



**2** spheres.

- one-dimensional
- temp is a function of radius only.

$$Q = \frac{4\pi K (T_i - T_o)}{\frac{1}{r_i} - \frac{1}{r_o}}$$

**P.2.17** sphere.

Aluminum

$$d_i = 4 \text{ cm}$$

$$d_o = 8 \text{ cm}$$

$$T_i = 100^\circ\text{C}$$

find  $Q$ .

$$r_i = 2 \text{ cm}$$

$$r_o = 4 \text{ cm}$$

$$T_o = 50^\circ\text{C}$$

$$R_{th} = \frac{\frac{1}{r_i} - \frac{1}{r_o}}{4\pi K}$$

$K \rightarrow$  from Table A-2.

Aluminum pure

$$K = 204 \text{ W/m}\cdot^\circ\text{C}$$

$$Q = \frac{4\pi * 204 (100 - 50)}{\frac{1}{0.02} - \frac{1}{0.04}} = \boxed{5127 \text{ W}}$$

\* Convection Boundary conditions.

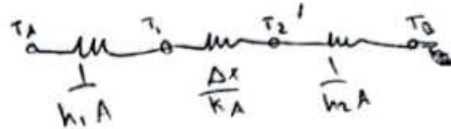
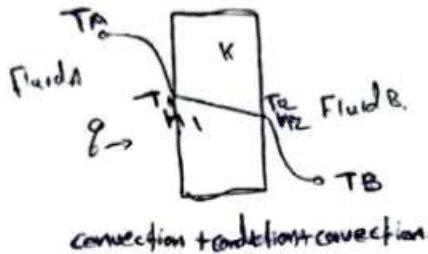
$$Q_{conv} = hA(T_w - T_\infty)$$

$$Q_{conv} = \frac{(T_w - T_\infty)}{\frac{1}{hA}} = \frac{\Delta T}{R_{th}}$$

$$R_{th} = \frac{1}{hA} \rightarrow \text{convection resistance.}$$



x plane wall exposed to hot fluid A on one side and a cooler fluid B on the other side.



$$R_{th} = \frac{1}{h_1 A} + \frac{\Delta x}{k A} + \frac{1}{h_2 A}$$

$$q = \frac{T_A - T_B}{\frac{1}{h_1 A} + \frac{\Delta x}{k A} + \frac{1}{h_2 A}}$$

P. 2-16

2-16 A spherical tank, 1 m in diameter, is maintained at a temperature of 120 °C and exposed to a convection environment. With  $h=25 \text{ W/m}^2 \cdot \text{°C}$  and  $T_\infty = 15 \text{ °C}$ , what thickness of urethane foam should be added to ensure that the outer temperature of the insulation does not exceed 40 °C? What percentage reduction in heat loss results from

$$q_{\text{without insulation}} = h A (T_w - T_\infty) = 25 \times 4 \pi (0.5)^2 (120 - 15)$$

$$q = \frac{4 \pi k (T_i - T_o)}{\frac{1}{r_i} - \frac{1}{r_o}} = h (4 \pi r_o^2) (T_o - T_\infty)$$

$$\frac{0.018 (120 - 40)}{\frac{1}{0.5} - \frac{1}{r_o}} = 25 r_o^2 (40 - 15)$$

$$r_o = 0.5023$$

$$\text{thick of insul.} = r_o - r_i = \boxed{0.023 \text{ m}}$$

$$q (\text{with insulation}) = 25 (4 \pi (0.5023)^2) (40 - 15) = \boxed{1982 \text{ W}}$$

$$\begin{aligned} h &= 25 \\ T_\infty &= 15 \\ T_o &= 40 \text{ °C} \\ k_f &= 0.018 \end{aligned}$$





\* over all Heat T. coeff. (U)

U: has the same unit of h  $W/m^2 \cdot C$

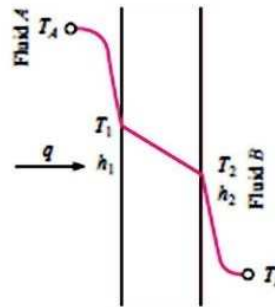
$$Q = UA \Delta T_{\text{overall}}$$

$$Q = hA \Delta T$$

$$U = \frac{Q}{A \Delta T}$$

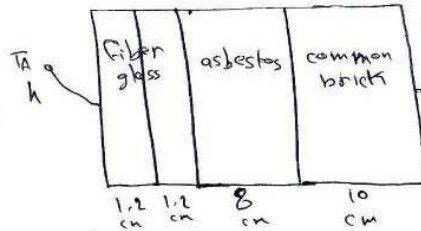
\* For plane wall.

$$Q = \frac{\Delta T}{\frac{1}{h_1 A} + \frac{\Delta x}{KA} + \frac{1}{h_2 A}}$$



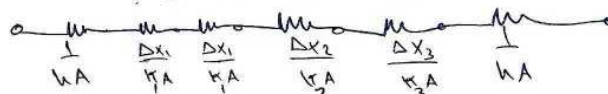
$$U = \frac{1}{\frac{1}{h_1} + \frac{\Delta x}{K} + \frac{1}{h_2}}$$

