine if beam meets the crack control criteria in the ACI code.



Solution:

$$A_s = 10\text{Ø}25 = 4910\text{mm}^2$$

$$E_s = 200000\text{MPa}$$

$$E_c = 4700\sqrt{f_c'} = 4700\sqrt{28} = 24870\text{MPa}$$

$$n = \frac{E_s}{E_c} = \frac{200000}{24870} = 8$$

Location of NA

$$\sum M_{NA} = 0$$

$$1715 * 180 \left( x - \frac{180}{2} \right) + 685 * (x - 180) * \frac{(x - 180)}{2}$$

$$= 8 * 4910(820 - x)$$

$$34205x^2 + 224672x - 48889040 = 0 \rightarrow x = kd = 172mm$$

$$jd = d - \frac{kd}{3} = 820 - \frac{172}{3} = 762mm$$

$$M_{ext} = \frac{Wl^2}{8} = \frac{(28 + 21) * 12^2}{8} = 882kN.m$$

$$M_{int} = A_s f_s jd \rightarrow f_s = \frac{M}{A_s jd} \rightarrow f_s = \frac{882 * 10^{-3}}{4910 * 10^{-6} * 0.762}$$

$$= 236MPa$$

$$C_c = 57 \text{ mm}$$

$$S_{max_{c/c}} = \frac{95000}{f_s} - 2.5C_c = \frac{95000}{236} - 2.5 * 57 = 260 \text{ mm}$$

$$\leq 300 \left( \frac{252}{f_s} \right) = 300 \left( \frac{252}{236} \right) = 321 \text{ mm}$$

$$\therefore S_{max_{c/c}} = 260 \text{ mm}$$

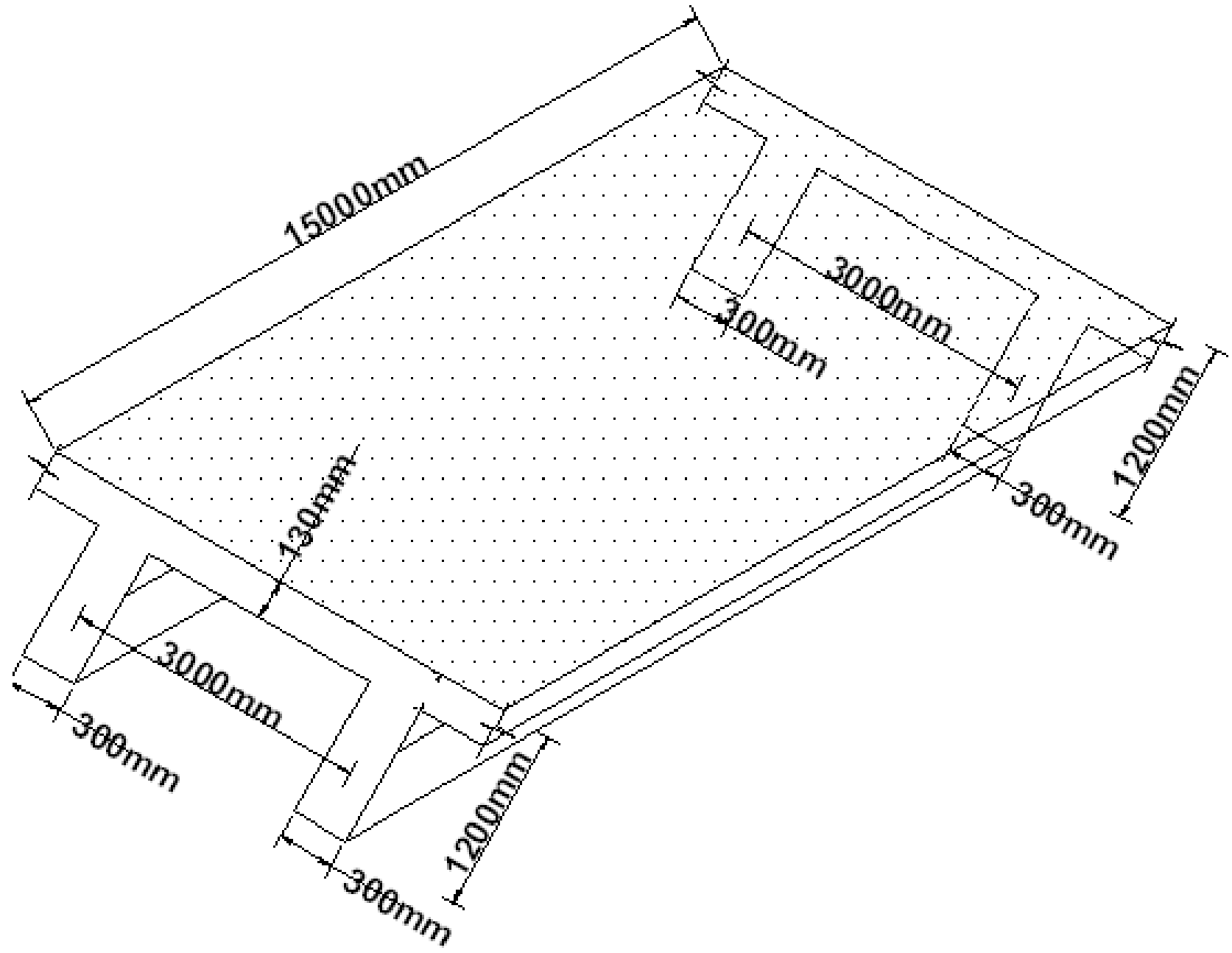
$$S_{c/c} = \frac{685 - 2 * 57 - 2 * \frac{25}{2}}{5 - 1} = 136 \text{ mm} < S_{max_{c/c}} = 260 \text{ mm} \rightarrow \therefore \text{the}$$