Q.2.27



$K_{\text{fiber glass}} = K_1 = 0.038$   
 $K_{\text{asbestos}} = K_2 = 0.154$   
 $K_{\text{brick}} = K_3 = 0.69$

$h = 12 \text{ W/m}^2 \cdot C$



$$Q = \frac{\Delta T}{\frac{1}{hA} + \frac{\Delta x_1}{K_1 A} + \frac{\Delta x_2}{K_2 A} + \frac{\Delta x_3}{K_3 A} + \frac{1}{hA}}$$

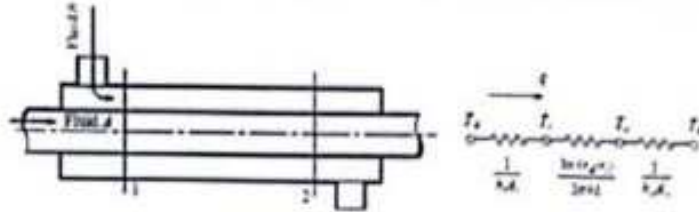
$$U = \frac{Q}{A \Delta T}$$

$$\therefore U = \frac{1}{\frac{1}{12} + \frac{0.012}{0.038} + \frac{0.012}{0.154} + \frac{0.08}{0.69} + \frac{1}{12}}$$

$$U = 0.624 \text{ W/m}^2 \cdot C \quad \#$$

\* U for cylindrical system

Figure 2-4 | Resistance analogy for hollow cylinder with convection boundaries



$$q = \frac{T_A - T_B}{\frac{1}{h_i A_i} + \frac{\ln(r_o/r_i)}{2\pi k L} + \frac{1}{h_o A_o}}$$

$U_i$ : overall H.T.C. Based on inside area.

$$U_i = \frac{q}{A_i \Delta T}$$

$$U_i = \frac{1}{\frac{1}{h_i} + \frac{A_i \ln(r_o/r_i)}{2\pi k L} + \frac{A_i}{A_o h_o}}$$

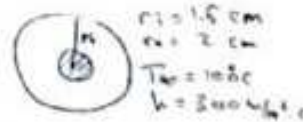
$U_o$ : overall H.T.C. Based on outside area.

$$U_o = \frac{q}{A_o \Delta T}$$

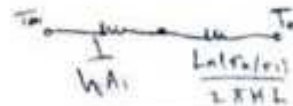
$$U_o = \frac{1}{\frac{A_o}{A_i} \frac{1}{h_i} + \frac{A_o \ln(r_o/r_i)}{2\pi k L} + \frac{1}{h_o}}$$

ex) A plastic ( $k = 0.5 \text{ W/m}\cdot\text{K}$ ) pipe carries fluid such that the convection H.T.C is  $300 \text{ W/m}^2\cdot\text{C}$ . The average fluid temp is  $100^\circ\text{C}$ , the pipe has an id (internal diameter) of 3cm and outer diameter of 4cm if the h.t rate through the pipe per unit length is  $500 \text{ W/m}$  determine

- Solu :-
- ① the external pipe temp
  - ②  $U_o$



①  $q = \frac{T_f - T_e}{\frac{1}{h_i A_{i,unit}} + \frac{\ln(r_o/r_i)}{2\pi k L}}$



$$\frac{q}{L} = 500 = \frac{100 - T_e}{\frac{1}{300 (2\pi \times 1.5 \times 10^{-2})} + \frac{\ln(2/1.5)}{2\pi (0.5)}}$$

$$A_i = 2\pi r_i L = 2\pi (1.5) L$$

$$\boxed{T_e = 36.5^\circ\text{C}}$$





$$\frac{q}{A_o \Delta T} = U_o A_o \Delta T = U_i A_i \Delta T$$

$$\frac{q}{A_o \Delta T} = U_o$$

لا ننسى!  $\Rightarrow$   
 لاحظ لايوجد  $A_o$

$$q = \frac{\Delta T}{\frac{1}{h_i A_i} + \frac{\ln(r_o/r_i)}{2\pi k L}}$$

$$\frac{q}{\Delta T} = U_o A_o = \frac{1}{\frac{1}{h_i A_i} + \frac{\ln(r_o/r_i)}{2\pi k L}}$$

$$U_o = \frac{1}{\frac{A_o}{h_i A_i} + \frac{A_o \ln(r_o/r_i)}{2\pi k L}} = \frac{1}{\frac{2\pi r_o k}{h_i (2\pi r_i k)} + \frac{2\pi r_o k \ln(r_o/r_i)}{2\pi k L}}$$

$$U_o = \frac{1}{\frac{r_o}{h_i r_i} + \frac{r_o \ln(r_o/r_i)}{k}} = \frac{1}{\frac{0.02}{300 \times 0.015} + \frac{0.02 \ln(2/1.5)}{0.5}}$$

$$U_o = 62.7 \text{ w/m}^2 \cdot \text{c} \quad \#$$

إذا أردت التحقق من الحل

$$q = U_o A_o \Delta T$$