beam meets the crack control criteria in the ACI code

EX3:

$f_y=400\text{MPa}$ ,  $f_c'=28\text{MPa}$ , continuous T-beam, span=15m,  
 $b_w=300\text{mm}$ ,  $h_f=130\text{mm}$ , over all depth=1200mm, negative  
service moment [ $M_d=350\text{kN.m}$ ,  $M_l=950\text{kN.m}$ ].

Select reinforcement for negative moment, then, check if beam  
meets the crack control criteria in the ACI code.



Solution:

$$\bullet \frac{b-b_w}{2} \leq 8h_f \rightarrow \frac{b-300}{2} \leq 8 * 130 \rightarrow b = 2380mm$$

$$\bullet b \leq \frac{l}{4} \rightarrow b \leq \frac{15000}{4} \rightarrow b = 3750mm$$

$$\bullet \frac{b-b_w}{2} \leq \frac{l_{c1}+l_{c2}}{4} \rightarrow \frac{b-300}{2} \leq \frac{3000+300}{4} \rightarrow b = 3300mm$$

Choose min. value of  $b=2380mm$

$$Mu^* = 1.2Md + 1.6Ml$$

$$= 1.2 * 350 + 1.6 * 950 = 1940 kN.m$$

$$Mu = \phi \rho b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f_c'}\right)$$

$$1.94 = 0.9 * \rho * 0.3 * 1.134^2 * 400 \left(1 - 0.59\rho * \frac{400}{28}\right)$$

$$1.94 = 138.88\rho - 1170.6\rho^2 \rightarrow \rho = 0.0162 > \rho_{min} \text{ O.K}$$

$$A_s = 0.0162 * 300 * 1134 = 5511 \text{ mm}^2$$

Use 7Ø32(5628mm<sup>2</sup>)

Distribute the –ve reinf. Over the distance =

min(span/10=15000/10=1500mm, effective flange

width=2380mm)=1500mm



$$f_s = 0.6f_y = 0.6 * 400 = 240 \text{ MPa}$$

$$C_c = 40 + 10 = 50 \text{ mm}$$

$$S_{max_{c/c}} = \frac{95000}{f_s} - 2.5C_c = \frac{95000}{240} - 2.5 * 50 = 271 \text{ mm}$$

$$\leq 300 \left( \frac{252}{f_s} \right) = 300 \left( \frac{252}{240} \right) = 315 \text{ mm}$$

$$\therefore S_{max_{c/c}} = 271 \text{ mm}$$

$$S_{c/c} = \frac{1500 - 2 * \frac{32}{2}}{7 - 1} = 245 \text{ mm} < S_{max_{c/c}} = 271 \text{ mm} \rightarrow \therefore \text{the}$$

beam meets the crack control criteria in the ACI code

